

## Agilent Laser and Optics

## User's Manual, Volume I



Agilent Technologies

## Notices

© Agilent Technologies, Inc. 1992, 1996, 2000, 2002, 2007

No part of this manual may be reproduced in any form or by any means (including electronic storage and retrieval or translation into a foreign language) without prior agreement and written consent from Agilent Technologies, Inc. as governed by United States and international copyright laws.

#### **Manual Part Number**

05517-90086

#### Edition

Fifth edition, September 2007

Printed in USA

Agilent Technologies, Inc. 5301 Stevens Creek Boulevard Santa Clara, California 95052-8059

#### Warranty

The material contained in this document is provided "as is," and is subject to being changed, without notice, in future editions. Further, to the maximum extent permitted by applicable law, Agilent disclaims all warranties, either express or implied, with regard to this manual and any information contained herein, including but not limited to the implied warranties of merchantability and fitness for a particular purpose. Agilent shall not be liable for errors or for incidental or consequential damages in connection with the furnishing, use, or performance of this document or of any information contained herein. Should Agilent and the user have a separate written agreement with warranty terms covering the material in this document that conflict with these terms, the warranty terms in the separate agreement shall control.

#### **Technology Licenses**

The hardware and/or software described in this document are furnished under a license and may be used or copied only in accordance with the terms of such license.

#### **Restricted Rights Legend**

If software is for use in the performance of a U.S. Government prime contract or subcontract, Software is delivered and licensed as "Commercial computer software" as defined in DFAR 252.227-7014 (June 1995), or as a "commercial item" as defined in FAR 2.101(a) or as "Restricted computer software" as defined in FAR 52.227-19 (June 1987) or any equivalent agency regulation or contract clause. Use, duplication or disclosure of Software is subject to Agilent Technologies' standard commercial license terms, and non-DOD Departments and Agencies of the U.S. Government will receive no greater than Restricted Rights as defined in FAR 52.227-19(c)(1-2) (June 1987). U.S. Government users will receive no greater than Limited Rights as defined in FAR 52.227-14 (June 1987) or DFAR 252.227-7015 (b)(2) (November 1995), as applicable in any technical data.

#### **Safety Notices**

#### CAUTION

A CAUTION notice denotes a hazard. It calls attention to an operating procedure, practice, or the like that, if not correctly performed or adhered to, could result in damage to the product or loss of important data. Do not proceed beyond a CAUTION notice until the indicated conditions are fully understood and met.

#### WARNING

A WARNING notice denotes a hazard. It calls attention to an operating procedure, practice, or the like that, if not correctly performed or adhered to, could result in personal injury or death. Do not proceed beyond a WARNING notice until the indicated conditions are fully understood and met.

## **User's Manual**

Agilent 5517A/B/C/D/DL/FL Laser Head Agilent 5519A/B Laser Head Agilent 5529A Dynamic Calibrator Agilent 10567A Dual Beam Beam-Splitter Agilent 10700A 33% Beam Splitter Agilent 10700B 4% Beam Splitter Agilent 10700C 15% Beam Splitter Agilent 10701A 50% Beam Splitter Agilent 10702A Linear Interferometer (and 10702A-001 with Windows) Agilent 10703A Retroreflector Agilent 10704A Retroreflector Agilent 10705A Single Beam Interferometer Agilent 10705A-080 Fiber Optic Receiver Adapter Agilent 10706A Plane Mirror Interferometer Agilent 10706A-080 Fiber Optic Receiver Adapter Agilent 10706B High Stability Plane Mirror Interferometer Agilent 10707A Beam Bender Agilent 10710B Adjustable Mount Agilent 10711A Adjustable Mount Agilent 10713B/C/D Cube Corner Agilent 10715A Differential Interferometer (and 10715A-001 Turned Configuration) Agilent 10716A High Resolution Interferometer (and 10716A-001 Turned Configuration) Agilent 10717A Wavelength Tracker Agilent 10719A One-axis Differential Interferometer Agilent 10719A-C02 One-axis Differential Interferometer (low thermal drift) Agilent 10721A Two-axis Differential Interferometer Agilent 10721A-C01 Two-axis Differential Interferometer (low thermal drift) Agilent 10722A Plane Mirror Converter Agilent 10723A High Stability Adapter Agilent 10724A Plane Mirror Reflector Agilent 10725A 50% Beam Splitter Agilent 10725B 4% Beam Splitter Agilent 10725C 15% Beam Splitter Agilent 10726A Beam Bender

Agilent 10728A Plane Mirror Agilent 10735A Three-axis Interferometer Agilent 10736A Three-Axis Interferometer Agilent 10736A-001 Three-Axis Interferometer / Beam Bender Agilent 10737L, R Compact Three-axis Interferometers Agilent 10753B Laser Tripod Agilent 10759A Footspacing Kit Agilent 10766A Linear Interferometer Agilent 10767A Linear Interferometer Agilent 10767B Lightweight Retroreflector Agilent 10768A Diagonal Measurement Kit Agilent 10769A Beam Steering Mirror Agilent 10766A Linear Interferometer Agilent 10767A Linear Interferometer Agilent 10767B Lightweight Retroreflector Agilent 10770A Angular Interferometer Agilent 10771A Angular Retroreflector Agilent 10772A Turning Mirror Agilent 10773A Flatness Mirror Agilent 10774A Short Range Straightness Optics Agilent 10776A Straightness Accessory Kit Agilent 10777A Optical Square Agilent 10780C Receiver Agilent 10780F Remote Receiver Agilent 10790A/B/C Receiver Cable Agilent 10880A/B/C Receiver Cable Agilent 10881A/B/C Laser Head Cable Agilent 10882A/B/C Laser Head Cable Agilent 10884B Power Supply Agilent E1705A Fiber Optic Cable Agilent E1706A Remote Sensor Agilent E1708A Remote Dynamic Receiver Agilent E1709A Remote High-Performance Receiver Agilent E1705A Fiber-Optic Cable Agilent E1706A Remote Sensor Agilent E1708A Remote Dynamic Receiver Agilent E1709A Remote High-Performance Receiver

Continued on next page . .

## **Laser and Optics**

## **User's Manual**

#### (Continued)

Agilent E1826E/F/G One-Axis Plane Mirror Interferometer Agilent E1827A Two-Axis Vertical Beam Interferometer Agilent E1837A Three-Axis Vertical Beam Interferometer Agilent E1833C 15% Bare Beam Splitter Agilent E1833E 33% Bare Beam Splitter Agilent E1833G 50% Bare Beam Splitter Agilent E1833J 67% Bare Beam Splitter Agilent E1833M 100% Bare Beam Splitter (Beam Bender) Agilent N1203C Precision Beam Translator Agilent N1204C Precision Horizontal Beam Bender Agilent N1207C Precision Vertical Beam Bender Agilent N1208C 33% Bare Beam Splitter Agilent N1208D 40% Bare Beam Splitter Agilent N1208E 50% Bare Beam Splitter Agilent N1208F 66% Bare Beam Splitter Agilent N1208G 60% Bare Beam Splitter Agilent N1250A/B High Performance Receiver Cable Agilent N1251A/B High Performance Laser Head Cable Agilent Z4399A Three-Axis Interferometer Agilent Z4420B Five-Axis Interferometer

#### Certification and Warranty

#### Certification

Agilent Technologies certifies that this product met its published specification at the time of shipment from the factory. Agilent further certifies that its calibration measurements are traceable to the United States National Institute of Standards and Technology (formerly National Bureau of Standards), to the extent allowed by the Institute's calibration facility, and to the calibration facilities of other International Standards Organization members.

#### Warranty

Agilent warrants Agilent hardware, accessories and supplies against defects in materials and workmanship for a period specified by each product from date of shipment. If Agilent receives notice of such defects during the warranty period, Agilent will, at its option, either repair or replace products which prove to be defective. Replacement products may be either new or like-new.

Agilent warrants that Agilent software will not fail to execute its programming instructions, for the period specified above, due to defects in material and workmanship when properly installed and used. If Agilent receives notice of such defects during the warranty period, Agilent will replace software media which does not execute its programming instructions due to such defects.

For detailed warranty information, see back matter.

#### Safety Considerations

#### General

This product and related documentation must be reviewed for familiarization with this safety markings and instructions before operation.

This product is a safety Class I instrument (provided with a protective earth terminal).

#### **Before Applying Power**

Verify that the product is set to match the available line voltage and the correct fuse is installed.

#### **Before Cleaning**

Disconnect the product from operating power before cleaning.

#### Safety Earth Ground

An uninterruptible safety earth ground must be provided from the mains power source to the product input wiring terminals or supplied power cable.

Warning Symbols That May Be Used In This Book



Instruction manual symbol; the product will be marked with this symbol when it is necessary for the user to refer to the instruction manual.



Indicates hazardous voltages.



Indicates earth (ground) terminal.





Indicates terminal is connected to chassis when such connection is not apparent. Safety Considerations (contd)



Indicates Alternating current.

Indicates Direct current.

#### WARNING

BODILY INJURY OR DEATH MAY RESULT FROM FAILURE TO HEED A WARNING. DO NOT PROCEED BEYOND A WARNING UNTIL THE INDICATED CONDITIONS ARE FULLY UNDERSTOOD AND MET.

#### CAUTION

Damage to equipment, or incorrect measurement data, may result from failure to heed a caution. Do not proceed beyond a CAUTION until the indicated conditions are fully understood and met.

These CAUTION labels are required by the United States Center for Devices and Radiological Health. Failure to follow their instructions may result in personal injury.

This symbol indicates laser radiation.



CAUTION: Laser radiation when open. DO NOT STARE INTO THE BEAM

For additional safety and acoustic noise information, see back matter.

#### Agilent Technologies, Inc. Santa Clara Site 5301 Stevens Creek Boulevard Santa Clara, California 95052-8059

Contents

## Contents

#### 1 About This Manual

Introduction 20 How to Locate Information 20 Manual Organization 20 Manuals Available 23 Table 1. Laser Head and Receiver Manuals 23 How to Order Manuals 24

#### 2 Familiarization and Initial Operation

Introduction 26 A one-axis example is used for simplicity 26 26 Basic steps apply to all laser systems Agilent laser interferometer positioning systems at a glance 26 Figure 1. Typical single-axis Agilent Laser Interferometer Positioning System 27 All Agilent laser systems share a similar configuration 27 A controller is required for all laser positioning systems 28 What follows? 28 Setting Up the System Electronics 29 Install the laser electronics board in the PC 29 Install the API library and monitor program on computers used for program development 29 Connect the electronics cables 31 Power up the laser head 31 Aligning the Optics 32 **Making Measurements** 33 Figure 2. Start/Programs pop-up menu 33 Figure 3. Monitor screen after opening the application 34

Figure 4. Measurement screen 35

Solving Problems 36

#### 3 System Design Considerations

```
Introduction
               38
   Figure 5. Possible component motions
                                           39
Accuracy Considerations
                           40
Determining What Equipment is Needed
                                          40
   Table 2. Equipment choices
                                  41
Electronic Components
                          46
   Transducer Systems
                          46
   PC-Based Electronics
                           46
   VME Compatible Electronics
                                  46
   PC-Based PCI Electronics
                               46
   Calibrator System Electronics
                                   47
Adjustment Considerations
                              48
                                       48
   Laser beam and optics protection
   Figure 6. Protective covers for optics and laser beam
                                                         49
   Figure 7. Collapsible spiral cover for movable retroreflector
                                                               50
System Grounding
                     51
Laser Head
              52
                 52
   Orientation
   Mounting plane tolerance
                                52
   Figure 8. Laser position transducer mounting
                                                  52
   Pointing stability
                       53
   Thermal isolation
                       53
   Vibration isolation
                        53
                         53
   Magnetic shielding
   Mounting
                53
Optics
         54
   Plane of orientation with respect to laser head
                                                    54
   Effect of optics on measurement direction sense
                                                      54
   Figure 9. Direction sense - fringe counts increase as optics move apart
                                                                           54
   Configuration effects
                           55
   Vibration isolation for optics
                                  55
   Adjustable mounts for optics
                                  56
   Fasteners for optics
                          56
   Vacuum applications
                           56
```

	Differential measurements with interferometers 57 Moving interferometer instead of reflector 58 Introducing an offset into the laser beam 58
	Beam Path Loss Computation 59 Considerations 59 Figure 10. Introducing an offset into the laser beam 60 Calculation of signal loss 61
	Receivers 64 General 64 Clearance for laser beam 64 Alignment adjustment required 64
	<ul> <li>Example Configurations 65</li> <li>Single-axis system for servo-track writing 65</li> <li>Figure 11. Single-axis system for servo-track writing 66</li> <li>Multiaxis configurations 66</li> <li>Multiaxis system for a precision x-y stage 67</li> <li>Figure 12. Multiaxis system for a precision x-y stage 67</li> <li>Figure 13. Four-axis configuration 69</li> <li>Figure 14. Two-axis plane mirror interferometer configuration 70</li> <li>Figure 15. X-Y stage installed in a vacuum chamber 70</li> <li>Figure 16. Two-axis system using two Agilent 10715A differential interferometers 72</li> <li>Figure 17. Yaw measurement of x-y stage using discrete plane mirror interferometers 72</li> <li>Figure 18. Optical Method for Yaw Measurement 74</li> <li>Figure 19. Optical Method for Yaw Measurement 74</li> </ul>
	Optical Device Troubleshooting 75
	Site Preparation 76 Site preparation for laser head 76 Site preparation for optical devices 76 Figure 20. Agilent 5517C-009 Mounting Location - Dimensions 77 Site preparation for referenced interferometers 78
4 System	n Installation and Alignment
	Introduction 80
	Pre-Installation Checklist 80

System Grounding 81

External Cabling 81

Laser head cables 81

```
Receiver cables
                     82
Mounting Optics
                   84
   Adjustable mounts
                        84
   Figure 21. Agilent 10710B and Agilent 10711A adjustable mounts
                                                                      84
   Typical mounting of optics which use adjustable mounts
                                                             84
   Fasteners
                85
   Figure 22. Horizontal plane mounting using the Agilent 10710B adjustable mount
                                                                                    85
   Figure 23. Vertical plane mounting using the Agilent 10710B adjustable mount
                                                                                  86
   Figure 24. Horizontal plane mounting using the Agilent 10711A adjustable mount
                                                                                    87
   Figure 25. Vertical Plane Mounting Using the Agilent 10711A Adjustable Mount
                                                                                   87
Aligning Optics
                  88
   General
              88
   Figure 26. Optimum alignment
                                   88
   Figure 27. Effect of optics misalignment
                                             89
   Figure 28. Effects of angular misalignment to the direction of travel
                                                                       90
   Alignment principles
                          90
Receiver Alignment and Gain Adjustment
                                           92
Autoreflection Method Summary
                                   92
   Figure 29. Using reference surfaces to align mirror
                                                       93
Overlapping Dots Method Summary
                                     94
   Figure 30. Measurement beam dot movement
                                                   95
   Figure 31. Results of reflector movement
                                              96
Aligning the Agilent 10702A Linear, Agilent 10766A Linear, and Agilent 10705A Single
Beam Interferometers
                        96
   Alignment aids (for Agilent 10702A, Agilent 10766A, Agilent 10705A)
                                                                         97
                                                                    97
   Figure 32. Linear and single-beam interferometer alignment aids
   Autoreflection alignment procedure (for Agilent 10702A, Agilent 10766A,
   Agilent 10705A)
                      98
   Figure 33. Autoreflection alignment
                                         98
   Overlapping dot alignment procedure (for Agilent 10702A, Agilent 10766A,
   Agilent 10705A)
                      102
   Figure 34. Overlapping dot alignment
                                          103
```

#### 5 Measurement Optics (General Information)

General 106 
 Table 3. Measurement Optics Summary
 107 Resolution 110 Table 4. Interferometer Resolutions 110 Range 110 Measurement Direction Sense 110 Figure 35. Effect of beam-directing optics on laser beam polarization orientations 112 Vibration Isolation 113 Fasteners 113 Vacuum Applications 114 **Use Through Window** 114 **Differential Measurements with Interferometers** 114 Moving Interferometer Instead of Reflector 116 6 NGI Measurement Optics (General Information) Introduction 118 Table 5. NGI Interferometers summary 119 NGI Optical Schematic 120 Figure 36. Next Generation Interferometer laser beam path 120 **NGI** Angular Resolution 121 Figure 37. NGI Angular Resolution diagram 122 Alignment and Mounting 123 General 123 Procedure 123 Figure 38. Interferometer datums relative to ideal zero stage angles 124 Figure 39. Setup for determining system zero stage angles 125

Figure 40. Interferometer mounting126Table 6. Screw Torque Requirement127

Figure 41. Input beam cone angle for ideal zero stage angles 127

Figure 42. Input Beam Position Adjustment128Measure Point Tolerance129Figure 43. Measure Point Tolerance129Fiber Optic Interface Specifications130

#### 7 Maintenance

General 132 **Procedures for Cleaning Optics** 132 Agilent Receivers 133 Measurement optics and beam-directing optics 133 Lens tissue 134 Alcohol 135 Maintenance Procedures 135 Before and After Service Product Safety Check 135

### 8 Troubleshooting

Figure 46. Agilent 10717A Wavelength Tracker troubleshooting tree 150

Before and After Service Product Safety Check 151

#### 9 Unpacking and Incoming Inspection

Introduction 154 Unpacking and Incoming Inspection 154 Warranty Claims 154

#### 10 Packaging for Storage or Shipment

Laser Tube156Tagging for Service156Original Packaging156Other Packaging156

#### 11 Principles of Operation

Introduction 160

Measurement Technique 161	
Introduction 161	
Creating the two-frequency las	er beam 161
Using the two-frequency laser	beam at the interferometer 162
Doppler frequency shifting 1	62

Basic Measurement System163Figure 47. Typical (older) Agilent Laser Position Transducer block diagram163

Basic Agilent Laser Measurement System Components 164

Laser head 164 System optics 164 Receiver 165 Environment sensors 166

#### 12 Accuracy and Repeatability

Introduction 168

The Components of System Accuracy and Repeatability 168

Table 10. Error components for accuracy and long- and short-term repeatability errorbudgets169Laser wavelength169Electronics error170Table 11.System measurement resolution for each interferometer171

**Optics nonlinearity** 172 Figure 48. Worst-case error resulting from imperfect separation of two beam components 173 Atmospheric compensation 173 176 Material thermal expansion **Optics thermal drift** 176 Figure 49. Conventional plane mirror interferometer with unequal path lengths that result in optics thermal drift 177 Figure 50. Agilent 10706B High Stability Plane Mirror Interferometer Beam Paths 178 Figure 51. Comparison of optics thermal drift between Interferometers 179 Deadpath error 180 Figure 52. Deadpath caused by unequal lengths from initial point 181 Table 12. Deadpath mirror positions and values for Agilent interferometers 182 Figure 53. Optical configuration with and without deadpath 184 Abbé error 186 Figure 54. Abbé error 187 Cosine error 188 Figure 55. Cosine error 188 Determining System Accuracy and Repeatability 189 Table 13. Laser interferometer system accuracy and repeatability error 189 Examples — Determining System Accuracy and Repeatability 190 Table 14. Parameters needed to calculate each error component 191 Precision Coordinate Measuring Machine (CMM) example 191 Figure 56. Laser system configuration for a precision Coordinate Measuring Machine (CMM) 192 Table 15. System accuracy with and without atmospheric compensation 196 Figure 57. Worst-case System Accuracy with and without Atmospheric Compensation for the CMM example 197 Figure 58. Worst-case System Accuracy with Atmospheric Compensation for the CMM example 197 Figure 59. Worst-case System Repeatability with and without Atmospheric Compensation for the CMM example 198 Figure 60. Worst-case System Repeatability with Atmospheric Compensation for the CMM example 199 IC Wafer Stepper example 199 200 Figure 61. Laser System Configuration for an Integrated Circuit Wafer Stepper Table 16. IC Stepper system accuracy with and without atmospheric compensation 203 Figure 62. Worst-case System Accuracy with and without Atmospheric Compensation for the Wafer Stepper example 204 Figure 63. Worst-case System Accuracy with Atmospheric Compensation for the Wafer Stepper example 205

Figure 64. Worst-case System Long-term Repeatability with and without Atmospheric Compensation for the Wafer Stepper example 206 Figure 65. Worst-case System Long-term Repeatability with Atmospheric Compensation for the Wafer Stepper example 207 208 Achieving Optimum System Accuracy and Repeatability Minimizing environmental effects 208 Figure 66. Relative effect of errors in atmospheric and material temperature 209 Laser compensation capability 210 Manual compensation 210 210 Automatic compensation Sensor placement 211 Figure 67. Air sensor orientation (Agilent 10751D shown) 212 WOL compensation method comparison 213 Table 17. Laser system measurement accuracy comparison\* 213 Non-Uniform Environments 214 Changing temperature conditions 214 Air turbulence 214 **Optics installation effects** 215 216 Minimizing deadpath errors Figure 68. Equal path length correction 217 Compensation for deadpath errors 217 Minimizing Abbé error 220 Figure 69. Positioning of measurement axis to minimize Abbé error 221 Figure 70. X-Y Stage measurement with Agilent 10706A Plane Mirror Interferometer 222 222 References 13 Wavelength-of-Light Compensation Introduction 224 "Absolute" Pressure Versus "Barometric" Pressure 224 Calculation of Exact Wavelength-of-Light (WOL) Compensation Factor 225 Wavelength-of-Light (WOL) Compensation Tables 227 Table 18. Metric—Wide-Range (Temp = 2 to 50° C, Press = 525 to 800 mm, 50% Humidity) 228 Table 19. Metric—Low Alt, Low Temp, Low Humidity  $(\text{Temp} = 5 \text{ to } 13^{\circ} \text{ C}, \text{ Press} = 720 \text{ to } 800 \text{ mm}, 20\% \text{ Humidity})$ 229 Table 20. Metric—Low Alt, Low-Mid Temp, Low Humidity (Temp = 13.5 to 21.5° C, Press = 720 to 800 mm, 20% Humidity) 230 Table 21. Metric—Low Alt, Mid Temp, Low Humidity

 $(\text{Temp} = 22 \text{ to } 30^{\circ} \text{ C}, \text{ Press} = 720 \text{ to } 800 \text{ mm}, 20\% \text{ Humidity})$  231

Table 22. Metric—Low Alt, High-Mid Temp, Low Humidity (Temp = 30.5 to 38.5° C, Press = 720 to 800 mm, 20% Humidity) 232 Table 23. Metric—High Alt, Low Temp, Low Humidity (Temp = 5 to 13° C, Press = 640 to 720 mm, 20% Humidity) 233 Table 24. Metric—High Alt, Low-Mid Temp, Low Humidity  $(\text{Temp} = 13.5 \text{ to } 21.5^{\circ} \text{ C}, \text{ Press} = 640 \text{ to } 720 \text{ mm}, 20\% \text{ Humidity})$ 234 Table 25. Metric—High Alt, Mid Temp, Low Humidity  $(\text{Temp} = 22 \text{ to } 30^{\circ} \text{ C}, \text{ Press} = 640 \text{ to } 720 \text{ mm}, 20\% \text{ Humidity})$ 235 Table 26. Metric—High Alt, High-Mid Temp, Low Humidity (Temp = 30.5 to 38.5° C, Press = 640 to 720 mm, 20% Humidity) 236 Table 27. Metric—Low Alt, Low Temp, Med Humidity (Temp = 5 to 13° C, Press = 720 to 800 mm, 50% Humidity) 237 Table 28. Metric—Low Alt, Low-Mid Temp, Med Humidity (Temp = 13.5 to 21.5° C, Press = 720 to 800 mm, 50% Humidity) 238 Table 29. Metric—Low Alt, Mid Temp, Med Humidity (Temp = 22 to 30° C, Press = 720 to 800 mm, 50% Humidity) 239 Table 30. Metric—Low Alt, High-Mid Temp, Med Humidity (Temp = 30.5 to 38.5° C, Press = 720 to 800 mm, 50% Humidity) 240 Table 31. Metric—High Alt, Low Temp, Med Humidity  $(\text{Temp} = 5 \text{ to } 13^{\circ} \text{ C}, \text{ Press} = 640 \text{ to } 720 \text{ mm}, 50\% \text{ Humidity})$ 241 Table 32. Metric—High Alt, Low-Mid Temp, Med Humidity 242  $(\text{Temp} = 13.5 \text{ to } 21.5^{\circ} \text{ C}, \text{Press} = 640 \text{ to } 720 \text{ mm}, 50\% \text{ Humidity})$ Table 33. Metric—High Alt, Mid Temp, Med Humidity (Temp = 22 to 30° C, Press = 640 to 720 mm, 50% Humidity) 243 Table 34. Metric—High Alt, High-Mid Temp, Med Humidity 244 (Temp = 30.5 to 38.5° C, Press = 640 to 720 mm, 50% Humidity) Table 35. Metric—Low Alt, Low Temp, High Humidity 245  $(\text{Temp} = 5 \text{ to } 13^{\circ} \text{ C}, \text{ Press} = 720 \text{ to } 800 \text{ mm}, 80\% \text{ Humidity})$ Table 36. Metric—Low Alt, Low-Mid Temp, High Humidity (Temp = 13.5 to 21.5° C, Press = 720 to 800 mm, 80% Humidity) 246 Table 37. Metric—Low Alt, Mid Temp, High Humidity (Temp = 22 to 30° C, Press = 720 to 800 mm, 80% Humidity) 247 Table 38. Metric—Low Alt, High-Mid Temp, High Humidity (Temp = 30.5 to 38.5° C, Press = 720 to 800 mm, 80% Humidity) 248 Table 39. Metric—High Alt, Low Temp, High Humidity (Temp = 5 to 13° C, Press = 640 to 720 mm, 80% Humidity) 249 Table 40. Metric—High Alt, Low-Mid Temp, High Humidity (Temp = 13.5 to 21.5° C, Press = 640 to 720 mm, 80% Humidity) 250 Table 41. Metric—High Alt, Mid Temp, High Humidity (Temp = 22 to 30° C, Press = 640 to 720 mm, 80% Humidity) 251 Table 42. Metric—High Alt, High-Mid Temp, High Humidity  $(\text{Temp} = 30.5 \text{ to } 38.5^{\circ} \text{ C}, \text{ Press} = 640 \text{ to } 720 \text{ mm}, 80\% \text{ Humidity})$ 252 Table 43. English—Wide Range (Temp = 40 to  $120^{\circ}$  F, Press = 20 to 31 inches, 50% Humidity) 253

Table 44. English—Low Alt, Low Temp, Low Humidity	
(Temp = 40 to 56° F, Press = 27 to 31 inches, 20% Humidit	• •
Table 45. English—Low Alt, Low-Mid Temp, Low Humidity	
(Temp = 57 to 73° F, Press = 27 to 31 inches, 20% Humidit	y) 255
Table 46. English—Low Alt, Mid Temp, Low Humidity	
(Temp = 74 to 90° F, Press = 27 to 31 inches, 20% Humidit	y) 256
Table 47. English—Low Alt, High-Mid Temp, Low Humidity	
(Temp = 91 to 107° F, Press = 27 to 31 inches, 20% Humid	ity) 257
Table 48. English—High Alt, Low Temp, Low Humidity	
(Temp = 40 to 56° F, Press = 23 to 27 inches, 20% Humidit	y) <mark>258</mark>
Table 49. English—High Alt, Low-Mid Temp, Low Humidity	/
(Temp = 57 to 73° F, Press = 23 to 27 inches, 20% Humidit	y) 259
Table 50. English—High Alt, Mid Temp, Low Humidity	
(Temp = 74 to 90° F, Press = 23 to 27 inches, 20% Humidit	y) <mark>260</mark>
Table 51. English—High Alt, High-Mid Temp, Low Humidit	y
(Temp = 91 to 107° F, Press = 23 to 27 inches, 20% Humid	ity) 261
Table 52. English—Low Alt, Low Temp, Med Humidity	
(Temp = 40 to 56° F, Press = 27 to 31 inches, 50% Humidit	y) <mark>262</mark>
Table 53. English—Low Alt, Low-Mid Temp, Med Humidity	/
(Temp = 57 to 73° F, Press = 27 to 31 inches, 50% Humidit	y) <mark>263</mark>
Table 54. English—Low Alt, Mid Temp, Med Humidity	
(Temp = 74 to 90° F, Press = 27 to 31 inches, 50% Humidit	y) 264
Table 55. English—Low Alt, High-Mid Temp, Med Humidit	у
(Temp = 91 to 107° F, Press = 27 to 31 inches, 50% Humid	ity) 265
Table 56. English—High Alt, Low Temp, Med Humidity	
(Temp = 40 to 56° F, Press = 23 to 27 inches, 50% Humidit	y) <mark>266</mark>
Table 57. English—High Alt, Low-Mid Temp, Med Humidit	y
(Temp = 57 to 73° F, Press = 23 to 27 inches, 50% Humidit	y) 267
Table 58. English—High Alt, Mid Temp, Med Humidity	
(Temp = 74 to 90° F, Press = 23 to 27 inches, 50% Humidit	y) <mark>268</mark>
Table 59. English—High Alt, High-Mid Temp, Med Humidit	Σ <b>γ</b>
(Temp = 91 to 107° F, Press = 23 to 27 inches, 50% Humid	ity) 269
Table 60. English—Low Alt, Low Temp, High Humidity	
(Temp = 40 to 56° F, Press = 27 to 31 inches, 80% Humidit	y) 270
Table 61. English—Low Alt, Low-Mid Temp, High Humidity	/
(Temp = 57 to 73° F, Press = 27 to 31 inches, 80% Humidit	y) 271
Table 62. English—Low Alt, Mid Temp, High Humidity	
(Temp = 74 to 90° F, Press = 27 to 31 inches, 80% Humidit	y) 272
Table 63. English—Low Alt, High-Mid Temp, High Humidit	у
(Temp = 91 to 107° F, Press = 27 to 31 inches, 80% Humid	ity) 273
Table 64. English—High Alt, Low Temp, High Humidity	
(Temp = 40 to 56° F, Press = 23 to 27 inches, 80% Humidit	y) 274
Table 65. English—High Alt, Low-Mid Temp, High Humidit	у
(Temp = 57 to 73° F, Press = 23 to 27 inches, 80% Humidit	

Table 66. English—High Alt, Mid Temp, High Humidity276(Temp = 74 to 90° F, Press = 23 to 27 inches, 80% Humidity)276Table 67. English—High Alt, High-Mid Temp, High Humidity277(Temp = 91 to 107° F, Press = 23 to 27 inches, 80% Humidity)277

#### 14 Material Expansion Coefficients

Linear Thermal Expansion Coefficients of Metals and Alloys280Table 68.Linear thermal expansion coefficients of metals and alloys280

#### 15 Glossary

#### 292

Figure 71. Degrees of freedom (for X-Axis)293Table 69. Number systems295

#### Index

## Figures

Figure 1. Typical single-axis Agilent Laser Interferometer Positioning System 27
Figure 2. Start/Programs pop-up menu 33
Figure 3. Monitor screen after opening the application 34
Figure 4. Measurement screen 35
Figure 5. Possible component motions 39
Figure 6. Protective covers for optics and laser beam 49
Figure 7. Collapsible spiral cover for movable retroreflector 50
Figure 8. Laser position transducer mounting 52
Figure 9. Direction sense - fringe counts increase as optics move apart 54
Figure 10. Introducing an offset into the laser beam 60
Figure 11. Single-axis system for servo-track writing 66
Figure 12. Multiaxis system for a precision x-y stage 67
Figure 13. Four-axis configuration 69
Figure 14. Two-axis plane mirror interferometer configuration 70
Figure 15. X-Y stage installed in a vacuum chamber 70
Figure 16. Two-axis system using two Agilent 10715A differential interferometers 72
Figure 17. Yaw measurement of x-y stage using discrete plane mirror interferometers 72
Figure 18. Optical Method for Yaw Measurement 74
Figure 19. Optical Method for Yaw Measurement 74
Figure 20. Agilent 5517C-009 Mounting Location - Dimensions 77
Figure 21. Agilent 10710B and Agilent 10711A adjustable mounts 84
Figure 22. Horizontal plane mounting using the Agilent 10710B adjustable mount 85
Figure 23. Vertical plane mounting using the Agilent 10710B adjustable mount 86
Figure 24. Horizontal plane mounting using the Agilent 10711A adjustable mount 87
Figure 25. Vertical Plane Mounting Using the Agilent 10711A Adjustable Mount 87
Figure 26. Optimum alignment 88
Figure 27. Effect of optics misalignment 89
Figure 28. Effects of angular misalignment to the direction of travel 90
Figure 29. Using reference surfaces to align mirror 93
Figure 30. Measurement beam dot movement 95
Figure 31. Results of reflector movement 96
Figure 32. Linear and single-beam interferometer alignment aids 97
Figure 33. Autoreflection alignment 98
Figure 34. Overlapping dot alignment 103
Figure 35. Effect of beam-directing optics on laser beam polarization orientations 112
Figure 36. Next Generation Interferometer laser beam path 120
Figure 37. NGI Angular Resolution diagram 122
Figure 38. Interferometer datums relative to ideal zero stage angles 124
Figure 39. Setup for determining system zero stage angles 125
Figure 40. Interferometer mounting 126

- Figure 41. Input beam cone angle for ideal zero stage angles 127
- Figure 42. Input Beam Position Adjustment 128
- Figure 43. Measure Point Tolerance 129
- Figure 44. Agilent 5517A/B/C/D Laser Head—troubleshooting tree 143
- Figure 45. Agilent Receiver troubleshooting tree 147
- Figure 46. Agilent 10717A Wavelength Tracker troubleshooting tree 150
- Figure 47. Typical (older) Agilent Laser Position Transducer block diagram 163
- Figure 48. Worst-case error resulting from imperfect separation of two beam components 173
- Figure 49. Conventional plane mirror interferometer with unequal path lengths that result in optics thermal drift 177
- Figure 50. Agilent 10706B High Stability Plane Mirror Interferometer Beam Paths 178
- Figure 51. Comparison of optics thermal drift between Interferometers 179
- Figure 52. Deadpath caused by unequal lengths from initial point 181
- Figure 53. Optical configuration with and without deadpath 184
- Figure 54. Abbé error 187
- Figure 55. Cosine error 188
- Figure 56. Laser system configuration for a precision Coordinate Measuring Machine (CMM) 192
- Figure 57. Worst-case System Accuracy with and without Atmospheric Compensation for the CMM example 197
- Figure 58. Worst-case System Accuracy with Atmospheric Compensation for the CMM example 197
- Figure 59. Worst-case System Repeatability with and without Atmospheric Compensation for the CMM example 198
- Figure 60. Worst-case System Repeatability with Atmospheric Compensation for the CMM example 199
- Figure 61. Laser System Configuration for an Integrated Circuit Wafer Stepper 200
- Figure 62. Worst-case System Accuracy with and without Atmospheric Compensation for the Wafer Stepper example 204
- Figure 63. Worst-case System Accuracy with Atmospheric Compensation for the Wafer Stepper example 205
- Figure 64. Worst-case System Long-term Repeatability with and without Atmospheric Compensation for the Wafer Stepper example 206
- Figure 65. Worst-case System Long-term Repeatability with Atmospheric Compensation for the Wafer Stepper example 207
- Figure 66. Relative effect of errors in atmospheric and material temperature 209
- Figure 67. Air sensor orientation (Agilent 10751D shown) 212
- Figure 68. Equal path length correction 217
- Figure 69. Positioning of measurement axis to minimize Abbé error 221
- Figure 70. X-Y Stage measurement with Agilent 10706A Plane Mirror Interferometer 222
- Figure 71. Degrees of freedom (for X-Axis) 293

#### **Tables**

## Tables

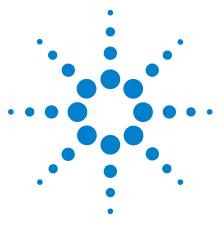
- Table 1. Laser Head and Receiver Manuals 23
- Table 2. Equipment choices 41
- Table 3. Measurement Optics Summary
   107
- Table 4. Interferometer Resolutions
   110
- Table 5. NGI Interferometers summary 119
- Table 6.
   Screw Torque Requirement
   127
- Table 7. Chapter content summary138
- Table 8. Recommended test equipment141
- Table 9. Agilent 10780C or Agilent 10780F Receiver signal chart
   145
- Table 10. Error components for accuracy and long- and short-term repeatability error budgets
   169
- Table 11.
   System measurement resolution for each interferometer
   171
- Table 12. Deadpath mirror positions and values for Agilent interferometers
   182
- Table 13. Laser interferometer system accuracy and repeatability error
   189
- Table 14. Parameters needed to calculate each error component
   191
- Table 15. System accuracy with and without atmospheric compensation
   196
- Table 16. IC Stepper system accuracy with and without atmospheric compensation 203
- Table 17. Laser system measurement accuracy comparison\*
   213
- Table 18. Metric—Wide-Range<br/>(Temp = 2 to 50° C, Press = 525 to 800 mm, 50% Humidity)228
- Table 19. Metric—Low Alt, Low Temp, Low Humidity<br/>(Temp = 5 to 13° C, Press = 720 to 800 mm, 20% Humidity)229
- Table 20. Metric—Low Alt, Low-Mid Temp, Low Humidity<br/>(Temp = 13.5 to 21.5° C, Press = 720 to 800 mm, 20% Humidity)230
- Table 21. Metric—Low Alt, Mid Temp, Low Humidity (Temp = 22 to 30° C, Press = 720 to 800 mm, 20% Humidity)
   231
- Table 22. Metric—Low Alt, High-Mid Temp, Low Humidity<br/>(Temp = 30.5 to 38.5° C, Press = 720 to 800 mm, 20% Humidity)232
- Table 23. Metric—High Alt, Low Temp, Low Humidity<br/>(Temp = 5 to 13° C, Press = 640 to 720 mm, 20% Humidity)233
- Table 24. Metric—High Alt, Low-Mid Temp, Low Humidity<br/>(Temp = 13.5 to 21.5° C, Press = 640 to 720 mm, 20% Humidity)234Table 25. Metric—High Alt, Mid Temp, Low Humidity
- (Temp = 22 to 30° C, Press = 640 to 720 mm, 20% Humidity) 235
- Table 26. Metric—High Alt, High-Mid Temp, Low Humidity(Temp = 30.5 to 38.5° C, Press = 640 to 720 mm, 20% Humidity)236
- Table 27. Metric—Low Alt, Low Temp, Med Humidity<br/>(Temp = 5 to 13° C, Press = 720 to 800 mm, 50% Humidity)237
- Table 28. Metric—Low Alt, Low-Mid Temp, Med Humidity<br/>(Temp = 13.5 to 21.5° C, Press = 720 to 800 mm, 50% Humidity)238

#### Tables

Table 29.	Metric—Low Alt, Mid Temp, Med Humidity (Temp = 22 to 30° C, Press = 720 to 800 mm, 50% Humidity)	239	
Tabla 20	Metric—Low Alt, High-Mid Temp, Med Humidity	200	
Table 30.	(Temp = $30.5$ to $38.5^{\circ}$ C, Press = $720$ to $800$ mm, $50\%$ Humidity)	24	0
Table 31.	Metric—High Alt, Low Temp, Med Humidity		
		241	
Table 32.	Metric—High Alt, Low-Mid Temp, Med Humidity		
	(Temp = 13.5 to 21.5° C, Press = 640 to 720 mm, 50% Humidity)	24	2
Table 33.	Metric—High Alt, Mid Temp, Med Humidity		
	(Temp = 22 to 30° C, Press = 640 to 720 mm, 50% Humidity)	243	
Table 34.	Metric—High Alt, High-Mid Temp, Med Humidity (Temp = 30.5 to 38.5° C, Press = 640 to 720 mm, 50% Humidity)	24	.4
Table 35.	Metric—Low Alt, Low Temp, High Humidity		
		245	
Table 36.	Metric—Low Alt, Low-Mid Temp, High Humidity		
	(Temp = 13.5 to 21.5° C, Press = 720 to 800 mm, 80% Humidity)	24	6
Table 37.	Metric—Low Alt, Mid Temp, High Humidity		
	(Temp = 22 to 30° C, Press = 720 to 800 mm, 80% Humidity)	247	
Table 38.	Metric—Low Alt, High-Mid Temp, High Humidity		
	(Temp = 30.5 to 38.5° C, Press = 720 to 800 mm, 80% Humidity)	24	8
Table 39.	Metric—High Alt, Low Temp, High Humidity		
	· · · · · · · · · · · · · · · · · · ·	249	
Table 40.	Metric—High Alt, Low-Mid Temp, High Humidity		
	(Temp = 13.5 to 21.5° C, Press = 640 to 720 mm, 80% Humidity)	25	0
Table 41.	Metric—High Alt, Mid Temp, High Humidity		
	(Temp = 22 to 30° C, Press = 640 to 720 mm, 80% Humidity)	251	
Table 42.	Metric—High Alt, High-Mid Temp, High Humidity		
	(Temp = $30.5$ to $38.5^{\circ}$ C, Press = $640$ to $720$ mm, $80\%$ Humidity)	25	2
Table 43.	English—Wide Range		
	(Temp = 40 to 120° F, Press = 20 to 31 inches, 50% Humidity)	253	
Table 44.	English—Low Alt, Low Temp, Low Humidity		
	(Temp = 40 to 56° F, Press = 27 to 31 inches, 20% Humidity)	254	
Table 45.	English—Low Alt, Low-Mid Temp, Low Humidity		
	(Temp = 57 to 73° F, Press = 27 to 31 inches, 20% Humidity)	255	
Table 46.	English—Low Alt, Mid Temp, Low Humidity		
	(Temp = 74 to 90° F, Press = 27 to 31 inches, 20% Humidity)	256	
Table 47.	English—Low Alt, High-Mid Temp, Low Humidity		
	(Temp = 91 to 107° F, Press = 27 to 31 inches, 20% Humidity)	257	
Table 48.	English—High Alt, Low Temp, Low Humidity		
	(Temp = 40 to 56° F, Press = 23 to 27 inches, 20% Humidity)	258	
Table 49.	English—High Alt, Low-Mid Temp, Low Humidity		
	(Temp = 57 to 73° F, Press = 23 to 27 inches, 20% Humidity)	259	
Table 50.	English—High Alt, Mid Temp, Low Humidity		
	(Temp = 74 to 90° F, Press = 23 to 27 inches, 20% Humidity)	260	

Table 51. English—High Alt, High-Mid Temp, Low Humidity (Temp = 91 to 107° F, Press = 23 to 27 inches, 20% Humidity)	261
Table 52. English—Low Alt, Low Temp, Med Humidity (Temp = 40 to 56° F, Press = 27 to 31 inches, 50% Humidity)	262
Table 53. English—Low Alt, Low-Mid Temp, Med Humidity (Temp = 57 to 73° F, Press = 27 to 31 inches, 50% Humidity)	263
Table 54. English—Low Alt, Mid Temp, Med Humidity (Temp = 74 to 90° F, Press = 27 to 31 inches, 50% Humidity)	264
Table 55. English—Low Alt, High-Mid Temp, Med Humidity (Temp = 91 to 107° F, Press = 27 to 31 inches, 50% Humidity)	265
Table 56. English—High Alt, Low Temp, Med Humidity (Temp = 40 to 56° F, Press = 23 to 27 inches, 50% Humidity)	266
Table 57. English—High Alt, Low-Mid Temp, Med Humidity (Temp = 57 to 73° F, Press = 23 to 27 inches, 50% Humidity)	267
Table 58. English—High Alt, Mid Temp, Med Humidity (Temp = 74 to 90° F, Press = 23 to 27 inches, 50% Humidity)	268
Table 59. English—High Alt, High-Mid Temp, Med Humidity (Temp = 91 to 107° F, Press = 23 to 27 inches, 50% Humidity)	269
Table 60. English—Low Alt, Low Temp, High Humidity (Temp = 40 to 56° F, Press = 27 to 31 inches, 80% Humidity)	270
Table 61. English—Low Alt, Low-Mid Temp, High Humidity (Temp = 57 to 73° F, Press = 27 to 31 inches, 80% Humidity)	271
Table 62. English—Low Alt, Mid Temp, High Humidity (Temp = 74 to 90° F, Press = 27 to 31 inches, 80% Humidity)	272
Table 63. English—Low Alt, High-Mid Temp, High Humidity (Temp = 91 to 107° F, Press = 27 to 31 inches, 80% Humidity)	273
Table 64. English—High Alt, Low Temp, High Humidity (Temp = 40 to 56° F, Press = 23 to 27 inches, 80% Humidity)	274
Table 65. English—High Alt, Low-Mid Temp, High Humidity (Temp = 57 to 73° F, Press = 23 to 27 inches, 80% Humidity)	275
Table 66. English—High Alt, Mid Temp, High Humidity (Temp = 74 to 90° F, Press = 23 to 27 inches, 80% Humidity)	276
Table 67. English—High Alt, High-Mid Temp, High Humidity (Temp = 91 to 107° F, Press = 23 to 27 inches, 80% Humidity)	277
Table 68.Linear thermal expansion coefficients of metals and alloysTable 69.Number systems295	280

**Tables** 



Agilent Laser and Optics User's Manual Volume I

1

## **About This Manual**

Introduction, 20 How to Locate Information, 20 Manual Organization, 20 Manuals Available, 23 How to Order Manuals, 24



## Introduction

This Laser and Optics User's Manual is intended for system designers concerned with designing and installing the optics, laser heads, and receivers for Agilent laser measurement systems into precision measuring or positioning equipment. Typical applications are for equipment used in the integrated circuit, disk drive, and precision machine industries.

This manual does not provide detailed information about laser head or receiver electronics. That information is provided in the manual for the particular unit. Refer to the section titled "Manuals Available" at the end of this chapter for details.

Information about measurement system electronic components (such as printed circuit boards, and air and material temperature sensors) is also not in this manual. Contact Agilent Technologies for help in ordering the documentation you want.

## **How to Locate Information**

The table of contents, list of figures, list of tables, and an alphabetical index of subjects help you locate information.

## **Manual Organization**

This user's manual consists of two volumes.

Volume I is organized as follows:

**Chapter 1, About this Manual** (this chapter), introduces you to the content and organization of this manual and gives information about available supplementary manuals.

**Chapter 2, Familiarization and Initial Operation**, describes a typical single-axis laser interferometer positioning system. It provides a simple "Getting Started" procedure that describes how to quickly set up and operate an Agilent laser interferometer positioning system, using PC-based electronics. Only essential information is included.

**Chapter 3, System Design Considerations**, provides general information that you should know and consider when designing Agilent laser measurement systems. Topics include: the basic components of an Agilent laser measurement system, effect of motion of any of the components, accuracy considerations, measurement range, adjustment considerations, laser beam and optics protection, system grounding, mounting plane tolerance, fastening,

clearance, pointing stability, thermal isolation, vibration isolation, magnetic shielding, effect of optics on measurement direction sense, and vacuum application.

**Chapter 4, System Installation and Alignment**, provides you with general procedures on how to install and align the various optics and accessories in various Agilent laser measurement systems. This chapter includes the alignment procedure for linear interferometers.

**Chapter 5, Measurement Optics (General Information)**, introduces Agilent's measurement optics—interferometers, straightness optics, retroreflectors (also called cube corners)—available for Agilent Technologies laser measurement systems. The first part of this chapter presents material that should be useful to the user of any of the interferometers.

Detailed information on the individual interferometer types, including characteristics and specifications are described in chapters 18 through 30. Each of these chapters provide descriptions, specifications, installation, and (except for linear interferometers) alignment information for each interferometer that is available for Agilent laser measurement systems. The alignment procedure for linear interferometers is in Chapter 4 of this manual.

**Chapter 6, NGI Measurement Optics (General Information)**, introduces Agilent's next generation interferometers (NGIs), and provides alignment, mounting, and fiber optics interface specifications.

Detailed information on the individual NGI types, including characteristics and specifications are described in chapters 31 through 34.

**Chapter 7, Maintenance**, provides general maintenance information and procedures for cleaning the lens of the Agilent 10780C, Agilent 10780F, Agilent E1708A, and Agilent E1709A receivers, the measurement optics, and the beam-directing optics. A "Before and After Service Product Safety Check" procedure is also provided.

**Chapter 8, Troubleshooting**, provides information to help you find defective components in an Agilent laser measurement system when a problem occurs. It can help determine whether the problem source is in the system electronics, environmental sensor, laser head, receiver, or the optics.

**Chapter 9, Unpacking and Incoming Inspection**, provides information for unpacking and inspection, and warranty claims.

**Chapter 10, Packaging for Storage or Shipment**, provides specific detailed information on packaging the laser tube assembly for storage or for shipment to Agilent for an exchange laser tube.

**Chapter 11, Principles of Laser Interferometry**, provides basic concepts, techniques, and principles that determine the overall measurement performance of Agilent laser measurement systems.

**Chapter 12, Accuracy and Repeatability**, provides basic concepts, techniques and principles that determine the overall measurement performance of Agilent laser measurement systems.

**Chapter 13, WOL Compensation Numbers**, provides tables of Wavelength-of-Light (WOL) compensation values for different environmental conditions, and step-by-step instructions on how to calculate the compensation factor if your system operates in an environment other than those covered by the tables.

**Chapter 14, Material Expansion Coefficients**, provides the linear thermal expansion coefficients of the most frequently used metals and alloys.

**Chapter 15, Glossary** 

Volume II is organized as follows:

**Chapter 16, Laser Heads**, provides descriptions and specifications for each of the current nine Agilent laser heads (Agilent 5517A, Agilent 5517B, Agilent 5517BL, Agilent 5517C, Agilent 5517D, Agilent 5517DL, Agilent 5517FL, Agilent 5519A, and Agilent 5519B).

**Chapter 17, Beam-Directing Optics**, provides descriptions, specifications, and other information for the beam splitters, beam benders, and beam translator that are available for Agilent laser measurement systems.

Chapter 18, Agilent 10702A and 10766A Linear Interferometers, and Agilent 10703A and 10676A Retroreflectors

Chapter 19, Agilent 10705A Single Beam Interferometer and Agilent 10704A Retroreflector

Chapter 20, Agilent 10706A Plane Mirror Interferometer

Chapter 21, Agilent 10706B High Stability Plane Mirror Interferometer

Chapter 22, Agilent 10715A Differential Interferometer

Chapter 23, Agilent 10716A High-Resolution Interferometer

Chapter 24, Agilent 10717A Wavelength Tracker

Chapter 25, Agilent 10719A and 10719A-C02 One-Axis Differential Interferometers

Chapter 26, Agilent 10721A and 10721A-C01 Two-Axis Differential Interferometers

Chapter 27, Agilent 10735A, 10736A, and 10736A-001 Three-Axis Interferometers

Chapter 28, Agilent 10737L and Agilent 10737R Compact Three-Axis Interferometers Chapter 29, Agilent 10770A Angular Interferometer with Agilent 10771A Angular Reflector

Chapter 30, Agilent 10774A Short Range Straightness Optics and Agilent 10775A Long Range Straightness Optics

Chapter 31, Agilent E1826E/F/G One-Axis Plane Mirror Interferometer

Chapter 32, Agilent E1827A Two-Axis Vertical Beam Interferometer

Chapter 33, Agilent Z4420B and Agilent Z4421B Five-Axis Interferometers

Chapter 34, Agilent E1837A, Z4399A, and Z4422B Three-Axis Interferometers

**Chapter 35, Receivers**, provides descriptions and system information for the Agilent 10780C, Agilent 10780F, Agilent E1708A, and Agilent E1709A receivers.

**Chapter 36, Accessories**, provides descriptions of hardware such as adjustable mounts, height adjuster/post, base, and cables. This chapter also provides descriptions, specifications, and system information for the optics which are not interferometers, and are not usually referred to as "beam-directing optics", such as plane mirror reflectors.

Index

## **Manuals Available**

Table 1 lists manuals currently available for Agilent laser heads and receivers. These manuals provide component-level troubleshooting and adjustment information.

In addition to these manuals, manuals are available describing the electronic components of a laser measurement system. Contact Agilent Technologies for help in ordering the information you need.

Product	Name of Manual	Current Agilent Part Number <sup>1</sup> (See NOTE below)
Agilent 5517A Laser Head	Agilent 5517A Laser Head Operating and Service Manual	05517-90046
Agilent 5517B Laser Head or Agilent 5517C Laser Head or Agilent 5517D Laser Head	Agilent 5517B/C/D Laser Head Operating and Service Manual	05517-90047

Table 1 Laser Head and Receiver Manuals

Product	Name of Manual	Current Agilent Part Number <sup>1</sup> (See NOTE below)
Agilent 5519A /B Laser Head	Agilent 5519A/B Laser Head Service Manual	05519-90006
Agilent 10780C Receiver or Agilent 10780F Remote Receiver	Agilent 10780C/F Operating and Service Manual	10780-90028
Agilent E1708A Remote Dynamic Receiver	Agilent E1707A/E1708A Operating Manual	E1708-90010
Agilent E1709A Remote High-Performance Receiver	Agilent E1709A Operating Manual	E1709-90006

Table 1 Laser Head and Receiver Manuals

<sup>1</sup>The Agilent part number of a manual may be changed when the manual is updated.

## How to Order Manuals

The Agilent Part Number of this manual is given on the front title page and back inside cover. Use it to order additional copies of this manual.



Agilent Laser and Optics User's Manual Volume I

## 2 Familiarization and Initial Operation

Introduction, 26 Setting Up the System Electronics, 29 Aligning the Optics, 32 Making Measurements, 33 Solving Problems, 36



## Introduction

Your laser interferometer positioning system is a set of optics, electronics, and electro-optical products that measure distance very accurately. This chapter provides basic information on how to set up a laser system to make measurements.

### A one-axis example is used for simplicity

Each axis of a laser positioning system is set up, aligned, and operated in essentially the same way. A six-axis system is similar to a one-axis system; therefore, only a single-axis system will be described in this chapter. Additional axes are then operated like the axis in the example.

### Basic steps apply to all laser systems

Specific products (identified by Agilent model number) are used in the example, but the installation and operation of other Agilent products are similar.

The example shows the use of PC-compatible electronics and a linear interferometer. If you are using a different interferometer, you may need to refer to the chapter in this manual that describes that interferometer for more details on optical alignment.

Regardless of the specific products you are using, the information and procedures presented in this chapter will help you get started quickly and easily.

### Agilent laser interferometer positioning systems at a glance

Figure 1 shows the components of a typical single-axis Agilent laser system. All Agilent laser systems combine optics (interferometer and reflector), electronics, and opto-electronics (laser head and receiver) to make a highly accurate positioning system.

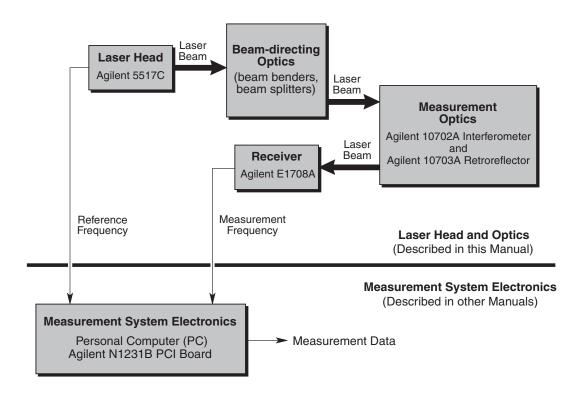


Figure 1 Typical single-axis Agilent Laser Interferometer Positioning System

### All Agilent laser systems share a similar configuration

Figure 1 shows PC-compatible electronics and a linear interferometer, but the system configuration is the same for all types of Agilent electronics and interferometers.

All Agilent laser systems require a reference signal from the laser head and a measurement signal from the receiver to be connected to the electronics to determine relative movement between the optics.

All Agilent laser systems feature separate laser head, interferometer, and reflector. The laser beam must be aligned with the optical elements and the motion of the optics to preserve beam alignment and provide an accurate measurement. The optics and receiver must be aligned so the beam strikes the lens of the receiver to generate a measurement signal. Misalignment results in loss of the measurement signal.

### A controller is required for all laser positioning systems

A controller is needed to control the system electronics and provide a display of the distance measured. The PC is the controller for PC-compatible electronics. Example and demo software programs are provided with the Agilent PC-compatible electronics to set up the system and display the measurement. VMEbus electronics require a separate controller.

### What follows?

The remaining sections of this chapter describe how to quickly set up and operate an Agilent laser interferometer positioning system, using PC-based electronics. Only essential information is included. Details not covered in this chapter are found in other chapters of this manual or in the manual(s) for the specific system electronics you are using.

The first step in system setup is connecting the system electronics. This includes installing the electronics boards in their backplane, connecting the cables from the laser head and receiver, and starting the software program.

The second step in system setup is aligning the optics. This step includes aligning the beam from the laser head parallel to the optics motion and aligning the optics and receiver lens so the beam enters the receiver lens during the entire range of motion.

The last step in system operation is making a measurement. This requires the software to be running on the controller to display measurement results.

Problem-solving is the last part in this chapter. The most common problems and their solutions are presented to help you operate your system successfully.

## Setting Up the System Electronics

#### WARNING

The PC power cord must be unplugged to prevent personal injury and damage to the electronics.

## Install the laser electronics board in the PC

#### CAUTION

The Agilent N1231B board contains components that may be damaged by electrostatic discharge (ESD). Do not handle the Agilent N1231B board or any of its components without taking adequate measures to prevent damage due to electrostatic discharge (ESD).

The Agilent N1231B PCI Three-Axis Board can be installed in any full-length PCI I/O backplane slot.

- 1 Unplug the PC power cord.
- 2 Remove the cover on the PC.

See the manual for your PC for specific instructions for this step and the next few steps.

- 3 Install the Agilent PC axis board in the PC.
- 4 Replace the PC cover.
- 5 Plug in the PC power cord, but leave the PC power off.

# Install the API library and monitor program on computers used for program development

#### To Install the N1231B API library

- 1 Exit from all applications.
- 2 Insert the CD in an appropriate drive.
- 3 Navigate to the directory: \N1231B API Development.
- 4 Run Setup.exe.
- 5 Follow the instructions on the screen.

When asked to choose a Setup Type, the default choice of Typical is recommended. Other choices are Compact and Custom. The setup types are described below:

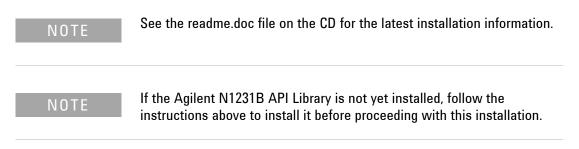
Typical installs all files.

Compact installs all files except those in the "User Files" directory.

Custom allows you to select the components to be installed.

- 6 If running under Windows NT and this is the first time the software has been installed, or if the software has been uninstalled prior to this installation, reboot the controller.
- 7 Perform the steps in the following subsection, "To Install the Agilent N1231B monitor program."

#### To Install the Agilent N1231B monitor program



- 1 Exit from all applications.
- 2 Insert the CD in an appropriate drive.
- 3 Navigate to the directory: \N1231B Monitor.
- 4 Run Setup.exe.
- 5 Follow the instructions on the screen.

#### **Connect the electronics cables**

- 1 Connect the largest connector on the laser head cable to the back of the laser head.
- 2 Connect the smallest connector on the laser head cable to the Reference connector<sup>\*</sup> on the Agilent N1231B PCI Three-Axis Board that you just installed in your PC.
- 3 Connect the Agilent 10884B Laser Power Supply to the remaining connector (the medium-size DIN connector) of the laser cable.
- 4 Connect the receiver cable to the back of the receiver and to one of the three MEASurement connectors\* in the Agilent N1231B PCI Three-Axis Board.

### Power up the laser head

1 Plug the Laser Power Supply into line power (nominally 110 V or 230 V ac) to start the laser.

All LEDs on the rear panel of the laser head should light except for the **READY** LED. The laser head should emit a red laser beam within 45 seconds after receiving power.

About halfway through the lock-up period, the **READY** LED blinks on and off to indicate that the laser is in the process of locking. When the head is ready for use, this LED remains on, indicating the laser has achieved lock and is generating a reference signal.

The laser head requires a period to stabilize the frequencies before a reliable measurement can be made. The length of the stabilization period depends on which model laser head is installed in the system.

#### WARNING

Do not stare directly into the beam (or its reflection from a polished surface) or this could result in eye damage.

2 Now, align the optics as described in the following section titled "Aligning the Optics."

<sup>\*</sup> To line up the connectors for the N1231B Ref and Meas cables, the red dot on the cable connector is to the right.

#### 2 Familiarization and Initial Operation

## **Aligning the Optics**

The laser head, optics, and receiver must be aligned so the laser beam from the optics returns to the receiver lens.

- 1 Set the laser head on a stable surface and point the beam in the direction you intend to move the optics.
- 2 Set the interferometer in the laser beam path so the beam enters the interferometer aperture perpendicular to the aperture. You may need to fasten the interferometer in place with a clamping fixture.
- 3 Set the reflector in the laser beam line coming from the interferometer. Adjust the reflector to reflect the beam back into the interferometer.
- 4 Place the receiver parallel to the laser beam from the laser head to the interferometer. The lens must be facing the interferometer. Fasten the receiver in place with a fixture or clamp.
- 5 Adjust the reflector and receiver to get the return beam on the receiver lens. When the **Laser Ready** indicator comes on, the green LED on the receiver will light when the beam alignment is satisfactory.
- 6 Block the beam from the interferometer to the receiver. The green LED on the receiver should go out. Unblock the beam and the green LED should light again. If this happens, the basic optics alignment is complete, and you can skip step 7 of this procedure.

If the receiver's green LED stays on when the beam from the interferometer is blocked, the receiver gain is too high. Go to the next step.

7 With the beam blocked, turn the receiver's gain adjustment control until the LED goes out. When the beam is unblocked, the LED should light again, indicating that the optics are aligned properly.

If the green LED does not light, readjust beam alignment until it does light.

## **Making Measurements**

NOTE	To make a measurement:
NOTE	a the electronics must be connected and on
	b the laser beam must be aligned
	c the software program must be running in the controller.

- 1 Turn on the power to the controller (PC).
- 2 Press the **Start** button, located at the bottom left of the task bar in the Start menu window as shown in Figure 2.
- 3 Select **Programs**, then select **Agilent N1231B API** from the pop-up menu.

The Agilent N1231B API pop-up menu is displayed as shown in Figure 2.

<ul> <li>Reflection Sessions</li> <li>Netscape SmartUpdate</li> </ul>				
📻 <u>P</u> rograms	•	🧓 Agilent N1231B API	Þ	N1231B Example
Documents	⊬	適 AvantGo	►	🖺 N1231B License
🌆 <u>S</u> ettings	⊬	🧓 Enhanced Keyboard Manager	►	🔆 N1231B Monitor
🔊 Eind	►	📵 HP Lock	►	🖺 N1231B Readme
🧼 <u>H</u> elp		画 InstallShield	÷	
🚰 <u>B</u> un		📴 IomegaWare	►	
🗊 Shut Down				-
🙀 Start				

Figure 2 Start/Programs pop-up menu

4 From the Agilent N1231B API pop-up menu, click on the **\* N1231B Monitor** icon to open the Monitor application.

With no input signals connected to the Agilent N1231B board, the Agilent N1231B Monitor screen should appear as shown in Figure 3.

#### NOTE

The PCI bus and slot number may differ from those shown in Figure 3.

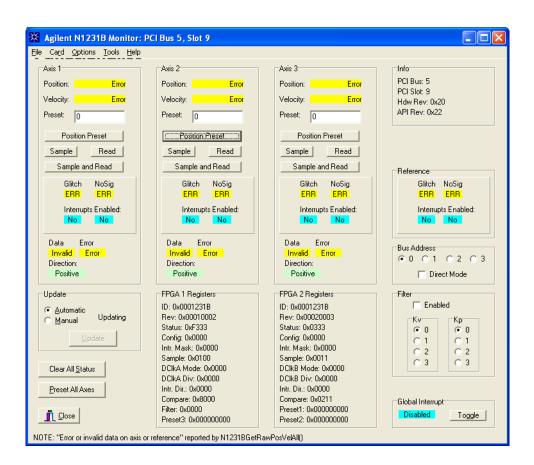


Figure 3 Monitor screen after opening the application

5 Press the **Clear All Status** button, and then the **Preset All Axes** button in the lower left of the screen.

The position in uncompensated raw lambda/2048 counts<sup>\*</sup> can now be read in the Position boxes corresponding to axes that have valid measurement signals as shown in Axis 2 in Figure 4.

<sup>\*</sup> These raw count values must be multiplied by 0.31nm/count and a compensation number (0.999728766 for standard air) to convert them into a measurement value.

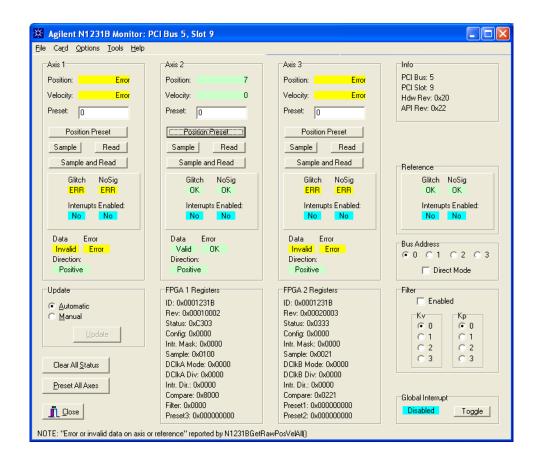


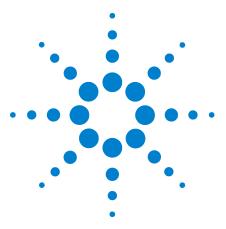
Figure 4 Measurement screen

To exit this application, click the Close button in the lower-left corner of the application's screen, or the close (X) button in the upper-right corner of the window.

## **Solving Problems**

Here is information about three simple problems that may occur while you are trying to make a measurement.

- If there is no red beam from the laser head:
  - Ensure that the laser head cable is securely connected to the back of the laser head.
  - Ensure that the power supply is connected to the laser head cable.
  - Ensure that the power supply is plugged into an operating outlet and that the **POWER ON** light is illuminated.
- If the green LED on the receiver does not light:
  - Ensure that there is a red beam from the laser head and the **Ready** LED is illuminated.
  - Ensure that the laser beam passes through the large aperture in the laser head.
  - Ensure the laser head's reference connector is connected to the electronics.
  - Ensure that the receiver cable is securely connected at the receiver and at the system electronics.
  - Ensure that the system electronics are connected to an operating power source and are turned on.
  - Ensure that the alignment of the laser head, optics, and receiver causes the beam from the interferometer to be centered on the receiver's lens.
  - Block the beam between the interferometer and measurement reflector. The reference-path beam should be centered on the receiver's lens. When you unblock the measurement-path beam, it should overlap the reference-path beam on the receiver lens.
  - If everything above seems correct, but the LED still doesn't light, adjust the receiver's gain control.
- If the controller does not indicate motion of the measurement reflector:
  - Ensure that there is a red beam from the laser head and the **Ready** LED is illuminated.
  - Ensure that the laser system electronics are powered.
  - Ensure that the laser beam is properly aligned and that the receiver's green LED is lighted.
  - If the receiver's green LED remains lighted when no measurement signal is present, reduce the receiver's gain via its gain control.
  - Ensure that the controller is on and the program is running.



Agilent Laser and Optics User's Manual Volume I

3

# System Design Considerations

Introduction, 38 Accuracy Considerations, 40 Determining What Equipment is Needed, 40 Electronic Components, 46 Adjustment Considerations, 48 System Grounding, 51 Laser Head, 52 Optics, 54 Beam Path Loss Computation, 59 Receivers, 64 Example Configurations, 65 Optical Device Troubleshooting, 75 Site Preparation, 76



## Introduction

Although there are many possible configurations of the laser and optics, all Agilent laser measurement systems have these basic parts in common:

- A laser source, to produce the two optical frequencies  $f_1$  and  $f_2$  and generate the reference signal. In discussions in this manual,  $f_1$  is the lower frequency and  $f_2$  is the higher.
- Beam-directing optics, to direct all or part of the laser beam to each measurement axis of the system, using right-angle bends.
- Measurement optics, to separate the two optical frequencies, direct them over the reference and measurement paths, and recombine them.
- One receiver per measurement axis, to detect the difference in optical frequencies and produce the measurement signal for that axis.
- Electronics to convert the measurement and reference signals into displacement data.

Two important characteristics of Agilent interferometers must be emphasized:

Only the change in relative position of the optics is detected.

Either optical component may move, as long as optical alignment is maintained. If the interferometer is fixed and the retroreflector is the moving component (toward or away from the interferometer), motion with respect to its original position is detected. Conversely, if the retroreflector is fixed, the interferometer can be the moving component.

Agilent laser position transducers can detect and measure all linear motions; that is, 3 degrees of the 18 degrees of freedom defined in the Glossary. Small angle measurements may be made by multiple measurements on the same axis.

The measurement system is relatively insensitive to all other motions, as briefly described below. See Figure 5.

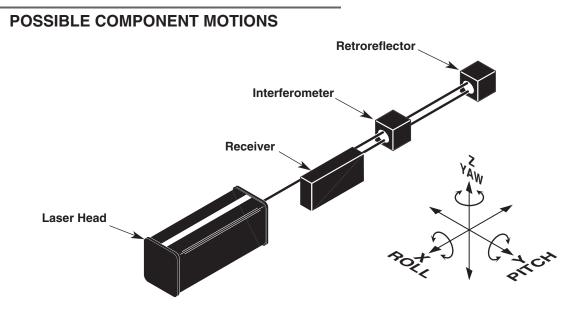


Figure 5 Possible component motions

- 1 Motion of the receiver or laser head along the beam path (X) has no effect on the measurement since both  $f_1$  and  $f_2$  would exhibit Doppler shift.
- 2 Small motions of the laser head, receiver, interferometer, or retroreflector in a direction perpendicular to the beam path (Y or Z) have no effect on the measurement. The only restriction is that sufficient light returns to the receiver.
- 3 Angular motion (pitch or yaw) of the laser head about the Z or Y axis has the effects described below:
- 4 It introduces a measurement error (cosine error).
- 5 It may displace the laser beam so that insufficient light returns to operate the receiver.
- 6 Although the laser head or the receiver may be rotated in 90° increments about the beam axis (roll), other roll deviations from the four optimum positions degrade the measurement signal. If either the laser head or receiver is rotated 45° about the beam axis, all position information will be lost because the receiver will not be able to distinguish between the two frequencies.
- 7 Angular motion of the receiver about the Y or Z axis has no effect on the measurement, within alignment limits specified for the receiver. (Receiver specifications are given in Chapter 35, Receivers," in Volume II of this manual.)
- 8 Angular motions of the interferometer and retroreflector depend on the particular components for limitations.

#### 3 System Design Considerations

## **Accuracy Considerations**

Several factors outside the laser measurement system can affect system accuracy. These factors (the measurement environment, machine and material temperature, and the optics installation) and their interrelationships must be understood in order to predict the performance of the system. Detailed descriptions and methods of compensation are given in Chapter 12, "Accuracy and Repeatability," of this manual.

Generally, Agilent laser measurement systems offer automatic compensation for air environments and also for temperature changes of the work material. For a temperature-controlled environment ( $20 \pm 0.5^{\circ}$  C), typical system accuracy using air sensor automatic compensation is 1.5 ppm. Using the Agilent 10717A Wavelength Tracker for compensation, the measurement repeatability is on the order of  $\pm 0.2$  ppm, depending on the environment.

### **Determining What Equipment is Needed**

First, sketch out your optical configuration. Remember:

- Each measurement axis (except for the Agilent 10717A Wavelength Tracker) requires an interferometer and associated retroreflector.
- Each measurement axis after the first one requires a beam splitter. The number of beam splitters required is n-1, where n is the number of measurement axes.
- If an Agilent 10717A Wavelength Tracker is used, it counts as a measurement axis.
- If a multiaxis interferometer, such as the Agilent 10721A, Agilent 10735A, Agilent 10736A, or Agilent 10737L,R is used, be sure the beam-directing optics you select will provide enough laser beam power to drive the receivers through the multiple measurement paths of the interferometer.
- Beam benders should be arranged so their exiting beams are perpendicular to one polarization plane of the incoming laser beam.
- Rotation of the beam during bending can result in problems due to the effects of polarization.
- Beam splitters should be arranged so:
  - one exiting beam is along the axis of the incoming beam, and the second beam is perpendicular to one polarization of the incoming beam, as described above for beam benders.
  - Each measurement axis requires an interferometer. The nature of the measurement(s) to be made influences the interferometer choice.

• Each measurement axis (including the Agilent 10717A Wavelength Tracker) requires a receiver. The interferometer used can influence the receiver choice. *Note that the Agilent 5519A and Agilent 5519B laser heads include a built-in receiver*.

Then, from your layout, determine your optics needs. Choose the Agilent laser head, optical and electronic components accordingly. Decide on a compensation scheme and, finally, select cables. Table 2 summarizes the equipment choices. For advice and help, contact Agilent Technologies.

Component	Comment(s)
Laser	One required per system
Agilent 5517A	Lowest velocity, largest size, 6 mm beam
Agilent 5517B/BL	25% higher velocity than Agilent 5517A, small size, 6 mm beam
Agilent 5517C Std 5517C-003 5517C-009	Higher velocity than Agilent 5517A and 5517B, small size 6 mm beam diameter 3 mm beam diameter 9 mm beam diameter
Agilent 5517D/DL	Higher velocity than Agilent 5517A/B/BL/C, small size, 6 mm beam
Agilent 5517FL Std 5517FL-009	Highest velocity, small size, 6 mm beam 6 mm beam diameter
Agilent 5519A	9 mm beam diameter Largest size, built-in receiver and power supply used in the Agilent 5529A Dynamic Calibrator System and Metrology applications.
Agilent 5519B	Largest size, built-in receiver and power supply, higher velocity than Agilent 5519A; used in the Agilent 5529A Dynamic Calibrator System and Metrology applications.
Beam-Directing Optics	Order as required to manipulate beam path to your configuration
Agilent 10567A	Dual-Beam Beam Splitter, useful in vacuum applications
Agilent 10700A	33% Beam Splitter
Agilent 10700B	4% Beam Splitter
Agilent 10700C	15% Beam Splitter
Agilent 10701A	50% Beam Splitter
Agilent 10707A	Beam Bender
Agilent 10725A	50% Beam Splitter, no housing
Agilent 10725B	4% Beam Splitter, no housing
Agilent 10725C	15% Beam Splitter, no housing
Agilent 10726A	Beam Bender, no housing
Agilent E1833C	15% Bare Beam Splitter
Agilent E1833E	33% Bare Beam Splitter

Table 2 Equipment choices

Component	Comment(s)	
Beam-Directing Optics (cont.)		
Agilent E1833G	50% Bare Beam Splitter	
Agilent E1833J	67% Bare Beam Splitter	
Agilent E1833M	100% Bare Beam Splitter	
Agilent N1203C	Precision Beam Translator	
Agilent N1204C	Precision Horizontal Beam Bender	
Agilent N1207C	Precision Vertical Beam Bender	
Agilent N1208C	33% Bare Beam Splitter	
Agilent N1208D	40% Bare Beam Splitter	
Agilent N1208E	50% Bare Beam Splitter	
Agilent N1208F	66% Bare Beam Splitter	
Agilent N1208G	60% Bare Beam Splitter	
Agilent N1209A	RPT RTP (Beam) Manipulator	
Measurement Optics	One Interferometer-plus-Reflector pair required per axis	
Agilent 10702A	Linear Interferometer	
Agilent 10702A-001	Same as above, but with wedge windows — required if interferometer is the moving component.	
Agilent 10703A	Reflector — paired with Agilent 10702A	
Agilent 10704A	Reflector — paired with Agilent 10705A	
Agilent 10705A	Single Beam Interferometer	
Agilent 10706A	Plane Mirror Interferometer	
Agilent 10706B	High Stability Plane Mirror Interferometer	
Agilent 10715A	Differential Interferometer	
Agilent 10715A-001	Differential Interferometer, turned configuration	
Agilent 10716A	High Resolution Interferometer	
Agilent 10716A-001	High Resolution Interferometer, turned configuration	
Agilent 10717A	Wavelength Tracker (requires measurement receiver and cable)	
Agilent 10719A	One-Axis Differential Interferometer, requires 3 mm beam from Agilent 5517C-003	
Measurement Optics (cont.)	One Interferometer-plus-Reflector pair required per axis	
Agilent 10721A	Two-Axis Differential Interferometer, requires 3 mm beam from Agilent 5517C-003	
Agilent 10724A	Plane Mirror Reflector	
Agilent 10735A	Three-Axis Interferometer	
Agilent 10736A	Three-Axis Interferometer	
Agilent 10736A-001	Three-Axis Interferometer with Beam Bender	

Table 2 Equipment choices (continued)

Component	Comment(s)
Measurement Optics (cont.)	One Interferometer-plus-Reflector pair required per axis
Agilent 10737L	Compact Three-Axis Interferometer, left
Agilent 10737R	Compact Three-Axis Interferometer, right
Agilent 10766A	Linear Interferometer
Agilent 10767A	Linear Retroreflector — paired with Agilent 10766A
Agilent 10767B	Lightweight Retroreflector
Agilent 10770A	Angular Interferometer
Agilent 10771A	Angular Retroreflector — paired with Agilent 10770A
Agilent 10774A	Short Range Straightness Optics (matched set)
Agilent 10775A	Long Range Straightness Optics (matched set)
Agilent E1826E	One-Axis Plane Mirror Interferometer (right)
Agilent E1826F	One-Axis Plane Mirror Interferometer (left)
Agilent E1826G	One-Axis Plane Mirror Interferometer (straight)
Agilent E1827A	Two-Axis Vertical Beam Interferometer
Agilent E1837A	Three-Axis Vertical Beam Interferometer
Agilent Z4399A	Three-Axis Interferometer
Agilent Z4420B	Five-Axis Interferometer
Agilent Z4421B	Five-Axis Interferometer
Agilent Z4422B	Three-Axis Interferometer
Optic Mounts	Adjustable mounts simplify installation and alignment
Agilent 10710B	Use with Agilent 10700A, 10701A, 10705A, 10707A
Agilent 10711A	Use with Agilent 10702A, 10706A, 10706B, 10715A, 10716A
Measurement Receivers	One required per axis; one required with Agilent 10717A Wavelength Tracker (if used)
Agilent 10780C	Receiver
Agilent 10780F	Remote Receiver
Agilent E1708A	Remote Dynamic Receiver
Agilent E1709A	Remote High-Performance Receiver
Receiver Cables for use with Agile	ent 10895A VME Axis board — one cable per system
Agilent 10790A	5 meters long
Agilent 10790B	10 meters long
Agilent 10790C	20 meters long

Table 2 Equipment choices (continued)

Component	Comment(s)
Receiver Cables for use with Ag — one cable per receiver	ilent 10885A or 10889B Axis boards or Agilent N1231A/B PCI Three-Axis Board
Agilent 10880A	5 meters long
Agilent 10880B	10 meters long
Agilent 10880C	20 meters long
	517A/B/BL/C/D/DL/FL Laser Head used with Agilent 10885A, 10889B, or is a DIN connector for connecting to the Agilent 10884B Power Supply to ) — one cable per system
Agilent 10881A	3 meters long
Agilent 10881B	7 meters long
Agilent 10881C	20 meters long
N1231A/B axis boards (cable ha head)— one cable per system	517A/B/BL/C/D/DL/FL Laser Head used with Agilent 10885A, 10889B, or s spade lugs for connection to a power supply to provide power to the laser
Agilent 10881D	3 meters long
Agilent 10881E	7 meters long
Agilent 10881F	20 meters long
	519A/B Laser Head used with Agilent 10887P Programmable PC Calibrator 02A system— one cable per system
Agilent 10882A	3 meters long
Agilent 10882B	7 meters long
Agilent 10882C	20 meters long
used with Agilent 10885A, 1088	517A/B/BL/C/D/DL/FL Laser Head, with no reference leg, and carry power only. 9B, or N1231A/B axis boards (cable has spade lugs for connection to a power aser head)— one cable per system
Agilent E1847A-060	3 meters long
Agilent E1847A-140	7 meters long
Agilent E1847A-200	10 meters long
Agilent E1847A-300	15 meters long
Agilent E1847A-400	20 meters long
Agilent E1848A-300	15 meters long
Agilent E1848B-060	3 meters long
Agilent E1848B-140	7 meters long
Agilent E1848B-200	10 meters long

#### Table 2 Equipment choices (continued)

Component	Comment(s)		
Laser Head Cables for Agilent 5517A/B/BL/C/D/DL/FL Laser Head, with no reference leg, and carry power only. used with Agilent 10885A, 10889B, or N1231A/B axis boards (cable has spade lugs for connection to a power supply to provide power to the laser head)— one cable per system (Cont.)			
Agilent E1848B-300	15 meters long		
Agilent E1848B-400	20 meters long		
Accessory Reflectors	Order as required for your application		
Agilent 10728A	Plane Mirror		
Agilent 10769A	Beam Steering Mirror		
Agilent 10772A	Turning Mirror		
Agilent 10773A	Flatness Mirror		
10898A VME Axis boards, an	d Cable for Agilent 5517B/C/D Laser Head used with the Agilent 10897C and d N1231A/B PCI Axis board (cable has a DIN connector for connecting to the y to provide power to the laser head) — one cable per system		
Agilent N1251B	7 meters (23.0 feet)		
High Performance Receiver Cables for use with Agilent 10897C and 10898A VME Axis boards, and N1231A/B PCI Axis board — one cable per receiver			
Agilent N1250A	5 meters (16.4 feet)		
Agilent N1250B	10 meters (32.8 feet)		

Table 2	Equipment choices	(continued)
---------	-------------------	-------------

## **Electronic Components**

### **Transducer Systems**

There are three different types of electronics for Agilent laser transducer systems. These electronics use different backplanes and have different performance and outputs. Full details are given in the appropriate electronics system manuals.

### **PC-Based Electronics**

The Agilent 10885A PC Axis Board and Agilent 10889B PC Servo-Axis Board are compatible with PC (ISA) backplanes.

Up to six Agilent 10885As may be used in a single system.

#### VME Compatible Electronics

The Agilent 10898A High Resolution VMEbus Dual Laser Axis Board, Agilent 10897C High Resolution VMEbus Laser Axis Board, and Agilent 10895A VMEbus Laser Axis Board are compatible with VME backplanes.

The Agilent 10896B VME Laser Compensation Board is also compatible with VME backplanes and works with the other Agilent VME Axis boards. Up to six Agilent 10895As and several Agilent 10896As (up to one for each Agilent 10895A) may be used in a single system.

#### **PC-Based PCI Electronics**

The Agilent N1231A PCI Three-Axis Board is optimized for connection to a PMAC motion control system from Delta Tau<sup>®</sup>. It is a full size, Universal (3.3V and 5.0V signaling compatibility), 32-bit, 33 MHz, PCI Rev. 2.2 compliant card for use in PC-compatible controllers as part of an Agilent laser interferometry position measurement system. The Agilent N1231B PCI Three-Axis Board with external sample has a generalized hardware interface and twice the resolution of the Agilent N1231A PCI Three-Axis Board.

#### **Calibrator System Electronics**

#### Agilent 5529A/55292A Dynamic Calibrator

The Agilent 5529A/55292A Dynamic Calibrator is a laser system used to ensure the accuracy of a machine's motion and positioning. Controlled through your PC (with Microsoft® Windows installed), the system is able to collect and analyze measurement data for a number of measurements. The Agilent 5529A/55292A Dynamic Calibrator typically includes the following electronic components:

- Agilent 5519A/B Laser Head
- Agilent 10886A PC Compensation board (optional, for automatic compensation)
- Agilent 10887B PC Calibrator Board
- Agilent 10751C/D Air sensor and Agilent 10757D/E/F Material Temperature sensor(s) (optional, as required)
- Agilent 10888A Remote Control units (optional)
- Agilent 55292A USB Expansion Module (optional, to house the PCI-ISA bus 10886A and 10887B boards and provide USB connectivity to them.)

The PC compensation boards provide the interfaces between the air and material temperature sensors and your PC. The boards convert the analog electrical voltages from the sensors to digital forms that the PC uses to calculate the compensation factors. These factors adjust for changes in the systems' operating environments. Typical sensors used with each Agilent 10886A PC Compensation board are the Agilent 10751C,D Air Sensor and one to three Agilent 10757D,E,F Material Temperature sensors.

The Agilent 10887B PC Calibrator Board enable the PC to perform laser calibrator-related functions with the Agilent 5529A calibrator software.

An Agilent Two-Axis 5529A/5529A Dynamic Calibrator and an Agilent 55292A USB Expansion Module are also available. The USB software hosts up to five axes on one computer.

## **Adjustment Considerations**

In general, when aligning the Agilent optics, it will be necessary to adjust most or all of the optical components. Most optics are not referenced to their housings since simple adjustments by the user can usually provide optimum alignment. The Agilent 10710B and Agilent 10711A Adjustable Mounts should be used to provide the adjustment capability for most optical components.

For systems having many measurement axes, using the Agilent N1209A RPT beam maniplulator may pay for itself by reducing the time spent aligning the system. See Chapter 17, "Beam-Directing Optics" in Volume II for details on the Agilent N1209A RPT.

There are a few exceptions, however. Certain optics designed for multiaxis systems provide referenced housings. Installation and alignment of these optics depends on the optic; refer to specific instructions for these optics (Agilent 10719A, Agilent 10721A, Agilent 10735A, Agilent 10736A) elsewhere in this manual.

Other optics require you to fabricate your own mounts.

In general, the alignment procedures are performed with all optical components in place. Your measurement system design should allow for adjustment of the laser, optics, and receivers during alignment.

#### Laser beam and optics protection

The laser measurement system requires protection against unintentional laser beam blockage and air turbulence problems. In some applications, such as machine tools, protection should be provided to prevent metal chips or cutting fluid from interfering with the measurements. Also, the optical components usually require protection to prevent contamination of the optical surfaces by oil or cutting fluid. In applications which are considered "clean", protection may not be needed.

If protection of the laser beam and optical components is required, there are two general types: moving-component protection and stationary component protection.

In many applications, the only moving component is the interferometer or the reflector. Many of the beam benders are stationary and only direct the laser beam to the measurement axis. In these cases, it is only necessary to provide fixed tubing for the laser beam and some type of sealed enclosure for the optics. Since only one laser beam of approximately 6 mm (0.24 inch) in diameter is involved, relatively small diameter tubing can be used. Since either the interferometer or the reflector is moving during the measurement,

protecting the laser beam and the moving components requires a telescoping cover or a cover that is self-sealing. A wide variety of commercially available protective covers are suitable for this purpose.

Figure 6 illustrates techniques for protecting the laser beam and optical components with different types of protective covering. Note that the cover for the retroreflector allows the retroreflector to be moved very close to the interferometer. This helps minimize the deadpath errors. Chapter 12, "Accuracy and Repeatability," in this manual has more details on minimizing deadpath

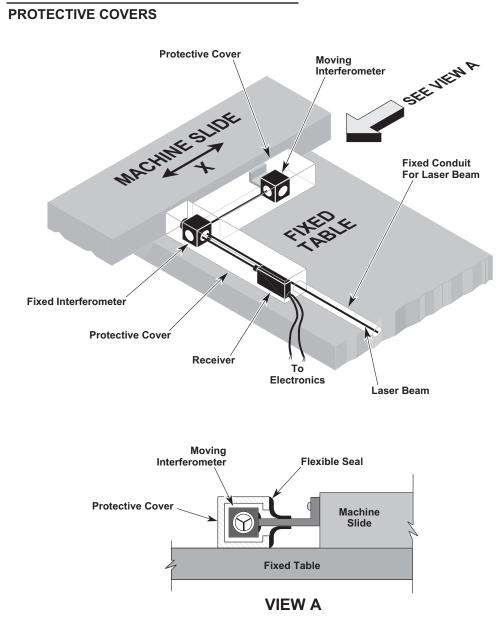


Figure 6 Protective covers for optics and laser beam

Figure 7 shows a different type of protective cover. Again, the mechanical arrangement allows the retroreflector to be close to the interferometer at the closest point of travel, even though the telescoping cover is not entirely collapsible. Another type of protective cover is the flexible bellows. This is generally used for short travel distances.

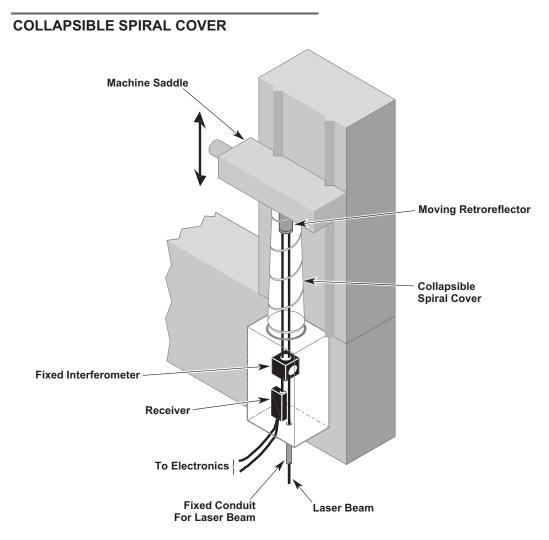


Figure 7 Collapsible spiral cover for movable retroreflector

## **System Grounding**

Be sure to consider electrical grounding requirements as you plan and install your Agilent laser measurement. Grounding is important for safety reasons, but your grounding arrangement can also affect your laser system's performance.

Best practice requires that all system components that are connected to electrical ground should be connected to ground at a common point, not at separate points. Your electrical ground connections should radiate from a single point. Using more than one grounding point could create a ground loop, which could introduce an unacceptable level of electrical noise into the electronics.

Signal grounds on each Agilent laser head, each Agilent receiver and the Agilent laser measurement system electronics are all connected to their respective chassis. To prevent ground loops they all should be grounded through one common point.

The Agilent 10780C or Agilent 10780F receiver mounting is isolated from ground by using the nylon screws supplied.

A system using VME electronics (Agilent 10898A, Agilent 10897C, and Agilent 10895A axis boards), PC electronics (Agilent 10885A and Agilent 10889B axis boards) or PCI electronics (N1231A/B axis board) should be grounded through the electronics power line.

### **Laser Head**

### Orientation

An Agilent laser head may be mounted in any orientation as long as it is positioned to direct the beam into the optical system parallel to or orthogonal with the machine axes being measured. See Chapter 16, Laser Heads," in Volume II of this manual for more information about laser head orientation.

### Mounting plane tolerance

The plane defined by the three mounting feet on the laser head must be parallel to either the bottom or sides of the beam-splitters and of the beam-bender housings to within  $\pm 3^{\circ}$ , and to the bottom or sides interferometers to within  $\pm 11^{\circ}$ . This ensures that the polarization axes of the interferometers are oriented properly relative to the polarization vectors of the laser beam (Figure 8). The laser head can be rotated in 90° increments about the beam axis (roll) without affecting the system performance, but the measurement direction sense will change with each 90° rotation.

Allow 50 mm (2 inches) clearance around the laser head for easy servicing. Allow at least 100 mm (4 inches) clearance at the back of the laser head for cable connections.

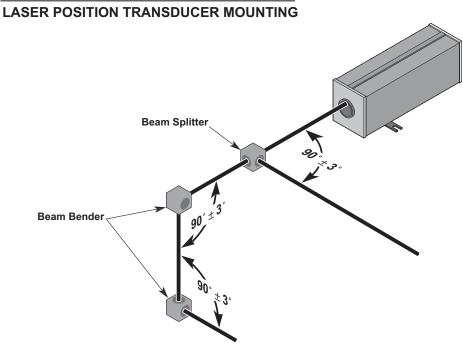


Figure 8 Laser position transducer mounting

#### **Pointing stability**

To maintain good pointing stability, it is good practice to use kinematic mounting principles. Refer to Chapter 16, Laser Heads," in Volume II of this manual for more information about laser head pointing stability.

### **Thermal isolation**

Because there is some heat dissipation from the laser heads, you should choose the mounting method and location with care. Where possible, mount the laser head away from the measuring area, to avoid any thermal effects.

#### Vibration isolation

Since the system measures only the relative motion between the interferometer and reflector, measurements are not affected by vibration along the beam axis of the laser source or the receiver.

When vibration of the laser head causes displacement of the beam (perpendicular to beam axis) at an interferometer or receiver, the beam signal power can fluctuate. If this fluctuation is too great, insufficient beam signal will arrive at the receiver, causing a "measurement signal error."

#### **Magnetic shielding**

Agilent laser heads contain a permanent magnet. When installing an Agilent laser measurement system in an application sensitive to magnetic fields, shielding around the laser head may be required.

### Mounting

See Chapter 16, Laser Heads," in Volume II of this manual for laser head installation and mounting instructions.

The laser source in Agilent 5517C-009 9-mm Laser Head is referenced to locations on the outside of the laser head, allowing the laser head to be installed in a predefined mounting location, minimizing the need for laser head alignment. A diagram of the mounting location for this laser head is presented in Figure 20.

## **Optics**

### Plane of orientation with respect to laser head

The mounting plane tolerance of the optics to the laser head is the same as discussed in the paragraph titled "Mounting plane tolerance," above. That is, the bottom or sides of the interferometers should be parallel to within  $\pm 1^{\circ}$  of the plane defined by the laser head's three mounting feet.

#### Effect of optics on measurement direction sense

The orientation and configuration of the interferometers affects the measurement direction sense. The direction sense depends on which frequency is in the measurement path of the interferometer. For example, if  $f_1$  (lower frequency) is in the measurement path and  $f_2$  (higher frequency) is in the reference path and the optics are moving away from each other, the fringe counts will be INCREASING. This corresponds to using an Agilent 5517A, Agilent 5517B, or Agilent 5517C Laser Head (mounting feet in horizontal plane) with an Agilent 10702A Linear Interferometer mounted with labels facing up and down (see Figure 9). Interchanging  $f_1$  and  $f_2$  (e.g., rotating interferometer 90°) in this example will result in the fringe counts DECREASING.

The optical schematics for the interferometers, in Chapter 5, "Measurement Optics (General Information)," show which frequency polarizations are in the measurement path.

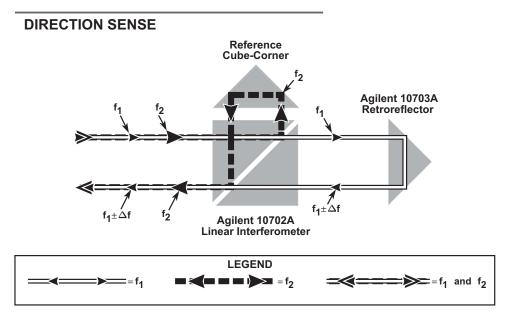


Figure 9 Direction sense - fringe counts increase as optics move apart

As with the laser heads, when the interferometers are rotated 90°, the measurement direction sense will change. This rotation causes switching of frequencies in the measurement path.

#### **Configuration effects**

Many of the distance-measuring interferometers can be configured to turn the beam at right angles. When configuring the linear, single-beam, and plane mirror interferometers to turn the beam, the measurement direction sense will be changed. This is because the measurement and reference paths are switched on the interferometers, therefore changing the direction sense. For more information, see the Chapter 5, "Measurement Optics (General Information)," in this manual.

#### Vibration isolation for optics

Vibration of the optics along the beam can cause the fringe count in the laser measurement system electronics to fluctuate rapidly. Vibrations along this axis constitute real, measurable, displacements; you will have to decide if these fluctuating measurements are acceptable in your application. In extreme cases, however, the velocity of the optics may momentarily exceed the velocity limitation of the laser system, causing an error.

When vibration occurs perpendicular to the beam, the beam signal power can fluctuate. If this fluctuation is too great, insufficient beam signal will arrive at the receivers, causing a "measurement signal error".

Loose mounting can cause the optics to move inappropriately during a measurement, causing a measurement error or loss of beam power.

Elastic mounting can have the same effect as loose mounting. It can also be responsible for a "sag" offset in the optics' positions. If there is vibration in the machine, an elastic mounting can transmit and amplify the vibration to the attached optic, possibly causing more errors. You should anticipate these effects and minimize them, if necessary, during the laser measurement system design process.

Certain interferometers are inherently less susceptible to vibration effects than others. This is particularly true of differential-style interferometers such as the Agilent 10715A, Agilent 10719A, and Agilent 10721A. The stability of these interferometers is due to the fact that both their reference beams and their measurement beams travel to external mirrors. Any motion of the interferometer itself that is common to both beams will not appear as a measurement. Of course, any vibration between the reference and measurement mirrors will constitute real, measurable, displacements.

### Adjustable mounts for optics

The optical elements inside several of the Agilent laser measurement system optics are not precisely referenced to their housings. In most applications involving these optics, a few simple alignments during system installation can usually provide equal or better alignment than referencing the optics to their housings. Therefore, slight positioning adjustments of the unreferenced interferometers, beam splitters, and beam benders are needed for proper system alignment.

Positioning adjustments for most optics can be provided by using Agilent 10710B or Agilent 10711A Adjustable Mounts, as appropriate. These mounts allow adjustment of pitch and yaw of any attached optic. (Roll adjustment is typically not required, and can usually be avoided by careful optical system layout.)

For a listing of which Adjustable Mount supports which optic, see the Chapter 36, Accessories," in Volume II of this manual.

In some applications, referenced housings can provide significant advantages. For example, the alignment requirements for certain multiaxis applications can be difficult or impossible to achieve without referenced housings. In those cases, interferometers such as the Agilent 10719A, Agilent 10721A, Agilent 10735A, Agilent 10736A, and all of the NGI optics should be considered. These products have referenced housings and prealigned optical elements. Because they have individual mounting requirements, these products are not intended for use with the adjustable mounts described above. For more information about these optics, refer to Chapter 5, "Measurement Optics (General Information)," and Chapter 6, "NGI Measurement Optics (General Information) in this manual.

### **Fasteners for optics**

Any optical component that fits an adjustable mount is supplied with mounting screws to mount it on the appropriate adjustable mount.

### **Vacuum applications**

There are vacuum options for Agilent optical components, which are compatible with vacuum environments. Contact Agilent Call Center for information (telephone numbers of various call centers are listed on the "Service and Support" page at the back of this manual). The housings of these components are made of stainless steel and the optical elements are attached to these housings using a low volatility (space grade) adhesive. See the "Specifications" information for each optic for a list of materials used in the optic. If the laser beam has to go through a window (for example into a vacuum chamber) the window must meet the following requirements:

- 1 A minimum window aperture of 25.4 mm (1 inch) with a minimum thickness of 8 mm (0.3 inch). If a larger window is used, it must be proportionally thicker to assure no distortion in the window when under differential pressures.
- 2 Transmitted wavefront distortion less than  $\lambda$  /10 (peak-valley, single-pass) over a 23 mm (0.9 inch) diameter.
- 3 Parallelism of faces less than ±2 arc-minutes, to reduce beam steering.
- 4 Surface quality 60-40 or better, per Mil-0-13830.
- 5 The window must be strain-free.

#### Differential measurements with interferometers

Several interferometers have the capability to make differential measurements. A differential measurement is one in which both the reference beam and the measurement beam travel to external mirrors outside the interferometer housing. This allows measurement of the relative positions of the two external mirrors, either or both of which may be moving. Viewed another way, this allows measuring the motion of one reflector relative to a reference datum elsewhere in the machine, external to the interferometer itself. This is unlike the typical interferometer configuration because usually the reference beam path length does not change; in differential configurations, it can.

One useful example of a differential measurement in a lithography application is for measuring the motion of the X-Y stage relative to the optical column. The Agilent 10719A One-Axis Differential Interferometer (shown in Figure 170 of Chapter 25 in Volume II) and the Agilent 10721A Two-Axis Differential Interferometer (shown in Figure 178 in Chapter 26) are ideally suited to this type of measurement, because they provide parallel reference and measurement paths which are offset vertically by 19 mm (0.750 inch). For such an application, a user-supplied reference plane mirror is required in addition to the measurement reflector on the X-Y stage.

The Agilent 10715A interferometer (shown in Figure 140 in Chapter 22 of Volume II) also permits differential measurements between two plane mirrors. However, instead of having an offset spacing as in the Agilent 10719A or Agilent 10721A, the Agilent 10715A permits the reference beams and the measurement beams to be aligned essentially coaxially. A specially-shaped reference plane mirror is supplied with the Agilent 10715A.

Customized differential configurations are possible with several other interferometers. However, considerable care should be exercised during design and layout to avoid introduction of alignment errors, thermal or mechanical instabilities, and potential deadpath problems. When making differential measurements, both reflectors (reference and measurement) should be of the same type (cube corner or plane mirror); this minimizes thermal drift problems with ambient temperature changes.

To use the Agilent 10702A, Agilent 10705A, or Agilent 10766A in a differential configuration, the reference cube corner can simply be detached from the interferometer housing and attached to the reference surface of interest. This is shown in Figure 106 in Chapter 18 of Volume II. Be aware that all installation and alignment requirements for the measurement reflector now apply also to the reference reflector.

To use the Agilent 10706A or Agilent 10706B interferometer in a differential configuration, a plane mirror is recommended as the reference reflector. Simply replace the reference cube corner (or high-stability adapter) with the Agilent 10722A Plane Mirror Converter and attach the reference plane mirror to the reference surface of interest. This is shown in Figure 122 in Chapter 20 of Volume II. Again, install and align the reference reflector the same as you would the measurement reflector.

#### Moving interferometer instead of reflector

When moving the interferometer instead of the measurement reflector is required, the Agilent 10702A-001 (or Agilent 10766A) should be used. In practice, for alignment reasons, these are the only interferometers (except the straightness interferometers) that can be moved while making measurements. For a detailed explanation of why this option is required, see Figure 101 in Chapter 18 of Volume II.

#### Introducing an offset into the laser beam

There may be an occasion when you will want to simply introduce an offset into your laser beam, to get it from the laser head to the interferometer without having to relocate either one of them. Figure 10 shows two ways in which this can be done.

To simply translate the beam, you can use two reflectors (such as the Agilent 10726A Beam Bender) as a "periscope", as shown in Figure 10(A). Changing the spacing between the reflectors, or rotating the device can change the amount of offset.

To reverse the direction of the beam, you can use two reflectors in a "retroreflector" arrangement as shown in Figure 10(B).

### **Beam Path Loss Computation**

Multiaxis positioning systems must be designed to allow sufficient optical power to reach each Agilent 10780C, Agilent 10780F, Agilent E1708A, or Agilent E1709A Receiver in the system.

Since all optics have an efficiency of less than 100%, an optical power loss budget must be created as a part of any multiaxis system design. This chapter defines optical efficiency as it relates to the signal loss through components. A method for computing the optical power loss in a system is described.

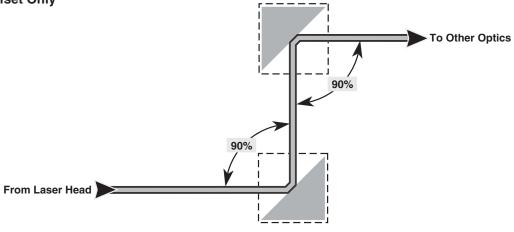
#### Considerations

The following considerations are important in designing a reliable multiaxis measuring system:

- When using the Agilent 10780C/F or Agilent E1708A receivers, typically up to four measurement axes can be easily implemented without optical power loss imposing significant constraints. A system of five or six axes is usually feasible, although closer attention to the power loss budget is required. A system having more than six axes is possible under certain circumstances (with PC- or VME-based electronics), but the optical power loss budget quickly becomes the limiting constraint. The Agilent E1709A receiver was designed for systems that have more than six measurement axes.
- Minimum laser output power is 120 microwatts for the laser heads. The typical laser output power is about 400 microwatts. The output power is relatively constant over the life of the tube, and tends to drop off immediately at the end.
- Higher laser output power is available upon request.

#### **INTRODUCING AN OFFSET**

#### A: Offset Only



#### **B: Offset Plus Direction Change**

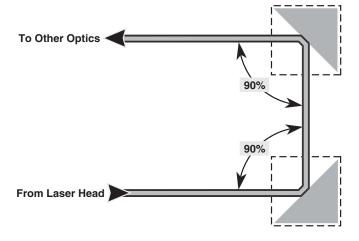


Figure 10 Introducing an offset into the laser beam

• Minimum required power at the Agilent 10780C Receiver is 1.5 microwatts. The Agilent 10780F Remote Receiver and Agilent E1708A Remote Dynamic Receiver require 2.2 microwatts with its standard 2-meter fiber-optic cable (more with longer cables). The Agilent E1709A Remote High-Performance Receiver requires a minimum of 0.20 to 0.80 microwatts, depending on the AC/DC ratio, with standard 2-meter plastic fiber-optic cable. (Adjustment of the receiver's gain is required to obtain this sensitivity. See the alignment and gain adjustment procedures in Chapter 35, Receivers," in Volume II of this manual.)

- The beam splitters have "worst-case" as well as "typical" transmission and reflection specifications. Refer to the paragraphs titled "Axis component efficiencies (worst case)" and "Axis component efficiencies (typical)" on the following pages, for these specifications.
- In addition, all optics have small reflection and absorption losses that occur at each internal interface or component, which is taken into account in their efficiency value.
- Fingerprints, dirt, or oil on a glass surface significantly reduce optical efficiency by increasing both reflection and absorption losses.
- System misalignment also reduces the amount of light reaching the receiver.
- Thermal gradients in the beam path can bend the beam and distort the wave front, both of which reduce optical signal strength at the receiver.

### **Calculation of signal loss**

In order to assess the signal loss in a measurement system, each optical component has been characterized by both worst case and typical optical efficiencies. These efficiency values for each optical component are listed in the "Specifications" section for each optic (that is, the specifications section in Chapter 17, Beam-Directing Optics," for beam splitters and chapters 18 through 34 in Volume II of this manual for interferometers.)

Optical efficiency is defined as:

Efficiency = Optical Power Out Optical Power In

The optical efficiencies for the interferometers are given with the respective measurement reflector efficiency included. For example, the Agilent 10702A Linear Interferometer efficiency includes the efficiency of the Agilent 10703A Retroreflector.

The combined optical efficiency of a given measurement axis is the product of the efficiencies of the individual optics in the beam path. This combined efficiency times the minimum laser output power in microwatts yields the worst case optical power at the receiver. This value must be at least 1.5 microwatts for the Agilent 10780C Receiver, or 2.2 microwatts for the Agilent 10780F Remote Receiver and Agilent E1708A Remote Dynamic Receiver, or 0.20 to 0.80 microwatts for Agilent E1709A Remote High-Performance Receiver. A beam power safety factor of at least three is recommended even though worst case laser and optics are assumed. Creating a system with five or more axes of measurement may result in a beam power safety factor that is less than three.

As an example, consider a typical installation with two measurement axes and a Wavelength Tracker axis (Figure 165 in Chapter 24 of Volume II). Assume differential interferometers, good optical alignment, 98% efficient plane mirrors (on the stage), comparable path lengths, and use of any Agilent laser head.

The three axes - X, Y, and Wavelength Tracker (WT) - have the components listed in the following table.

Axis	Component	Component Efficiencies (Worst Case)
Х	Agilent 10700A (67% path)	61%
Х	Agilent 10701A	39%
х	Agilent 10715A	25%
Y	Agilent 10700A (67% path)	61%
Y	Agilent 10701A	39%
Y	Agilent 10715A	25%
W	Agilent 10700A (33% path)	27%
W	Agilent 10707A	98%
W	Agilent 10717A	25%

#### Axis component efficiencies (worst case)

Assuming a minimum laser power of 120 microwatts, you can calculate the worst-case power at the X, Y, and Wavelength Tracker receivers by multiplying the product of component efficiencies by the laser output power:

Power at X =  $0.61 \times 0.39 \times 0.25 \times 120 = 7.1$ 

Power at Y =  $0.61 \times 0.39 \times 0.25 \times 120 = 7.1$ 

Power at WT =  $0.27 \times 0.98 \times 0.25 \times 120 = 7.9$ 

This system has a power safety factor of 4.7 at worst case (based on use of the Agilent 10780C Receiver, which requires 1.5 microwatts) for each axis resulting in reliable operation and easy alignment.

You can also calculate this safety factor using the typical optical efficiency values, listed in the following table.

Axis	Component	Component Efficiencies (Typical)
Х	Agilent 10700A (67% path)	63%
Х	Agilent 10701A	45%
Х	Agilent 10715A	36%
Y	Agilent 10700A (67% path)	63%
Y	Agilent 10701A	45%
Y	Agilent 10715A	36%
W	Agilent 10700A (33% path)	30%
W	Agilent 10707A	99%
W	Agilent 10717A	36%

#### Axis component efficiencies (typical)

Using the typical laser power of 400 microwatts, you can calculate the typical power at the X, Y, and Wavelength Tracker receivers by multiplying the product of each component efficiency by the laser output power for each axis.

Power at X =  $0.63 \times 0.45 \times 0.36 \times 400 = 40.8$ 

Power at Y =  $0.63 \times 0.45 \times 0.36 \times 400 = 40.8$ 

Power at WT =  $0.30 \times 0.99 \times 0.36 \times 400 = 42.8$ 

By using the typical efficiencies of the component, a safety factor greater than 28 is achieved (based on use of the Agilent 10780C Receiver, which requires 1.5 microwatts). The Agilent 10780F (2.2 microwatts), Agilent E1708A (2.2 microwatts), and Agilent E1709A (0.20 to 0.80 microwatts) receivers are more sensitive. Hence, can operate with more axes.

## Receivers

### General

When determining the receiver mounting locations and positions, keep the following points in mind:

- 1 At a  $45^{\circ}$  position (roll), the signal will go to zero.
- 2 The receiver typically dissipates 2.0 Watts, with a maximum dissipation of 2.7 Watts. Plastic pads keep an air gap around the receiver and act as thermal and electrical isolators.

CAUTION

Use nylon screws only (Agilent 2360-0369). The receiver housing must be electrically isolated from the mounting fixture.

- 1 The remote sensor in the Agilent 10780F Remote Receiver, Agilent E1708A Remote Dynamic Receiver, and Agilent E1709A Remoter High-Performance Receiver does not dissipate any power. The remote sensor does not require a nylon screw.
- 2 Allow a 5 cm space at the rear of each receiver housing for each cable connection.
- 3 The fiber-optic sensor head of the Agilent 10780F, E1708A, and E1709A receivers may be mounted directly to certain interferometers (Agilent 10719A, Agilent 10721A, Agilent 10735A, Agilent 10736A, Agilent 10737L, R) or directly to optional adapter plates (Option 080) available for the Agilent 10702A, Agilent 10705A, and Agilent 10706A/B interferometers. Alignment pins are provided for easy installation and alignment. This eliminates the need for any other user-supplied mount for the sensor head.
- 4 Maintain a bend radius not less than 35 mm (1.4 inches) to prevent signal attenuation in the receiver's fiber optic cable.

### **Clearance for laser beam**

Figure 263 in Chapter 35 in Volume II of this manual shows the Agilent 10780C and Agilent 10780F receivers and the proper beam spacing.

### Alignment adjustment required

The Agilent 10780C, Agilent 10780F, Agilent E1708A, or Agilent E1709A receiver requires an alignment relative to the input beam to maximize measurement signal strength. See the alignment and gain adjustment procedures in Chapter 35, "Receivers," of this manual.

### **Example Configurations**

#### Single-axis system for servo-track writing

Figure 11 shows a single-axis system to control servo-track writing. This system uses one each of:

- Agilent 5517A, 5517B, or 5517C Laser Head
- · laser head cable
  - Use an Agilent N1251B High Performance Laser Head Cable to connect to Agilent 10898A VME electronics board or Agilent N1231A/B PCI electronics boards.
  - Use an Agilent 10881A/B/C Laser Head Cable to connect to Agilent 10885A or Agilent 10889B PC-compatible electronics boards.
  - Use an Agilent 10891A/B/C Laser Head Cable to connect to Agilent 10895A VME electronics boards.
- Agilent 10705A Single Beam Interferometer
- Agilent 10704A Reflector
- Agilent 10780C Receiver
- Receiver cable
  - Use an Agilent N1250A/B Receiver Cable to connect to Agilent N1231A/B PCI electronics boards, Agilent 10897C VME electronics board, or Agilent 10898A VME electronics board.
  - Use an Agilent 10880A/B/C Receiver Cable to connect to Agilent 10885A or Agilent 10889B PC-compatible electronics boards.
  - Use an Agilent 10790A/B/C Receiver Cable to connect to Agilent 10895A VME electronics boards..
- Agilent laser axis of measurement electronics (Agilent 10885A, 10889B, 10897C, 10898A, or N1231A/B)

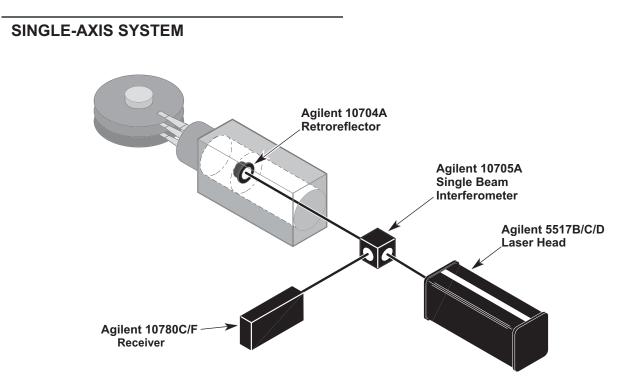


Figure 11 Single-axis system for servo-track writing

### **Multiaxis configurations**

The maximum number of independent axes of displacement that can be measured using one laser head depends on: 1) the measurement system electronics, 2) the strength of the beam from the laser head, and 3) the sensitivity of the receivers used.

By using the proper combination of beam splitters, beam benders, and interferometers, the measurement axes can be established with a minimum number of components. The following paragraphs provide examples of routing the laser beam for multiaxis measurement configurations.

## Multiaxis system for a precision x-y stage

Figure 12 shows a multiaxis system for a precision X-Y stage. This system uses:

- one Agilent 5517C Laser Head
- one laser head cable
  - Use an Agilent N1251A/B High Performance Laser Head Cable to connect to Agilent 10895A, Agilent 10897C, or Agilent 10898A VME electronic boards.
  - Use an Agilent 10881A/B/C Laser Head Cable to connect to Agilent 10885A, Agilent 10889B, or Agilent N1231A/B PC-compatible electronics.

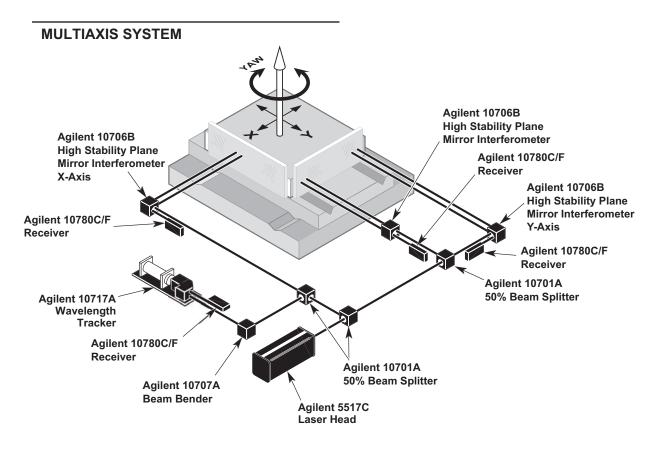


Figure 12 Multiaxis system for a precision x-y stage

- three Agilent 10701A 50% Beam splitters
- three Agilent 10706B High Stability Plane Mirror interferometers
- one Agilent 10707A Beam Bender
- one Agilent 10717A Wavelength Tracker

- four Agilent 10780F Remote receivers
- four receiver cables
  - Use Agilent 10790A/B/C Receiver cables to connect to Agilent 10895A VME electronics boards.
  - Use either the Agilent 10880A/B/C or the N1250A/B (high performance) Receiver cables to connect to Agilent 10885A, 10889B, or N1231A/B PC-compatible electronics boards or Agilent 10897C or Agilent 10898A VME electronics boards.
- four Agilent 10710B Optics mounts
- three Agilent 10711A Optics mounts
- three Agilent laser axis of measurement electronics (Agilent 10885A, Agilent 10889B, Agilent 10895A, Agilent 10897C, Agilent 10898A, or Agilent N1231A/B)

#### NOTE

The Agilent 10751A/A/B and Agilent 10757A/B/C sensors cannot be used with the Agilent 10886A PC-compatible electronics board, because the Agilent 10885A has different connectors. Use the Agilent 10751C/D and Agilent 10757D/E/F sensors instead.

• one Agilent Automatic Compensation Board

#### Four-axis linear configuration

Figure 13 shows a four-axis measurement configuration with all components aligned in one plane. Note that any of the components (beam benders, beam splitters, or interferometers) could be rotated in 90° increments to provide a three-dimensional configuration. Since interferometers can also bend the laser beam through 90°, the number of components can be minimized.

#### NOTE

In an application where the Agilent 10702A Linear Interferometer is the moving component and the Agilent 10703A Retroreflector is the fixed reference, the Agilent 10702A Linear Interferometer-001 must be used to eliminate alignment errors. If a right-angle beam bend is made through the Agilent 10702A, it must be the fixed component. When the Agilent 10705A Single Beam Interferometer is used, it must be the fixed component.

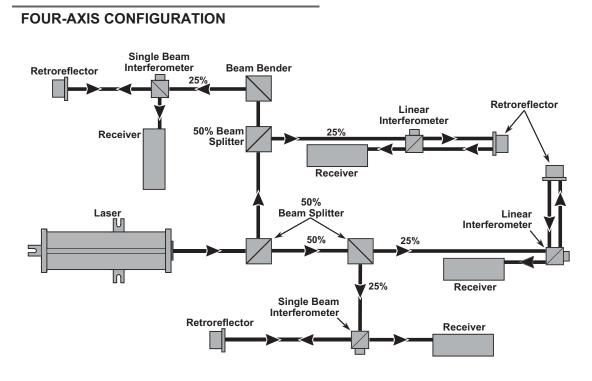


Figure 13 Four-axis configuration

#### Two-axis plane mirror

Figure 14 shows an X-Y stage measurement configuration using the Agilent 10706B High Stability Plane Mirror Interferometer. The X-Y stage has plane mirrors mounted at 90° to each other; these are the reflectors for the plane mirror interferometers. The advantages of this configuration are discussed in Chapter 12, "Accuracy and Repeatability," of this manual. The Agilent 10706A Plane Mirror Interferometer is used to bend the laser beam.

#### Two-axis plane mirror in a vacuum

In an application where the X-Y stage is installed in a vacuum chamber, the configuration in Figure 14 may not be suitable. Figure 15 shows a configuration using the Agilent 10567A Dual Beam Beam-Splitter which allows the laser beam to enter and exit the chamber through one window. This allows the receivers to remain outside the chamber and leaves only the optics inside. For window specifications, refer to the "Vacuum applications" on page 56. If the Agilent 10567A is not used, two windows (and possibly additional beam splitters and benders) will be required.

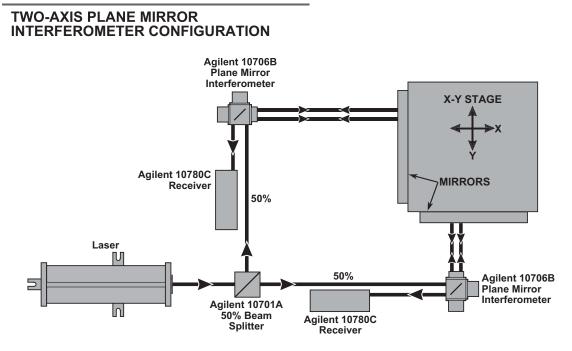


Figure 14 Two-axis plane mirror interferometer configuration

#### X-Y STAGE INSTALLED IN A VACUUM CHAMBER

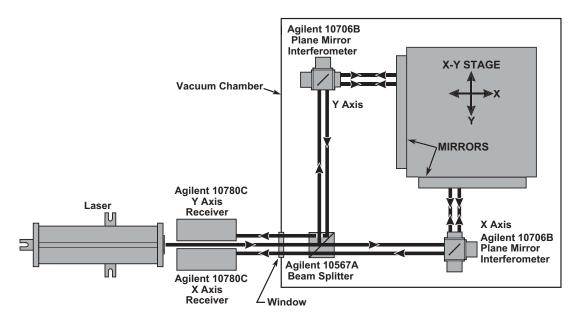


Figure 15 X-Y stage installed in a vacuum chamber

# Two-axis measurement system using two Agilent 10715A differential interferometers

In X-Y stage applications where maximum measurement accuracy and stability are required, the Agilent 10715A Differential Interferometer can be used instead of the Agilent 10706A/B Plane Mirror Interferometer. In Figure 16, an X-Y stage using Agilent 10715A's is illustrated. As with plane mirror interferometers, the reflectors are plane mirrors mounted at 90° to each other on the stage.

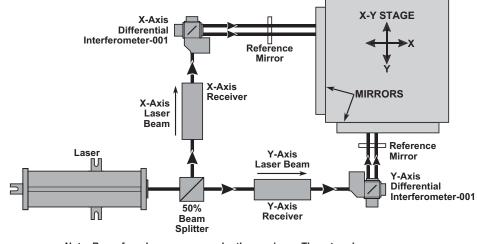
Using the Agilent 10715A Differential Interferometer also requires mounting the reference mirror (supplied with the Agilent 10715) between the interferometer and measurement reflector. Mounting instructions for the reference mirror are given later in this chapter.

The Agilent 10715A-001 interferometer turns the beam as shown in Figure 16. This configuration requires use of opposite input apertures for each interferometer, resulting in reversed direction senses for the X and Y axes. The reversed direction sense must be corrected in the electronics or by software. Note that the receiver for each axis is above the input beam.

# Three-axis measurement system using discrete plane mirror interferometers (X, Y, YAW)

Some X-Y stage applications require measurement or control of the stage yaw. Yaw is angular rotation of the stage about an axis (the Z-axis) perpendicular to the plane of the stage. With two interferometers on one axis of the stage, angular motion can be calculated. Figure 17, the yaw angle, THETA, is measured using axes Y and Y, and is calculated as follows:

$$THETA = arctan \frac{(Y - Y)}{D}$$

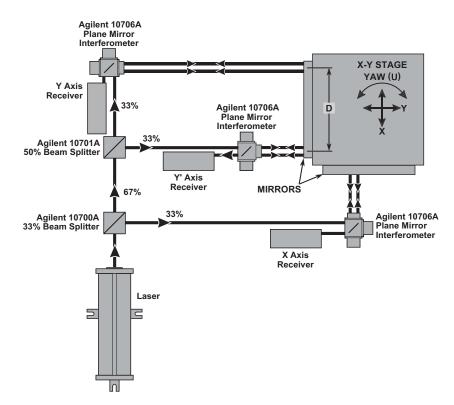


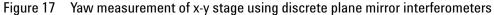
# Note: Beam from laser passes under the receivers. The return beams return to the receivers after being offset in the interferometers.



#### YAW MEASUREMENT OF X-Y STAGE

**TWO-AXIS MEASUREMENT SYSTEM** 





#### Laser and Optics User's Manual, Vol. I

The resulting angular measurement will only be as accurate as the measurement distance, "D". However, even if "D" is not known precisely, this technique can provide extremely high-resolution or relative angular changes.

The resolution depends on "D", and— with electronic resolution extension—can be well under 0.01 arc-seconds. For applications in which the stage is servo-controlled to its initial angle (THETA = 0), this high resolution is the key measurement consideration and the accuracy of D is not critical.

For applications in which accuracy and resolution are both critical, D may be determined precisely by rotating the stage through a known angle ("THETA") and solving the above equation for D.

When installing this type of yaw-measuring system, take care to ensure the parallelism of the adjacent linear measurements to minimize cosine errors.

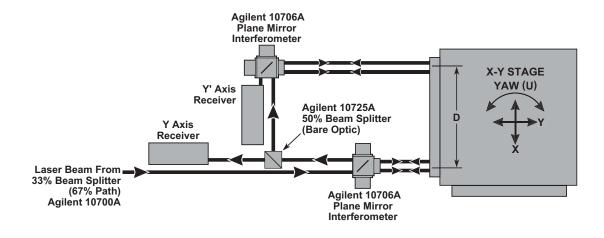
Angular rotation of the measurement mirror is limited to the "Alignment Requirement-vs-Distance" value for the interferometer used. See the "Specifications and Characteristics" section of Chapter 20, "Agilent 10706A Plane Mirror Interferometer," in Volume II of this manual.

When yaw control of a stage must be done at high speeds using a closed-loop control system, the (Y-Y') value needs to be obtained quickly. If the difference is calculated in software in the controller, it may be too slow. There are two methods to achieve a high-speed (Y-Y') output:

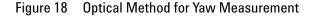
- Electronically
- Optically

**Electronic yaw calculation method** This difference calculation can be done in hardware for both the Y and the Y' axes. A custom servo board could be designed to accept position information from both Y and Y' and perform a fast angular calculation, yielding an input for the yaw servo. See the appropriate electronics documentation for servo-loop interfacing.

**Optical yaw calculation method** There are optical configurations that will allow direct output of the difference between Y and Y', for example on the Y' axis receiver. This is shown in Figures 18 and 19, both using the Agilent 10706A Plane Mirror Interferometer.



#### **OPTICAL METHOD FOR YAW MEASUREMENT**



#### **OPTICAL METHOD FOR YAW MEASUREMENT**

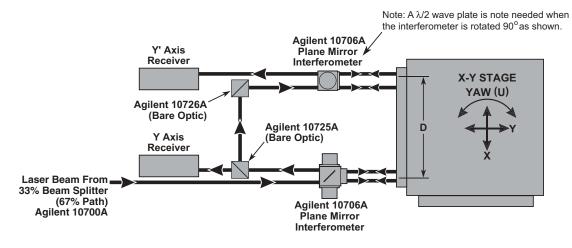


Figure 19 Optical Method for Yaw Measurement

Similar techniques can be used with the Agilent 10715A Differential Interferometer. This is done by splitting off part of the Y-axis combined measurement signal (after going completely through the interferometer) and using this as the input beam to the Y' axis interferometer. This technique outputs (Y-Y') information directly on the Y'-axis receiver. Both of these optical configurations require some special optical components not available through Agilent Technologies. In both figures, a small 50% non-polarizing beam splitter is required. This beam splitter must be very small to avoid blocking or clipping the adjacent beam. This is also true for the beam bender required in the configuration shown in Figure 19.

# Multiaxis systems using Agilent 10719A and Agilent 10721A interferometers

Multiaxis systems using Agilent 10719A and Agilent 10721A interferometers are described in Chapter 25, "Agilent 10719A One-Axis Differential Interferometer," and Chapter 26, "Agilent 10721A Two-Axis Differential Interferometer," in Volume II of this manual.

# Multiaxis systems using Agilent 10735A and Agilent 10736A three-axis interferometers

Multiaxis systems using Agilent 10735A and Agilent 10736A interferometers are described in Chapter 27, "Agilent 10735A, 10736A, and 10736A-001 Three-Axis Interferometers," in Volume II of this manual.

# **Optical Device Troubleshooting**

Problems with the optical devices are usually caused by their misalignment. Refer to the alignment procedures in Chapter 4, "System Installation and Alignment," of this manual for further information.

Air turbulence caused by ventilation equipment or temperature gradients near the laser beam path can also cause measurement problems. If this is suspected, shield the area around the laser beam and optical devices with cardboard tubing, plastic sheet, or other suitable material. Some problems with sporadic counting and drift can be traced to air turbulence around the measurement path. This should be considered as a possibility before troubleshooting other parts of the system.

The Agilent 10735A and Agilent 10736A interferometers are designed to use a 9-mm (nominal diameter) laser beam.

The required 9-mm beam is available from an Agilent 5517C-009 laser head. The laser tube in this laser head is referenced to the base of the laser head. The laser head base is different from that of the standard Agilent 5517C Laser Head, and requires a special mounting site configuration, as shown in Figure 20.

The standard Agilent beam-directing optics are designed for use with a 6-mm (maximum nominal diameter) laser beam. For use in 9-mm installations, Agilent offers the Agilent 10725A 9-mm Laser Beam Splitter and the Agilent 10726A 9-mm Laser Beam Bender. These two optical devices do not include mounting hardware. The 9-mm laser measurement system user, designer, or installer, must devise a mounting method that will hold the required optics in position without causing stress that may distort the optic.

The recommended receiver for 9 mm work is an Agilent 10780F Remote Receiver with a 9-mm lens on the fiber optic cable input. If you have an Agilent 10780F Remote Receiver with a 6-mm lens, you can order a 9-mm Replacement Lens Kit Assembly (Agilent part number 10780-67003) and a 9-mm Alignment Target (Agilent part number 10780-40009). The 9-mm lens can be used with any laser beam having a smaller diameter. The 9-mm lens can replace the 6-mm lens, if replacement becomes necessary; be sure to order the 9-mm Alignment Target, also.

The standard Agilent 10780C input aperture is designed for use with a 6-mm laser beam, so it is not recommended for use in a 9-mm laser system.

# **Site Preparation**

## Site preparation for laser head

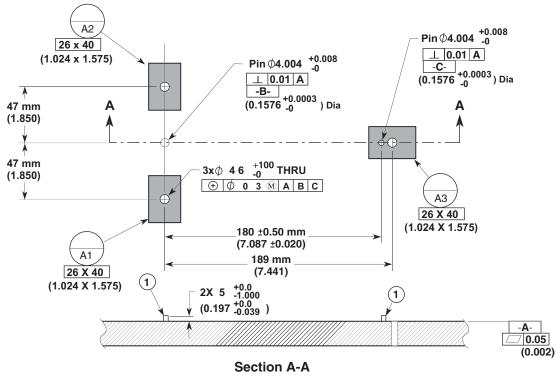
Generally, Agilent laser heads require no special site preparation other than providing appropriate mounting holes. The Agilent 5517C-009 Laser Head´s laser beam output is referenced to locations on its base. You can install this laser head simply by providing appropriate mounting holes, or you can create a specially prepared site to take advantage of its referenced output capability; specifications for a site for this latter use are given in Figure 20.

## Site preparation for optical devices

Beam Benders such as the Agilent 10726A are used to create the laser path from the laser head to the interferometer. The Agilent 10726A Beam Benders are supplied by Agilent without mounting hardware. When you attach these optical pieces to their mounting hardware, use an attachment method that will not damage or distort them.

In a measurement system having more than one interferometer unit, a Beam Splitter such as the Agilent 10725A is used to create a second laser path to deliver the laser beam from the laser head to the second interferometer. Agilent 10726A Beam splitters are supplied by Agilent without mounting hardware. When you attach these optical pieces to their mounting hardware, use an attachment method that will not damage or distort them.

#### AGILENT 5517C-009 MOUNTING LOCATION



Notes: 1. Dowel Pin-steel, ⊘4.004 - 4.012, 2 Places 2. Dimensioned in Accordance with ANSI Y14.5M - 1982

Figure 20 Agilent 5517C-009 Mounting Location - Dimensions

# Site preparation for referenced interferometers

"Referenced" interferometers currently available from Agilent are listed in the following table.

For information about	See chapter (in Volume II)
Agilent 10719A One-Axis Differential Interferometer	25
Agilent 10719A-C02 One-Axis Differential Interferometer	25
Agilent 10721A Two-Axis Differential Interferometer	26
Agilent 10721A-C01 Two-Axis Differential Interferometer	26
Agilent 10735A Three-Axis Interferometer	27
Agilent 10736A Three-Axis Interferometer	27
Agilent 10736A Option 001 Three-Axis Interferometer with Beam Bender	27
Agilent E1826E One-Axis Plane Mirror Interferometer (right)	31
Agilent E1826F One-Axis Plane Mirror Interferometer (left)	31
Agilent E1826G One-Axis Plane Mirror Interferometer (straight)	31
Agilent E1827A Two-Axis Vertical Beam Interferometer	32
Agilent E1837A Three-Axis Vertical Beam Interferometer	33
Agilent Z4399A Three-Axis Interferometer	33
Agilent Z4420B Five-Axis Interferometer	34
Agilent Z4421B Five-Axis Interferometer	34
Agilent Z4422B Three-Axis Interferometer	33

The optics in a "referenced" interferometer are referenced to points on the outside of the case., This allows the interferometer to be installed in a predefined position and minimizes any alignment required with, respect to the measurement mirror(s) used with it.

Refer to Chapter 5, "Measurement Optics (General Information)," and Chapter 6, "NGI Measurement Optics (General Information)" in this manual for information that can help you design the mounting location for an Agilent "referenced" interferometer.



Agilent Laser and Optics User's Manual Volume I

4

# System Installation and Alignment

Introduction, 80 Pre-Installation Checklist, 80 System Grounding, 81 External Cabling, 81 Mounting Optics, 84 Aligning Optics, 88 Receiver Alignment and Gain Adjustment, 92 Autoreflection Method Summary, 92 Overlapping Dots Method Summary, 94 Aligning the Agilent 10702A Linear, Agilent 10766A Linear, and Agilent 10705A Single Beam Interferometers, 96



# Introduction

This chapter provides information to help you install and align an Agilent laser measurement system. Information presented includes:

- Pre-installation checklist
- Installation of the laser heads and receivers
- Installation of optics
- Alignment procedures for the different interferometers
- Installation and alignment of the wavelength tracker

# **Pre-Installation Checklist**

In addition to reading chapters 1 through 3 of this manual, complete the following items before installing a laser position transducer into any application.

- □ Complete Beam Path Loss Calculation (see the "Beam Path Loss Computation" section in Chapter 3, "System Design Considerations").
- □ If you are using a plane mirror interferometer, you must supply the plane mirror reflector if the Agilent 10724A Plane Mirror Reflector will not work for your installation. See Chapter 5, "Measurement Optics (General Information)," and chapters 18 through 34 (in Volume II) of this manual for interferometer descriptions and mirror specifications. See Chapter 36, Accessories," in Volume II of this manual for a description of the Agilent 10724A Plane Mirror.
- ☐ If you are using the Agilent 10715A Differential Interferometer, you must supply an adjustable mount for the reference mirror included with the Agilent 10715A.
- □ Determine laser head and interferometer orientation for required direction sensing. (See the Chapter 11, "Principles of Operation," Chapter 3, "System Design Considerations," and Chapter 5, "Measurement Optics (General Information)," in this manual.)
- □ If you are using an Agilent 10719A One-Axis Differential Interferometer or an Agilent 10721A Two-Axis Differential Interferometer, you must supply a suitable mounting arrangement for the interferometer. (See chapters 25 and 26 for recommendations.)
- □ If you are using an Agilent 10735A Three-Axis Interferometer, Agilent 10736A Three-Axis Interferometer, or an Agilent 10736A-001 Three-Axis Interferometer with Beam Bender, you must: 1) provide a

suitable mounting location that references the interferometer to the stage whose motion is being measured, and 2) make provision for adjusting the laser beam input to the interferometer by translating and turning the beam.

- □ Provide for aligning the optics, laser head, and receiver(s) on the machine.
- □ Be sure to allow for transmitted beam offset of beam splitters (Agilent 10700A and Agilent 10701A) in your design.

# System Grounding

Most Agilent laser systems are grounded through the line cord. For these systems, additional grounding of the chassis is not required, but doing so shouldn't interfere with normal operation. Refer to system grounding information in Chapter 3, "System Design Considerations," of this manual.

# **External Cabling**

The following paragraphs cover all external connections to the laser head and receiver. Each instrument is shipped with a set of color-coded labels.

These can be used to label both the cables and their respective rear-panel connectors for easy identification.

## Laser head cables

#### For use with Agilent 10895A VME Axis Board

Agilent 10791A/B/C Laser Head Cable (has spade lugs for use with a power supply other than the Agilent 10884B) The Agilent 10791A/B/C Laser Head Cable connects an Agilent 5517A/B/BL/C/D/DL/FL to the Agilent 10895A VMEbus Aaxis Board. The Agilent 10791A/B/C Laser Head Cable has spade lugs for connecting the laser head to a customer-supplied power supply (see Figure 283 in Chapter 36 of Volume II).

# For use with Agilent 10885A PC, 10889B PC, 10896B VME, 10897C VME, 10898A VME, or N1231A/B PCI axis board

Agilent 10881A/B/C Laser Head Cable (has a DIN for use with the Agilent 10884B Power Supply) The Agilent 10881A/B/C Laser Head Cable connects an Agilent 5517A/B/BL/C/D/DL/FL to the Agilent 10885A PC Axis Board, Agilent 10889B PC Servo Axis Board, Agilent 10896B VME Laser Compensation Board, Agilent 10897C VME High Resolution Laser Axis Board, Agilent 10898A VME High Resolution Dual Laser Axis Board, or Agilent N1231A/B PCI Three-Axis Board. The Agilent 10881A/B/C cable is "Y" shaped and has three connectors that are all different as shown in Figure 285 in Chapter 36 of Volume II. The connectors on the laser head end of the cable and the laser head are "keyed" to go together only one way. The Agilent logo will be "up" on the connector "boot" when the connection is correctly made. The cable connector has locking rings, which take about 1/3-turn clockwise to secure the cable to the mating connector.

Agilent 10881D/F/E Laser Head Cable (has spade lugs for use with a power supply other than the Agilent 10884B) The Agilent 10881D/F/E Laser Head Cable connects an Agilent 5517A/B/BL/C/D/DL/FL to the Agilent 10885A PC Axis Board, Agilent 10889B PC Servo Axis Board, Agilent 10896B VME Laser Compensation Board, Agilent 10897C VME High Resolution Laser Axis Board, Agilent 10898A VME High Resolution Dual Laser Axis Board, or Agilent N1231A/B PCI Three-Axis Board. The Agilent 10881D/E/F Laser Head Cable has spade lugs for connecting the laser head to a customer-supplied power supply (see Figure 286 in Chapter 36 of Volume II).

Agilent N1251B High Performance Laser Head Cable (has a DIN for use with the Agilent 10884B Power Supply) The Agilent N1251B High Performance Laser Head Cable connects an Agilent 5517A/B/BL/C/D/DL/FL to the Agilent 10897C VME High Resolution Laser Axis Board, Agilent 10898A VME High Resolution Dual Laser Axis Board, or Agilent N1231A/B PCI Three-Axis Board. As shown in Figure 289, the Agilent N1251B cable is "Y" shaped and has three connectors that are all different. The connectors on the laser head end of the cable and the laser head are "keyed" to go together only one way. The Agilent logo will be "up" on the connector "boot" when the connection is correctly made. The cable connector has locking rings, which take about 1/3-turn clockwise to secure the cable to the mating connector.

## **Receiver cables**

See Chapter 35, "Receivers," in Volume II of this manual for installation and alignment information.

#### CAUTION

Each connector on the Agilent 10790A/B/C Receiver Cable has both a male and female half. Before making a connection, be sure the male half of the cable connector is properly aligned with the female half of the mating connector. Failure to align the pins prior to mating the connectors may result in damaged pins.

#### For use with Agilent 10895A VME Axis Board

#### Agilent 10790A/B/C Receiver Cable

The Agilent 10790A/B/C Receiver Cable is used to connect the Agilent receivers to the Agilent 10895A VME Axis Board, for both measurement and Wavelength Tracker axes. This cable's connectors are identical on either end as shown in Figure 282. The connectors on the cable and on the receiver and Agilent electronics are "keyed" to go together only one way. The connectors on the cable each have a locking ring, which take a 1/4-turn clockwise to secure the cable to its mating connector.

# For use with Agilent 10885A PC, 10889B PC, 10896B VME, 10897C VME, 10898A VME, or N1231A/B PCI axis board

#### Agilent 10880A/B/C Receiver Cable

The Agilent 10880A/B/C Receiver Cable is used to connect the Agilent receivers to the Agilent 10885A PC Axis Board, Agilent 10889B PC Servo Axis Board, Agilent 10896B VME Laser Compensation Board, Agilent 10897C VME High Resolution Laser Axis Board, Agilent 10898A VME High Resolution Dual Laser Axis Board, or Agilent N1231A/B PCI Three-Axis Board, for both measurement and Wavelength Tracker axes. This cable's connectors are different as shown in Figure 284. One connector is a bayonet connector that inserts into the Agilent axis board. The other connector fits the connector on the receiver; this connector is "keyed" to go together only one way. This connector has a locking ring, which takes a 1/4-turn clockwise to secure the cable to its mating connector on the receiver.

#### Agilent N1250A/B High Performance Receiver Cable

The Agilent N1250A/B High Performance Receiver Cable is used to connect the measurement signal from an Agilent E1708A or E1709A Receiver to the Agilent 10897C VME High Resolution Laser Axis Board, Agilent 10898A VME High Resolution Dual Laser Axis Board, or Agilent N1231A/B PCI Three-Axis Board, for both measurement and Wavelength Tracker axes. This cable's connectors are different as shown in Figure 288. One connector is a bayonet connector that inserts into the Agilent axis board. The other connector fits the connector on the receiver; this connector is "keyed" to go together only one way. This connector has a locking ring, which takes a 1/4-turn clockwise to secure the cable to its mating connector on the receiver.

# **Mounting Optics**

## **Adjustable mounts**

Agilent 10710B and Agilent 10711A Adjustable Mounts provide a convenient means of mounting, aligning, and securely locking in position, the optical components of the laser position transducer (see Figure 21). Since both mounts allow some tilt and yaw adjustment, the need for custom fixturing is minimized. These mounts allow the optic being adjusted to be rotated about its optical centerline, simplifying installation.

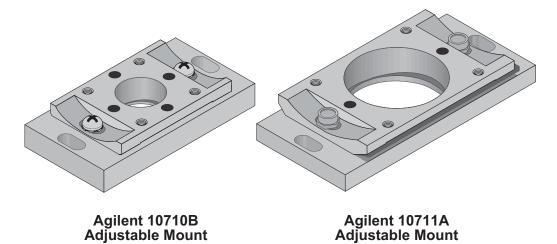


Figure 21 Agilent 10710B and Agilent 10711A adjustable mounts

Both mounts are made of 416 stainless steel. Its magnetic properties can be helpful at the design stage if magnetic clamps are used. However, in final installation, secure the mount with the screws provided.

The Agilent 10719A, Agilent 10721A, Agilent 10735A, and Agilent 10736A interferometers do not use adjustable mounts.

See Table 3 (in Chapter 5) or Table 80 in Volume II of this manual for a list of optics that can be used with these mounts.

## Typical mounting of optics which use adjustable mounts

- 1 Figure 22 shows how to mount the beam splitting and beam bending optics or the single-beam interferometer in the horizontal plane, using the Agilent 10710B Adjustable Mount.
- 2 Figure 23 shows how to mount the beam splitting and beam bending optics or the single-beam interferometer in the vertical plane, using the Agilent 10710B Adjustable Mount.

- 3 Figure 24 shows how to mount certain linear, plane mirror, or differential interferometers in the horizontal plane, using the Agilent 10711A Adjustable Mount.
- 4 Figure 25 shows how to mount certain linear, plane mirror, or differential interferometers in the vertical plane, using the Agilent 10711A Adjustable Mount.

## **Fasteners**

All optical components which are designed to be used with an Agilent 10710B or Agilent 10711A Adjustable Mount are supplied with English mounting hardware. The screws supplied with each optical component are those required to mount to its respective adjustable mount.

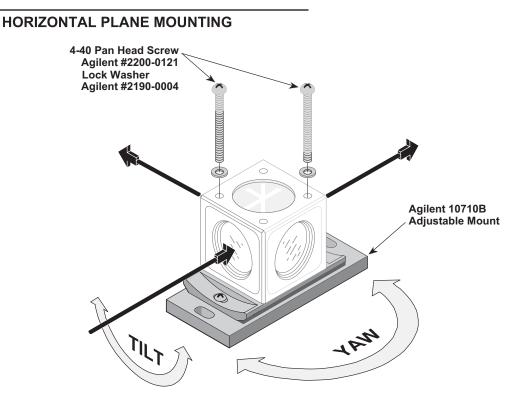


Figure 22 Horizontal plane mounting using the Agilent 10710B adjustable mount

#### 4 System Installation and Alignment

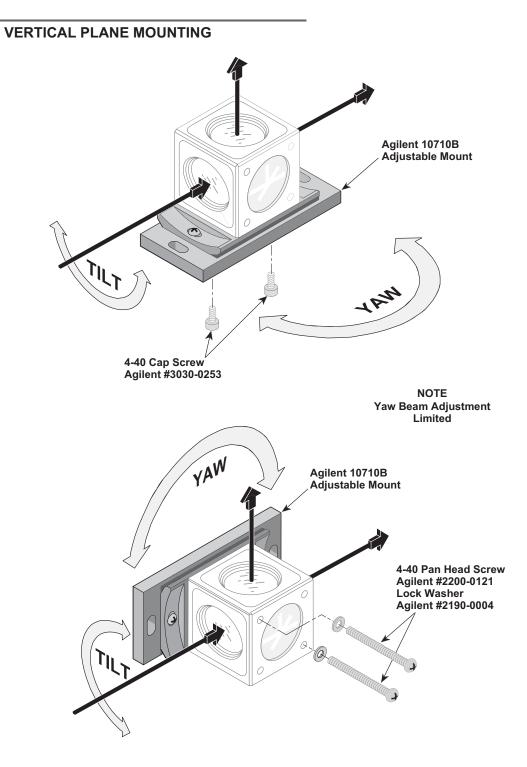


Figure 23 Vertical plane mounting using the Agilent 10710B adjustable mount

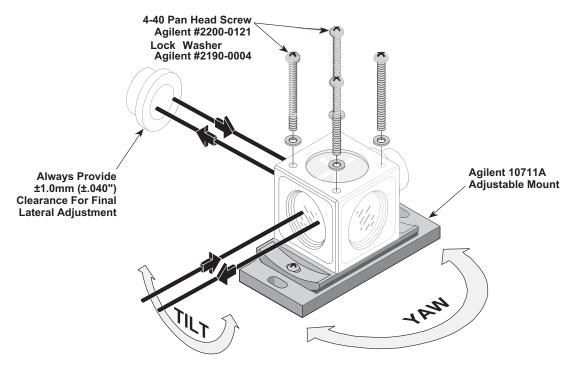


Figure 24 Horizontal plane mounting using the Agilent 10711A adjustable mount

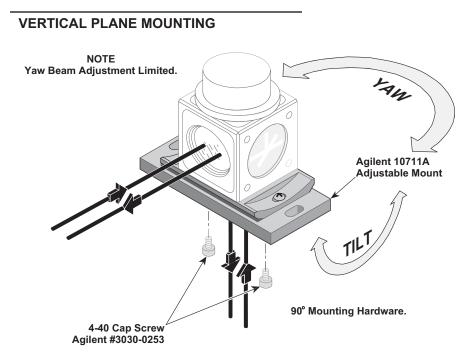


Figure 25 Vertical Plane Mounting Using the Agilent 10711A Adjustable Mount

# **Aligning Optics**

## General

When installed in a positioning system, any transducer must be aligned to ensure correct operation and minimum measurement error. The major objectives in aligning the laser system are: 1) maximizing the measurement signal at the receiver, and 2) minimizing cosine error.

#### In general,

- 1 the measurement signal at the receiver is maximized by aligning the optics to center the laser beam on the receiver input, and
- 2 cosine error is minimized by aligning the laser beam in the measurement axis parallel to the motion of travel.

Figure 26 shows a measurement axis where the laser beam is aligned parallel to the mechanical motion of travel of the retroreflector and centered on the receiver.

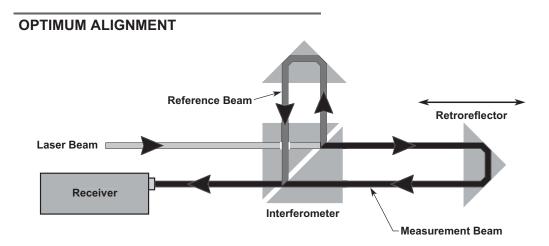


Figure 26 Optimum alignment

The receiver photodetector only measures the overlapping portion of the laser beams. For maximum signal, the interferometer and retroreflector are aligned so the reference beam from the interferometer and the measurement beam from the retroreflector exactly overlap upon recombination. These recombined laser beams then enter the receiver in the center of the lens aperture. From Figure 26, it is clear that if the recombined laser beams entering the receiver are not centered on the photodetector, measurement signal loss will occur. If the interferometer or the retroreflector are misaligned (Figure 27), the reference and measurement beams no longer completely overlap, resulting in signal loss.

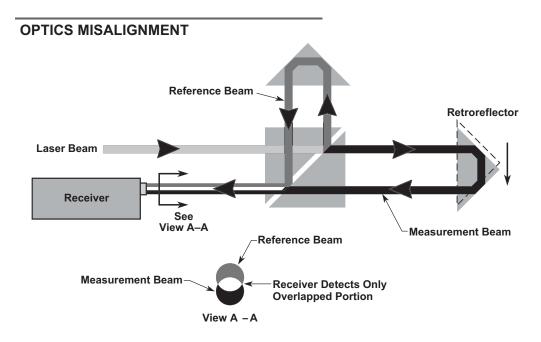
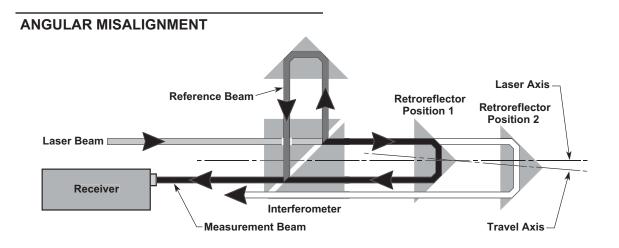
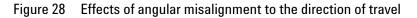


Figure 27 Effect of optics misalignment

Typically, a lateral offset of 1/4 of the beam diameter between the beams is allowable for an adequate measurement signal. However, you must make every effort to optimize the laser beam overlap for maximum performance.

If the measurement beam is not aligned parallel to the direction of retroreflector travel, there are two effects. First, a cosine error is generated of a magnitude directly related to the angle of misalignment. (For a complete description of cosine error, see Chapter 12, "Accuracy and Repeatability," in this manual.) Second, when movement occurs between the optics, the angular misalignment also causes a lateral displacement of the measurement beam with respect to the reference beam at recombination, resulting in additional signal loss. Figure 28 illustrates the result of angular misalignment.







The presence of measurement signal through the total length of travel does not guarantee that the measurement axis is aligned for minimum cosine error. Also, any angular misalignment of the laser beam to the direction of travel causes a decrease in the measurement signal strength.

# **Alignment principles**

Before beginning any alignment procedure, you should understand the basic principles. The following information summarizes the various factors that affect the optical alignment of the laser system. While performing the alignment procedure, keep in mind:

- 1 In order to achieve maximum accuracy, the laser beam must be parallel to each axis of travel.
- 2 For most systems, start the alignment at the laser head and move out one component at a time until the last component on an axis is aligned and the laser beam impinges on the receiver aperture.

The exception to this principle will be systems using an Agilent 10719A, Agilent 10721A, Agilent 10735A, or Agilent 10736A interferometer; these are "referenced" interferometers, whose design and construction allows them to be installed in specified fixed locations relative to the measurement mirrors with which they will be used. For these systems, it will be necessary to provide adjustment of the laser beam relative to the interferometer, since the interferometer itself is not adjustable.

3 The angular direction of the beam can be aligned by moving the laser head or adjusting a beam bender.

- 4 The reflected beam can be aligned by adjusting a beam splitter or interferometer.
- 5 The angular direction of the beam will not be changed by adjusting a retroreflector. Similarly, the angular direction of a beam transmitted straight through a beam splitter or interferometer will not be changed by adjusting that component.

#### NOTE

There will be up to a 30-arc-minute deviation of the beam when it passes through any interferometer except the Agilent 10702A-001, Agilent 10719A, Agilent 10721A, Agilent 10735A, Agilent 10736A, Agilent 10766A, or the NGI optics. (See the "Specifications" information in the appropriate chapter in this manual for specifications.)

- 6 The retroreflectors (also called cube corners) do not change the angular direction of the beam. However, they do displace the beam and reverse its direction. The laser beam remains parallel to its original path. In the case of the Agilent 10705A Single Beam Interferometer reference cube-corner and the Agilent 10704A Retroreflector, the displacement is zero because the beam hits the center of the cube-corner (when properly aligned)
- 7 On multiaxis configurations, the first axis to be adjusted is the axis whose angular adjustment of the laser beam requires adjustment of the laser head. After the first axis is aligned, the laser head is locked down and any angular adjustment of the laser beam in the other measurement axes is accomplished by rotating the optical components.
- 8 Properly aligned interferometers exhibit less sensitivity to temperature. See "Deadpath error" in Chapter 12, "Accuracy and Repeatability," of this manual for details.
- 9 Set up multiaxis systems with all legs of the laser beam orthogonal to each other and to the measurement mirrors. For ease of optical layout and alignment, you should keep the laser beams horizontal or vertical.
- 10 Define all beam legs (plane and direction) against machined surfaces known to be parallel or perpendicular to the stage plane. Use an auto reflection mirror with square sides (e.g., a metrologist's "true square").
- 11 Before installing the optics, define all beam bends (location and angle) with an optical square (Agilent 10777A) or pentaprism. This ensures the best possible starting point for the final adjustment of the laser system optics.

The remainder of this chapter has these major parts:

- 12 Receiver alignment and gain adjustment procedure, which is common to all measurement axes.
- 13 A discussion of the two major alignment methods: autoreflection and overlapping dots.
- 14 Specific alignment techniques for each type of interferometer.

# **Receiver Alignment and Gain Adjustment**

See Chapter 35, "Receivers," in this manual for this information.

There are two basic alignment techniques used with a laser measurement system: 1) Autoreflection, and 2) Overlapping Dots.

Autoreflection is the more accurate method, and is always preferred. Autoreflection should always be used: 1) for short travel applications, 2) measurements where cosine error must be reduced to the absolute minimum possible, and 3) when plane mirror reflectors are used.

Overlapping Dots is a satisfactory method in applications involving relatively long travel.

In general, regardless of the technique used, alignments are performed with all optical components in place.

# **Autoreflection Method Summary**

The autoreflection method of alignment is recommended for all applications, especially those having less than 0.5 meter (20 inches) travel. It is based on the principle of aligning a reflecting surface normal to the direction of travel and aligning the laser beam perpendicular to this reflecting surface (that is, parallel to the direction of travel) to minimize cosine error. This technique is fast and is the best way to eliminate cosine error.

The principle steps used for the "Autoreflection" method of alignment are given below. A detailed autoreflection alignment procedure for a specific configuration of optics follows the autoreflection method and the overlapping dots method summaries.

- 1 Mount the laser head and optics in the desired locations and align the laser beam roughly parallel to the axes.
- 2 Provide a reflector, aligned perpendicular to the axis of travel. Place the reflector between the interferometer and retroreflector.

<b>NOTE</b> Typical reflectors having required mirror flatness and referenced sides for autoreflection are:	
	True Square
	<ul> <li>Other precision angle plates or squares with a gage block wrung to the appropriate surface.</li> </ul>

The mirrored surface should be perpendicular to its sides (or angle plate) within 15 arcseconds.

Typical means for aligning the mirrored surface perpendicular to the axis of travel are:

- Locating the mirror reference surfaces against fixed reference surfaces on the machine's positioning system (e.g., ways, rails, guides). (See Figure 29.)
- Measuring the reference surfaces on the mirror, true square, or gauge block with a dial indicator, and adjusting the pitch and yaw of the mirror surface. (See Figure 31.)

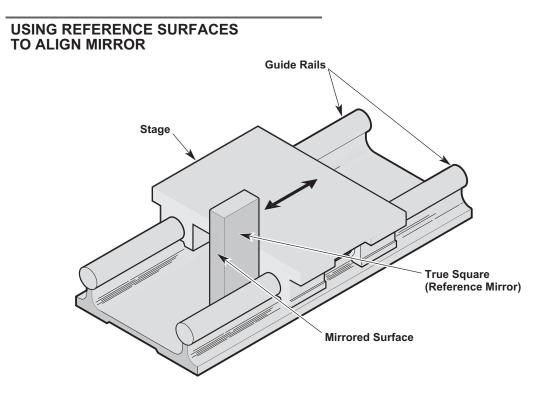


Figure 29 Using reference surfaces to align mirror

- 1 Place the perpendicular reflector at the far end of travel.
- 2 Select the small aperture on the laser head by rotating the front turret.
- 3 Adjust the laser beam so that the beam is reflected by the reflector back upon itself. Alignment is complete when the (small) return beam is centered on the small aperture of the laser head. This adjustment of the laser beam can be performed by moving the laser head, beam bender or interferometer, depending on the optical layout.

# **Overlapping Dots Method Summary**

The overlapping dots alignment method uses the principle that if the measurement beam to the retroreflector is not parallel to the direction of travel, it is offset upon recombination with the reference beam of the interferometer (see Figure 30). When motion occurs between the retroreflector and interferometer along the measurement path, any angular misalignment causes a displacement (at the receiver) of one laser beam with respect to the other which can be visually observed. Since the human eye can resolve a displacement of the beam of approximately 300 micrometers (0.01 inch), this technique can be applied to reduce cosine error for measurement travel of 0.5 meter (20 inches) or longer. For travel less than this, the sensitivity of this technique is normally not sufficient and autoreflection should be used. Cosine error (E), in parts per million (ppm), can be calculated from the following formula:

$$E = \frac{S^2}{8D^2}$$

Where D is the distance measured in millimeters (inches) and S is the lateral offset of the returning beam in micrometers (thousands of an inch). For example, if the distance measured is 600 mm and this results in an offset of the return beam of  $1.2 \text{ mm} (1200 \text{ }\mu)$  then:

$$= \frac{(1200)^2}{(8) \times (600)^2} = 0.5 ppm, 0.5 micrometer per meter of travel$$

The following are the principle steps used for the "Overlapping Dots" method of alignment, followed by a detailed alignment procedure for a specific configuration.

- 1 Mount the laser head and optics in their desired locations.
- 2 Select the small beam aperture on the laser head.

3 With the optics as close together as possible, adjust any component (laser head, interferometer, or retroreflector) to get the dots (reference and measurement beams) to overlap at the receiver.

NOTE

Placing a piece of translucent tape over the receiver lens will help in observing the incident beams.

# MEASUREMENT BEAM DOT MOVEMENT

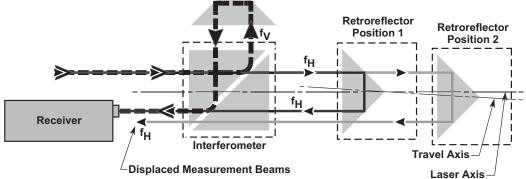
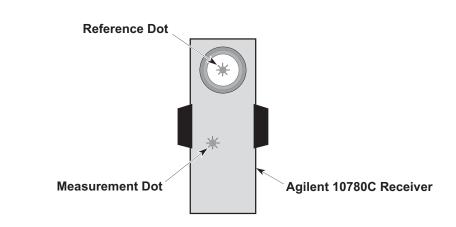


Figure 30 Measurement beam dot movement

- 4 Move the retroreflector away from the interferometer. If the laser beam is not parallel to the axis of travel, the measurement beam dot will begin to move away from the reference beam dot. The dot will move until the beam is cut off by the edge of the interferometer's aperture. Stop moving the retroreflector before the beam is thus blocked, or when the end of travel is reached. Figure 30 shows why the measurement dot moves.
- 5 Figure 31 illustrates a typical two-dot pattern on the receiver that is seen after the optics have moved. Now rotate the beam until the dots again overlap at the receiver. This adjustment of the laser beam can be done by moving the laser head, beam bender, or interferometer, depending on the optical layout.

#### NOTE

Lateral movement of either the laser head or interferometer may also be necessary to achieve alignment.



#### **RESULTS OF REFLECTOR MOVEMENT**

Figure 31 Results of reflector movement

# Aligning the Agilent 10702A Linear, Agilent 10766A Linear, and Agilent 10705A Single Beam Interferometers

The alignment techniques for the linear and single-beam interferometers are nearly the same. Both use a retroreflector (cube-corner) as the measurement reflector.

Either the Autoreflection or the Overlapping Dots method may be used to maximize return measurement signal power and to minimize cosine error. The Autoreflection method is always preferred because it is more accurate. It must be used for measurement distances less than 0.5 meter (20 inches) and is strongly recommended for distances over 0.5 meter.

The Overlapping Dots method should only be used when the measurement distance is over 0.5 meter.

The choice of method used depends on convenience and the nature of the application. The goal for both of these alignment methods is to have the reference and measurement beams be coincident at the receiver throughout the measurement.

# Alignment aids (for Agilent 10702A, Agilent 10766A, Agilent 10705A)

To help in aligning these interferometers, an alignment aid is included with each. They are:

- For Agilent 10702A and Agilent 10702A-001—Alignment target (Agilent Part Number 10702-60001). See Figure 32.
- For Agilent 10766A—Alignment target (Agilent Part Number 10767-60001). See Figure 32.
- For Agilent 10705A–Alignment Target (Agilent Part Number 10705-60001). See Figure 32.

These alignment aids are magnetic, to simplify positioning them on the interferometer. They are used on the input side of the interferometer to properly position the beam.

## ALIGNMENT AIDS



Figure 32 Linear and single-beam interferometer alignment aids

# Autoreflection alignment procedure (for Agilent 10702A, Agilent 10766A, Agilent 10705A)

This procedure describes the autoreflection alignment method used on a two-axis system.

Figure 33 shows a measurement setup similar to Figure 34(A) except that the referenced mirrors (true squares) are included.

```
NOTE
```

Steps 1 through 11 constitute the X-axis autoreflection alignment procedure.

- 1 With all optical components in place, install the alignment targets on the interferometer and the receiver (Figure 34, position 1). Place a piece of opaque material, such as frosted tape, in front of the retroreflector.
- 2 With the laser beam passing through the 50% beam splitter, adjust the laser head and interferometer until the laser beam enters one hole of the alignment target and exits the other to hit the receiver alignment target centered on the hole over the photodetector.

NOTE This is the reference beam that hits the receiver.

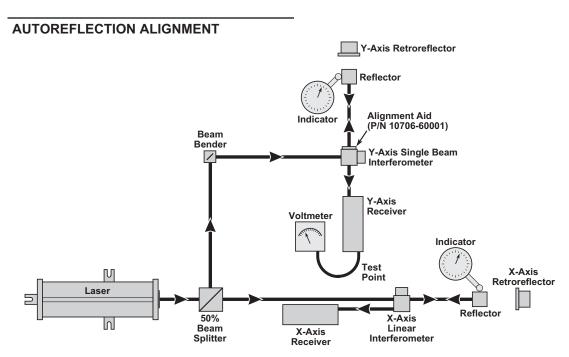


Figure 33 Autoreflection alignment

3 Place a referenced mirror (true square) between the interferometer and retroreflector so that the measurement beam from the interferometer hits its reflective surface. See Figure 33.

Align the referenced mirror (true square) with a precision indicator until its reflective surface is perpendicular to the direction of travel. See Figure 33.

4 Turn the front turret of the laser head to select the small aperture.

#### NOTE

If the distance between the laser head and the reflector is 0.5 meter (20 inches) or more, the formula given above in the paragraph on Overlapping Dots determines the cosine error based on the offset of the return beam at the laser head. For example, a distance between the laser head and reflector of 0.5 meter and an offset of the return beam at the small aperture of the laser of 500 microns (0. 0202 inch) gives a cosine error of approximately 0.12 ppm.

5 Pitch and yaw the laser head until the beam reflects back on itself from the referenced mirror (true square) and is centered on the small aperture of the laser head. Slight side-to-side movements of the interferometer may be required to ensure that the reference beam from the interferometer is centered on the receiver alignment target.

#### NOTE

For high-accuracy alignment or for installations where there is less than 0.5 meter (20 inches) between the laser head and reflector, perform steps 6 through 8.

- 6 Remove the receiver alignment target and interferometer alignment target and select the large aperture of the laser head.
- 7 With a fast-responding voltmeter (preferably an analog type) attached to the receiver test point and receiver case ground, pitch and yaw the laser beam (laser head or interferometer on this axis) until a signal is received on the receiver. (The voltmeter will suddenly jump to some value greater than 0.25 volt.) This is a critical adjustment and may initially require great care.
- 8 Adjust the laser beam in pitch and yaw to get the maximum voltmeter reading (which may be fluctuating). Now carefully readjust the interferometer until the voltage reading suddenly drops back down to about 0.3 volt.

#### NOTE

The alignment should be adjusted such that the voltage reading from the receiver test point occurs just below the sudden jump up in voltage. If the alignment is fixed to sustain this peaked voltage, system operation will be degraded.

This procedure will align the laser beam to within  $\pm 1.2$  arcminutes of the direction of travel, resulting in a cosine error of approximately 0.05 ppm. That is 0.05 micron per meter of travel (0.05 microinch per inch) of cosine error.

- 9 Fasten the laser head and interferometer securely, preserving the alignment. Remove the referenced mirror (true square) and the opaque material.
- 10 Reposition the retroreflector until the return measurement beam is centered on the receiver alignment target and overlaps the reference beam from the interferometer.

NOTE

Placing a piece of translucent tape over the receiver lens will help in observing the incident beams.

11 Verify that the receiver's LED is ON and the voltage at the receiver test point is between 0.6 and 1.3 Vdc (for 10780C/F), or 1.5 and 8.0 Vdc (for E1708A), or 1.8 and 10.0 Vdc (for E1709A).

<u>N</u>0TE

Steps 12 through 22 constitute the Y-axis autoreflection alignment.

- 12 Pitch and yaw the 50% beam splitter until the reflected laser beam is centered on the beam bender aperture. Slight side-to-side adjustments of the 50% beam splitter may be necessary to ensure there is no beam clipping. Fasten the 50% beam splitter securely.
- 13 Adjust the beam bender until the reflected beam is centered on the aperture of the single-beam interferometer. The single-beam interferometer alignment target can be used as an aid and then removed. Fasten the beam bender securely.
- 14 Place the receiver alignment target on the receiver and rotate the turret of the laser head to select the small aperture.
- 15 Place a referenced mirror (true square) between the interferometer and the retroreflector so that the measurement beam from the interferometer strikes its reflective surface. Align the referenced mirror with a precision indicator until its reflective surface is perpendicular to the direction of travel in both angular axes (arcseconds).
- 16 Place a single-beam interferometer alignment aid on the output side of the interferometer and adjust the single-beam interferometer in pitch and yaw until the beam 1) reflects back on itself and 2) is centered on the small aperture of the laser head. Slight side-to-side movement of the interferometer may be required to ensure that the reference beam from the

interferometer is still centered on the receiver alignment target. Do not adjust the laser head.

NOTE

For high-accuracy alignment or for installations where there is less than 0.5 meter (20 inches) between the laser head and reflector, perform steps 17 through 19.

- 17 Remove the receiver alignment target and interferometer alignment target and select the large aperture of the laser head.
- 18 With a fast-responding voltmeter (preferably an analog type) attached to the receiver test point and receiver case ground, pitch and yaw the laser beam (laser head or interferometer on this axis) until a signal is received on the receiver. (The voltmeter will suddenly jump to some value greater than 0.25 volt.) This is a critical adjustment and may initially require great care.
- 19 Adjust the laser beam in pitch and yaw to get the maximum voltmeter reading (which may be fluctuating). Now carefully readjust the interferometer until the voltage reading suddenly drops back down to about 0.3 volt.

#### NOTE

The alignment should be adjusted such that the voltage reading from the receiver test point occurs just below the sudden jump up in voltage. If the alignment is fixed to sustain this peaked voltage, system operation will be degraded.

This will align the laser beam to within  $\pm 1.2$  arcminutes to the direction of travel, resulting in a cosine error of approximately 0.05 ppm. That is 0.05 micron per meter of travel (0.05 microinch per inch) of cosine error.

- 20 Fasten the single-beam interferometer and beam bender securely, making sure the alignment is preserved. Remove the reflector (true square).
- 21 Adjust the retroreflector until the return measurement beam is centered on the receiver and overlaps the reference beam from the interferometer.

#### NOTE

Placing a piece of translucent tape over the receiver lens will help in observing the incident beams.

22 Verify that the receiver's LED is ON and the voltage at the receiver test point is between 0.6 and 1.3 Vdc (for 10780C/F), or 1.5 and 8.0 Vdc (for E1708A), or 1.8 and 10.0 Vdc (for E1709A).

# Overlapping dot alignment procedure (for Agilent 10702A, Agilent 10766A, Agilent 10705A)

This subsection describes the overlapping dots alignment method used on a two-axis configuration. Figure 34 is a typical measurement configuration which includes a linear interferometer and a single-beam interferometer.

#### NOTE

Steps 1 through 10 constitute the X-axis "Overlapping Dot" alignment procedure.

- 1 Place the interferometer alignment target on the laser side of the X-axis interferometer and place the receiver alignment target on the receiver so that it is not in the laser beam (see Figure 34, position 1). Place a piece of opaque material such as frosted tape between the interferometer and retroreflector.
- 2 With the retroreflector and interferometer at the closest point, adjust the laser head until the laser beam 1) passes through the 50% Beam Splitter, 2) enters one hole of the alignment target on the interferometer, and 3) exits the other hole to hit the receiver alignment target centered on the hole over the photodetector. A slight lateral adjustment of the interferometer or laser head may be required.
- 3 Remove the opaque material from between the retroreflector and interferometer and rotate the receiver alignment target to position 2 (see Figure 34).
- 4 Adjust the retroreflector to center the return measurement beam on the receiver alignment target.
- 5 Move the retroreflector to its furthest point of travel.
- 6 Pitch and yaw the laser head to center the return beam on the receiver alignment target.
- 7 Return the retroreflector to the point closest to the interferometer.
- 8 Repeat steps 4 through 7 until the return beam is centered on the receiver alignment target at both ends of travel. A lateral offset of 500 microns over a 0.5 meter travel is equal to a cosine error of 0.12 ppm or 0.12 micron per meter of travel (0.12 microinch per inch).

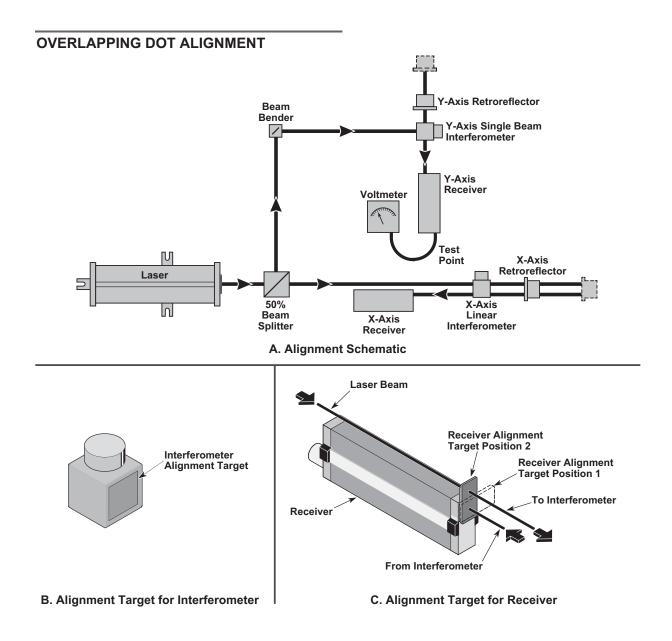


Figure 34 Overlapping dot alignment

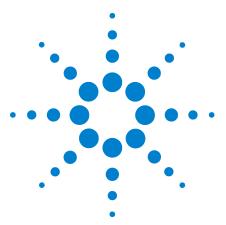
9 If the reference beam returning from the interferometer is not centered on the receiver target, adjust the interferometer until both the reference and the measurement beams are centered.

NOTE In step 10, make sure the alignment is not disturbed.	
--	--

10 Lock the laser head and X-axis optics down securely. Remove the receiver alignment target. Verify that the LED indicator on the receiver is lighted and that the voltage at the receiver test point is between 0.6 and 1.3 Vdc.

#### NOTE

- Steps 11 through 20 constitute the Y-axis "Overlapping Dot" alignment procedure
- 11 Place the alignment target on the Y-axis single-beam interferometer and on the Y-axis receiver. Place a piece of opaque material between the single-beam interferometer and the retroreflector.
- 12 Pitch and yaw the 50% beam splitter until the reflected laser beam is centered in the beam bender entrance aperture. Slight lateral adjustments of the 50% beam splitter may be necessary to ensure there is no beam clipping. Fasten the 50% beam splitter securely.
- 13 Adjust the beam bender until the reflected beam is centered on the alignment target installed on the single-beam interferometer. Fasten the beam bender securely in place.
- 14 With the single-beam interferometer and retroreflector at their closest points, adjust the single-beam interferometer until the reference beam is centered on the receiver alignment target. Remove the opaque material.
- 15 Adjust the Y-axis retroreflector until the measurement beam is centered on the receiver alignment target.
- 16 Move the retroreflector to its furthest point of travel.
- 17 Pitch and yaw the single-beam interferometer to center the return beam from the retroreflector on the receiver alignment target. When aligning the single-beam interferometer, it may also be necessary to make slight lateral adjustments to ensure that the reference beam from the single-beam interferometer is also centered on the receiver alignment target.
- 18 Return the retroreflector to the point closest to the single-beam interferometer.
- 19 Repeat steps 15 through 18 until the return beam from the retroreflector is centered on the receiver alignment target at both extremes of travel. Secure the single-beam interferometer, preserving the alignment.
- 20 Remove the single-beam alignment target and the receiver alignment target. Verify that the receiver's LED is ON and the voltage at the receiver test point is between 0.6 and 1.3 Vdc (for 10780C/F), or 1.5 and 8.0 Vdc (for E1708A), or 1.8 and 10.0 Vdc (for E1709A).



Agilent Laser and Optics User's Manual Volume I

# 5 Measurement Optics (General Information)

General, 106 Resolution, 110 Range, 110 Measurement Direction Sense, 110 Vibration Isolation, 113 Fasteners, 113 Vacuum Applications, 114 Use Through Window, 114 Differential Measurements with Interferometers, 114 Moving Interferometer Instead of Reflector, 116



## General

Each laser measurement system's measurement axis must have an interferometer and a reflector. Machine design considerations determine which type of interferometer is best. The choice of the interferometer for each axis usually determines the reflector for that axis.

This chapter describes the Agilent Technologies measurement optics available for Agilent Technologies laser measurement systems. The first part of this chapter presents material that should be useful to the user of any of the interferometers. Following this introductory material, chapters 8 through 25 describe individual interferometer types, including characteristics and specifications.

Table 3 lists the measurement optics in order by Agilent Model Number (it doesn't list the Next Generation Interferometers, see Chapter 6, "NGI Measurement Optics (General Information),". Table 3 also: 1) identifies the chapter in which each measurement optic is described, 2) provides summary descriptions of the measurement optics, and 3) lists the reflectors and Agilent adjustable optics mounts with which the optics may be used. (The mounts are described in Chapter 36, "Accessories," in Volume II of this manual.)

Agilent Technologies beam-directing optics are described in Chapter 17, "Beam-Directing Optics," of this manual.

Agilent Technologies next generation interferometers (NGIs) are introduced in Chapter 6, "NGI Measurement Optics (General Information)," in this manual. Chapters 31 through 34 describes the different NGI interferometer models.

Other Agilent optics that are neither 1) interferometers nor 2) beam-directing optics are described in Chapter 36, "Accessories," in Volume II of this manual.

Manual Chapter	Model Number and Name	Application	System Resolution	Beam Separation	Config- uration	Reflector	Reflector Weight	Mount Used
8	Agilent 10702A Linear Interferometer	General Purpose	λ/64 (10 nm)	12.7 mm (0.5 in)	Straight- through or Turned	Agilent 10703A	42 g (1.5 oz)	Agilent 10711A
8	Agilent 10702A-001 Linear Interferometer	General Purpose	λ/64 (10 nm)	12.7 mm (0.5 in)	Straight- through or Turned	Agilent 10703A	42 g (1.5 oz)	Agilent 10711A
9	Agilent 10705A Single Beam Interferometer	Low-mass Limited space	λ/64 (10 nm)	Not Applicable (single beam)	Straight- through or Turned	Agilent 10704A	10.5 g (0.4 oz)	Agilent 10710B
10	Agilent 10706A Plane Mirror Interferometer	Plane Mirror	λ/128 (5 nm)	12.7 mm (0.5 in)	Straight- through or Turned	Agilent 10724A or user supplied	50 g (1.8 oz)	Agilent 10711A
11	Agilent 10706B High Stability Plane Mirror Interferometer	Plane Mirror	λ/128 (5 nm)	12.7 mm (0.5 in)	Straight- through or Turned	Agilent 10724A or user supplied	50 g (1.8 oz)	Agilent 10711A
12	Agilent 10715A Differential Interferometer	High Accuracy Plane Mirror	λ/128 (5 nm)	12.7 mm (0.5 in)	Straight- through or Turned	Agilent 10724A or user supplied	50 g (1.8 oz)	Agilent 10711A
12	Agilent 10715A-001 Differential Interferometer	High Accuracy Plane Mirror	λ/128 (5 nm)	12.7 mm (0.5 in)	Turned	Agilent 10724A or user supplied	50 g (1.8 oz)	Agilent 10711A
13	Agilent 10716A High Resolution Interferometer	High Resolution Plane Mirror	λ/256 (2.5 nm)	12.7 mm (0.5 in)	Straight- through or Turned	Agilent 10724A or user supplied	50 g (1.8 oz)	Agilent 10711A
14	Agilent 10717A Wavelength Tracker	Wavelength-of-li ght compensation	_	Not Applicable	Not Applicable	Built-in	Not Applicable	none
15	Agilent 10719A One-axis Differential Interferometer	One Linear Plane Mirror Measurement (Differential) or One Angular Measurement	λ/128 (5 nm) 0.054 arcsec (0.26 µrad)	See Specifications	Straight- through only	custom	custom	custom

### Table 3 Measurement Optics Summary

Manual Chapter	Model Number and Name	Application	System Resolution	Beam Separation	Config- uration	Reflector	Reflector Weight	Mount Used
16	Agilent 10721A Two-axis Differential Interferometer	Two Linear Plane Mirror Measurements (Differential) Linear	λ/128 (5 nm) 0.08 arcsec	See Specifications	Straight- through only	custom	custom	custom
17	Agilent 10735A Three-axis Interferometer	Yaw 3 Linear Plane Mirror Measurements (Displacement,	(0.4 μrad) λ/128 (5 nm)	See Specifications	Turned only	custom	custom	custom
		Yaw, Pitch)	0.04 arcsec, (0.2 μrad) 0.05 arcsec, (0.24 μrad)					
17	Agilent 10736A Three-axis Interferometer	3 Linear Plane Mirror Measurements (Displacement,	λ/128 (5 nm)	See Specifications	Turned only	custom	custom	custom
		Yaw, Pitch)	0.04 arcsec, (0.2 μrad) 0.05 arcsec, (0.24 μrad)					
17	Agilent 10736A- 001 Three-axis Interferometer with Beam Bondor	3 Linear Plane Mirror Measurements ( Displacement,	λ/128 (5 nm)	See Specifications	Turned only	custom	custom	custom
	Bender	Pitch)	0.05 arcsec, (0.24 µrad)					

Table 3 Measurement Optics Summary (continued)

Manual Chapter	Model Number and Name	Application	System Resolution	Beam Separation	Config- uration	Reflector	Reflector Weight	Mount Used
18	Agilent 10737L/R Compact Three-axis Interfero-meters	3 Linear Plane Mirror Measurements (Displacement, Yaw,	See Specs.	See Specs.	Turned only	Plane mirror or cube corners	Customer determined	Agilent 10711A
		Pitch)						
8	Agilent 10766A Linear Interferometer	General Purpose	λ/64 (10 nm)	11 mm (0.43 in)	Straight- through or Turned	Agilent 10767A	224 g (0.5 lb)	Agilent 10785A
19	Agilent 10770A Angular Interferometer	High Accuracy Plane Mirror	λ/64 (10 nm)	11 mm (0.43 in)	_	Agilent 10771A	650 g (1.5 lb)	Agilent 10785A
20	Agilent 10774A Short Range Straightness Optics	High Resolution Plane Mirror	_	Not Applicable	_	Included	800 g (1.8 lb)	Agilent 10776A
20	Agilent 10775A Long Range Straightness Optics	High Resolution Plane Mirror		Not Applicable		Included	800 g (1.8 lb)	Agilent 10776A

#### Table 3 Measurement Optics Summary (continued)

## Resolution

The fundamental optical resolution for each interferometer type is listed in Table 4. Using electronic resolution extension, the system resolution is increased significantly. Depending on the system, additional resolution extension factors of 32 is available.

Interferometer Type	Fundamental Resolution
Linear	$\lambda$ /2 0.316 micron (12.44 microinches)
Plane Mirror	$\lambda$ /4 0.158 micron (6.32 microinches)
High Resolution Plane Mirror	$\lambda$ /8 0.079 micron (3.12 microinches)

Table 4 Interferometer Resolutions

## Range

The nominal optical measurement range for an Agilent laser measurement system is usually 40 meters (130 feet) for the sum of all axes. In calibrator systems, this range may be doubled with the Agilent 5519A/B optional long range kit.

The 3 mm diameter beam of the Agilent 5517C-003 Laser Head allows a maximum range of 10 meters (32 feet) for the sum of all axes.

### **Measurement Direction Sense**

Direction sense depends on the relation of the optical frequencies in the interferometer's reference and measurement paths. This, in turn, depends on: 1) the orientation of the laser head, 2) the effect of any beam-bending optics in the path between the laser head and the interferometer, 3) the interferometer's configuration (straight-through or turned), and 4) the orientation of the interferometer itself.

For example, if: 1)  $f_1$  (the lower frequency from the laser head) is in the measurement path (that is, the path going to the measurement mirror), and 2)  $f_2$  (the higher frequency from the laser head) is in the reference path (that is, the path going to the reference mirror), 3) the measurement optics are moving away from each other, the fringe counts will be INCREASING.

Interchanging  $f_1$  and  $f_2$  will reverse the direction sense, resulting in the fringe counts DECREASING as measurement optics move away from each other.

In this manual, " $f_1$ " and " $f_2$ " have been used to identify the two frequency components of the laser beam. However, because the components that left the laser head having horizontal and vertical orientations can have the opposite orientations when they arrive at an interferometer, " $f_A$ " and " $f_B$ " are used to identify the beam paths through the interferometers. Figure 35 shows how two parallel beams, derived from the same source, can have different polarization orientations at interferometer inputs. An interferometer using one of these beams will produce increasing counts as its measurement mirror moves away from it; an identical interferometer, parallel to the first, but using the second beam, will produce decreasing counts as its measurement mirror moves away.

#### VERTICAL AND HORIZONTAL POLARIZATION

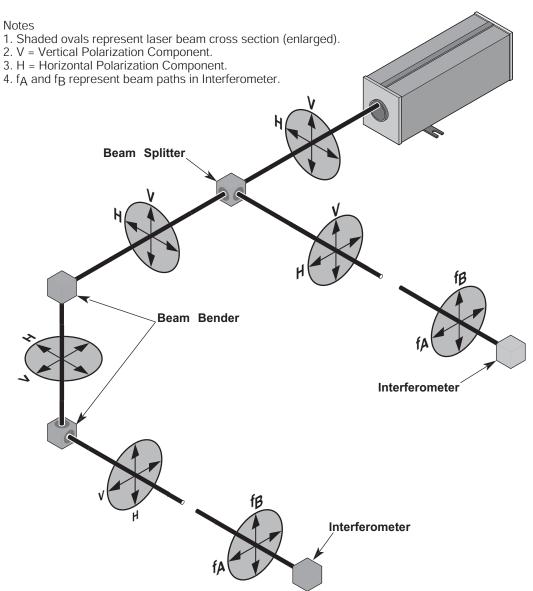


Figure 35 Effect of beam-directing optics on laser beam polarization orientations

## **Vibration Isolation**

Vibration of the optics along the laser beam can cause the fringe count in the laser measurement system electronics to fluctuate rapidly. Vibrations along this axis constitute real, measurable, displacements; you will have to decide if these fluctuating measurements are acceptable in your application. In extreme cases, however, the velocity of the optics may momentarily exceed the velocity limitation of the laser measurement system, causing an error.

When vibration occurs perpendicular to the beam, the beam signal power can fluctuate. If this fluctuation is too great, insufficient beam signal will arrive at the receivers, causing a "measurement signal error."

Loose mounting can cause the optics to move inappropriately during a measurement, causing a measurement error or loss of beam power.

Elastic mounting can have the same effect as loose mounting. It can also be responsible for a "sag" offset in the optics' positions. If there is vibration in the machine, an elastic mounting can transmit and amplify the vibration to the attached optic, possibly causing more errors. You should anticipate these effects and minimize them, if necessary, during the laser measurement system design process.

Certain interferometers are inherently less susceptible to vibration effects than others. This is particularly true of differential-style interferometers such as the Agilent 10715A, Agilent 10719A, and Agilent 10721A. The stability of these interferometers is due to the fact that both their reference beams and their measurement beams travel to external mirrors. Any motion of the interferometer itself that is common to both beams will not appear as a measurement. Of course, any vibration between the reference and mirrors will constitute real, measurable, displacements.

### Fasteners

Any optical component that fits an adjustable mount is supplied with mounting screws to mount it on the appropriate adjustable mount.

### Vacuum Applications

Many of the optical components of the laser measurement system have vacuum options, which are compatible with vacuum environments. Contact Agilent Call Center for information (telephone numbers of various call centers are listed on the "Service and Support" page at the back of this manual). Typically, these components have housings made of stainless steel and optical elements attached to the housings using a lower volatility (vacuum-grade) adhesive. See the specifications for a list of materials used in the optics.

### Use Through Window

If the laser beam has to go through a window (for example into a vacuum chamber) the window must meet the following requirements:

- A minimum window aperture of 25.4 mm (1 inch) with a minimum thickness of 8 mm (0.3 inch). If a larger window is used, it must be proportionally thicker to assure no distortion in the window when under differential pressures.
- Transmitted wavefront distortion less than  $\lambda/10$  (peak-valley, single-pass) over a 23 mm (0.9 inch) diameter.
- Parallelism of faces less than ±2 arc-minutes, to reduce beam steering.
- Surface quality 60-40 or better, per Mil-0-13830.
- The window must be strain-free.

### **Differential Measurements with Interferometers**

Several interferometers have the capability to make differential measurements. A differential, measurement is one in which both the reference beam and the measurement beam travel to external mirrors outside the interferometer housing. This allows measurement of the relative positions of the two external mirrors, either or both of which may be moving. Viewed another way, this allows measuring the motion of one reflector relative to a reference datum elsewhere in the machine, external to the interferometer itself. This is unlike the typical interferometer configuration because usually the *reference* beam path length does not change; in differential configurations, it can.

One useful example of a differential measurement in a lithography application is for measuring the motion of the X-Y stage relative to the optical column. The Agilent 10719A One-Axis Differential Interferometer and the Agilent 10721A Two-Axis Differential Interferometer are ideally suited to this type of measurement, because they provide parallel reference and measurement paths which are offset vertically by 19 mm (0.750 inch). For such an application, a user-supplied reference plane mirror is required in addition to the measurement reflector on the X-Y stage.

Differential measurements that can be made using an Agilent 10719A interferometer are shown in Figure 170 in Volume II of this manual. Differential measurements that can be made using an Agilent 10721A interferometer are shown in Figure 178.

The Agilent 10715A Differential Interferometer, instead of having an offset spacing as in the Agilent 10719A or Agilent 10721A interferometers, permits the reference beams and the measurement beams to be aligned essentially coaxially. A specially-shaped reference plane mirror (shown in Figure 144) is supplied with the Agilent 10715A. For more information about the Agilent 10715A, see Chapter 22, "Agilent 10715A Differential Interferometer," in Volume II of this manual.

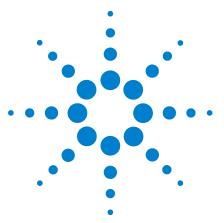
Customized differential configurations are possible with several other interferometers. However, considerable care should be exercised during design and layout to avoid introduction of alignment errors, thermal or mechanical instabilities, and potential deadpath problems. When making differential measurements, both reflectors (reference and measurement) should be of the same type (cube corner or plane mirror); this minimizes thermal drift problems with ambient temperature changes.

To use the Agilent 10702A, Agilent 10705A, or Agilent 10766A in a differential configuration, the reference cube corner can simply be detached from the interferometer housing and attached to the reference surface of interest. This is shown in Figure 105 in the Linear Interferometers chapter (Chapter 18) of this manual. Be aware that all installation and alignment requirements for the measurement reflector now apply also to the reference reflector.

To use the Agilent 10706A or Agilent 10706B interferometer in a differential configuration, a plane mirror is recommended as the reference reflector. Simply replace the reference cube corner (or high-stability adapter) with the Agilent 10722A Plane Mirror Converter and attach the reference plane mirror to the reference surface of interest. This is shown in Figure 121 in the plane mirror chapter (Chapter 20) of this manual. Again, install and align the reference reflector the same as you would the measurement reflector.

## **Moving Interferometer Instead of Reflector**

When moving the interferometer instead of the measurement reflector is required, the Agilent 10702A-001 (or Agilent 10766A) should be used. In practice, for alignment reasons, these are the only interferometers (except the straightness interferometers) that can be moved while making measurements. For a detailed explanation of why this option is required, see Figure 100 in the Linear Interferometers chapter (Chapter 18) in Volume II of this manual.



Agilent Laser and Optics User's Manual Volume I

# 6 NGI Measurement Optics (General Information)

Introduction, 118 NGI Optical Schematic, 120 NGI Angular Resolution, 121 Alignment and Mounting, 123 Measure Point Tolerance, 129 Fiber Optic Interface Specifications, 130



## Introduction

The Next Generation Interferometer (NGI) differs from previous interferometers due to its monolithic structure. The optical elements (i.e., quarter-wave plates, cube corners, and input rhomboids) are optically cemented or contacted directly onto the polarizing beam-splitter (PBS) surfaces. Also, the quarter-wave plates have highly reflective (HR) coatings that serve as reference mirrors. The reference beam path then remains inside the interferometer without crossing any air interfaces; hence, this eliminates most external mounting parts, and increases measurement stability by avoiding thermal expansion problems. The overall optical structure is condensed.

The input laser beam has two polarizations that are orthogonal to each other. Nonpolarizing beam-splitters composed of rhomboid/prism and sometimes spacer assemblies are used to split an input laser beam into two separate beams according to power level and beam pattern. An example beam-splitting percentage is 50% and 50%, where the ratio of S to P polarization is unaffected. The distance between separate beams is determined by the rhomboid length, which is adjustable for each design. The input splitting optics and coatings are configured (by design) to support many beam pattern and power level requirements.

This chapter provides:

- a list of next-generation measurement optics in order by Agilent Model Number (Table 5). The table also: 1) identifies the chapter in which each measurement optic is described, and 2) provides summary descriptions of the measurement optics
- an optical schematic of the Agilent NGI (Figure 36)
- a diagram of angular resolution of the Agilent NGI (Figure 37)
- procedures for aligning and mounting the NGI (page 123)
- fiber optics specifications (page 130)

Chapters 31 through 34, in Volume II of this manual, provide complete descriptions of the different NGI interferometer models.

Table 5 lists and summarizes the Agilent NGI interferometers. All of the NGIs products are *dual-pass interferometers* and hence have an optical resolution of  $\lambda/4$ . Depending on the resolution extension, the measurement resolution can go down to 0.15 nm.

Manual Chapter	Model Number and Name	Number Axes	Beam Diameter	Optical Resolution	Typical Optical Efficiency (Input power/axis output power)	Base Plate Material	Mass
31	Agilent E1826E/F/G	1	φ9 mm, maximum (visible)	λ/4	65%	Invar (Option 070), Passivated 416 Stainless Steel (Option 071)	0.40 kg (.89 lbs)
32	Agilent E1827A	2	φ9 mm, maximum (visible)	λ/4	All axes = 26%	Passivated 416 Stainless Steel	2.35 kg (5.22 lbs)
33	Agilent E1837A	3	φ9 mm, maximum (visible)	λ/4	All axes = 18%	Passivated 416 Stainless Steel	2.67 kg (5.93 lbs)
33	Agilent Z4399A	3	φ9 mm, maximum (visible)	λ/4	All axes = 18%	Invar	1.66 kg (3.65 lbs)
33	Agilent Z4422B	3	φ9 mm, maximum (visible)	λ/4	Axis 3 = 13% Axes 1 and 2 = 18%	Passivated 416 Stainless Steel	1.95 kg (4.3 lbs)
34	Agilent Z4420B	5	φ9 mm, maximum (visible)	λ/4	Axis 5 = 7% Axes 1 thru 4 = 10%	Passivated 416 Stainless Steel	3.13 kg (6.9 lbs)
34	Agilent Z4421B	5	φ9 mm, maximum (visible)	λ/4	Axis 5 = 7% Axes 1 thru 4 = 10%	Passivated 416 Stainless Steel	3.15 kg (7 lbs)

#### Table 5 NGI Interferometers summary

## **NGI Optical Schematic**

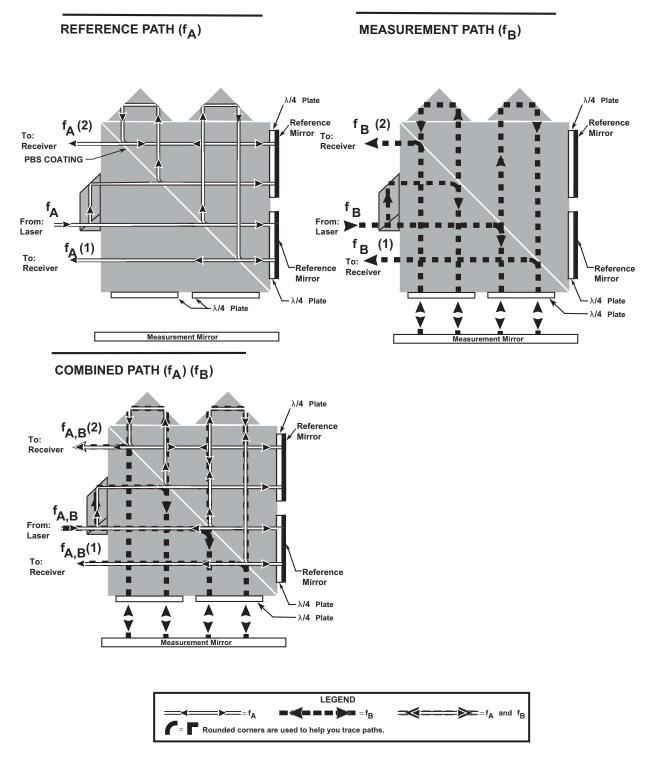


Figure 36 Next Generation Interferometer laser beam path

### **NGI Angular Resolution**

The angular resolution can be calculated by using the following equation:

$$\alpha = \frac{\Delta x}{d} = \frac{\text{Linear resolution}}{\text{Beam separation}}$$

Where (see Figure 37 on page 122):

- $\Delta x$  = the position change of the stage (linear resolution)
  - d = the distant between the measure points (distance between the image at the cube corners' apexes on the measurement mirror)

The distance between the measurement points (d) will vary due to several factors. If you do not compensate for these factors with a system calibration step, you can estimate the angular resolution error by considering all of the contributing tolerances. The tolerances that affect the distance between the measurement points on the measurement mirror (where the image of the cube corners' apexes will be located on the measurement mirror) are as follows:

- error due to beam parallelism (e.g., 25 µradians)
- error due to beam primary to secondary parallelism (e.g., 15 µradians)
- error due to initial alignment (e.g., data alignment, input beam alignment)
- error due to cube corner positions (e.g., 50 µmeters)

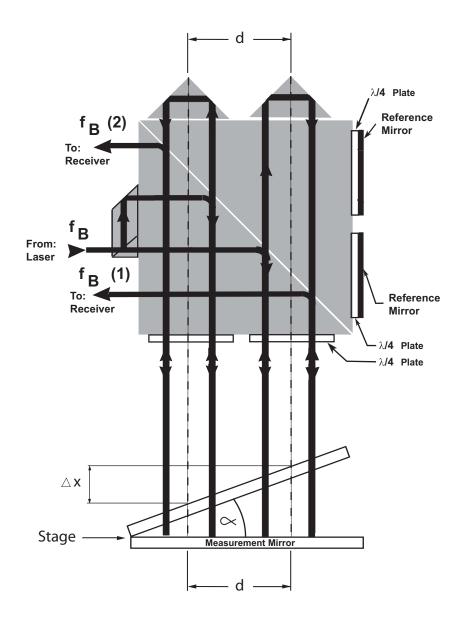


Figure 37 NGI Angular Resolution diagram

### **Alignment and Mounting**

### General

Before any interferometer is installed, a suitable mounting location must be prepared for it. The interferometer's mounting location defines the relationship of its measurement beams to the stage whose motion is to be measured. Preparing a proper mounting location minimizes initial beam walkoff. The following information in this section will allow you to design and build a mounting location for a next generation interferometer.

### **Procedure**

The Agilent Next Generation interferometers installation can be performed in four parts.

- 1 Adjust stage angle to the system zero stage angles (see the "Ideal zero stage angles", "Determining system zero stage angles", and "Effect of misalignment" subsections).
- 2 Mount the interferometers (see the "Mounting the interferometers" subsection).
- 3 Adjust the input beam angle to be normal to the stage, see the "Adjusting the input beam angle" subsection).
- 4 Translate the input beam to the center of the primary remote sensor (see "Beam translation alignment" subsection).

#### Ideal zero stage angles

To minimize beam walkoff, the stage mirror should ideally be aligned to the ideal zero stage angle using the interferometer's datums; the ideal zero stage angle is when the stage mirror is normal to the A datum and parallel to the B datum of the interferometers as shown in Figure 38.

The mounting surface (A datum) shall be a similar material to the interferometer baseplate or have similar coefficients of thermal expansion (CTE). This mounting surface should be prepared to have a surface profile of 20  $\mu$ m and surface finish of 0.4  $\mu$ m or better. Please contact Agilent to discuss alternatives for mounting to materials that do not match the baseplate CTE.

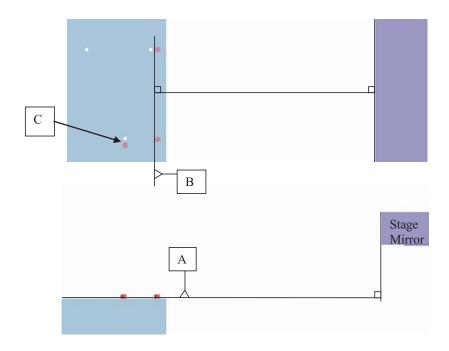


Figure 38 Interferometer datums relative to ideal zero stage angles

#### Determining system zero stage angles

Assuming the system zero stage angle is ideal, one method is to use large true squares as shown in Figure 39. First, position true squares firmly against the interferometers' datums, namely A and B. An autocollimator can then determine the relative angle between the true squares (representing the interferometer datums) and the stage mirror. The true squares are then removed and the interferometers mounted.

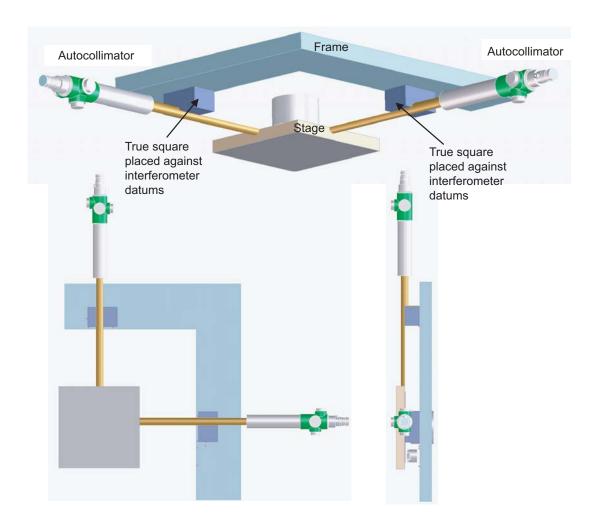


Figure 39 Setup for determining system zero stage angles

#### Effect of misalignment

The interferometers' datums will have slight tolerances between them. The two orthogonal mirrors on the stage will also have a tolerance on their orthogonality. Hence, the system zero stage angle between the stage mirror and the interferometer's datums will not be ideal.

Once the stage angle has been adjusted to the system zero stage angles, the stage angle range will be reduced 1  $\mu rad$  for every 10  $\mu rad$  of datum misalignment from ideal.

#### Mounting the interferometers

The Agilent interferometer is to be placed on the plane (A datum, the mounting surface), slid on the plane into position along the line (B datum, created by two dowels), and finally slid along the line, on the plane, to the stopping point (C datum, created by a single dowel). See Figure 40.

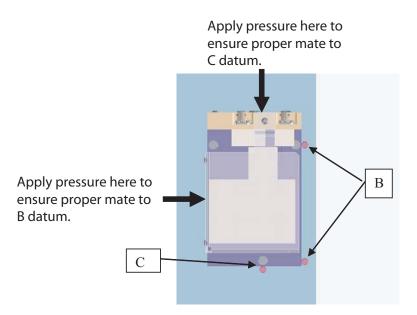


Figure 40 Interferometer mounting

The interferometers must stabilize to the frame temperature before mounting bolts are tightened<sup>1</sup>.

Approximately 44 Newtons should be continuously applied on the interferometer in the two positions shown in Figure 40 to ensure proper mate to the B and C datums. Torque each of the three screws as listed in Table 6.

<sup>&</sup>lt;sup>1</sup> The interferometer can be stabilized by attaching it to the frame, tightening screws to ~0.5 newton-m, and waiting >1 hour. Then loosen screw and tighten to final torque.

Screw Size	Torque
M3	1 Nm
M4	2.4 Nm
M5	5 Nm

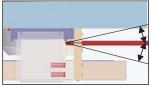
Table 6Screw Torque Requirement

### Adjusting the input beam angle

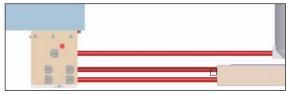
**Input beam angles for ideal zero stage angles** Assuming the system zero stage angles are ideal, the input beam has a unique angle that is not perfectly normal due to glass tolerances. This unique input beam angle that minimizes initial beam walkoff and maximizes the stage angle range will fall within the input beam cone angle (IBCA). If the system zero stage angles are ideal, meaning that the stage mirror is square to the datums, the only input beam angular adjustment necessary would be the IBCA.

Assuming ideal zero stage angle, to find the unique input beam angle, two conditions must exist:

- The measurement mirror must be perpendicular to datum A and parallel to datum B of the mounting location, which is the ideal zero stage angle.
- The interferometer's measurement axis' primary beam must be perpendicular to the measurement mirror.



Distinct pitch angle of input beam ranges < 1 mrad for the interferometer.



Distinct yaw angle of input beam ranges < 1 mrad for the interferometer.

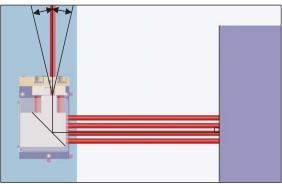


Figure 41 Input beam cone angle for ideal zero stage angles

**Input beam angles for system zero stage angles** There are still tolerances between the orthogonal stage measurement mirrors and the A and B datums, meaning that the system zero stage angle would not be ideal. Therefore, to account for both the tolerance in the glass and the tolerances in the system's alignment to the datums, this latter tolerance must be added to the IBCA. The beam directing optics must be able to manipulate the input laser beam such that its angular adjustment range includes the sum of the tolerances.

The stage angle range will be reduced 1  $\mu rad$  for every 1  $\mu rad$  of input beam misalignment.

**Beam translation alignment** The input beam position should be translated to the center of the input aperture once the input angle is set. This provides the maximum angular range.

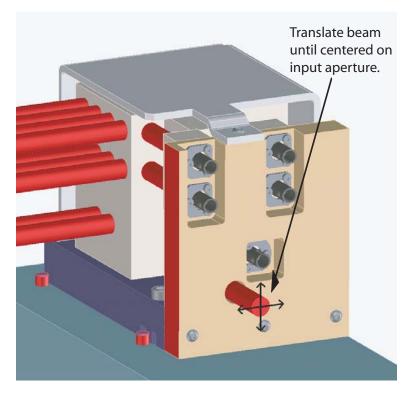


Figure 42 Input Beam Position Adjustment

**Manipulator requirements** The beam directing optics must be able to manipulate the input laser beam to the center of the interferometer's input aperture with total input beam angle.

## **Measure Point Tolerance**

Measure point tolerance defines the tolerance of the location of the apex of each cube corner relative to each other (deviation tolerance) and their average locations to the interferometer datums (mean tolerance). The *mean offset* is defined by the average of all cube corner actual offsets relative to the datums in a multi-axis interferometer. Individual cube corner's *deviation offset* is defined by the distance each cube corner is actually located relative to its nominal position shifted by the mean offset.

This tolerance is important for achieving repeatable and known measure point positions from unit to unit on a customer system. The alignment system metrology may rely on this in order to define abbé offsets and define angles calculated by measurements made by two interferometer axes (i.e., Pitch or Yaw). The accuracy of the measure point locations also affects the beam locations and should be considered when sizing the measurement mirror(s).

The measure point mean and deviation tolerances are shown in Figure 43, using a five-axis interferometer as an example.

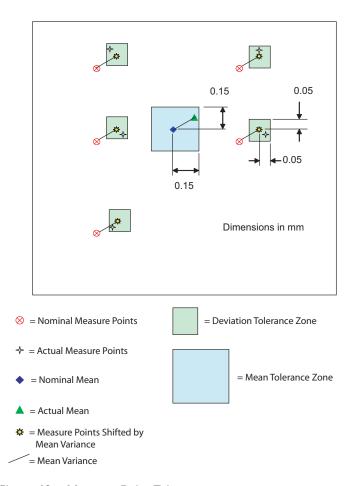


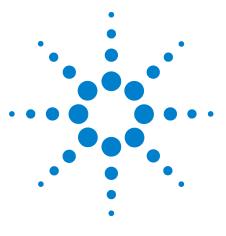
Figure 43 Measure Point Tolerance

## **Fiber Optic Interface Specifications**

NGI interferometers have integral remote sensors with ST connectors, eliminating the need to mount separate remote sensors. The ST connectors are pre-aligned at the factory so the customer will only need to connect the fiber optic cables. Both plastic and glass fibers with ST connectors can be used, which can be obtained from Agilent. Multiple lengths are available for your requirements.

If an ST type bulk head feedthrough is necessary for connecting the fibers, customers can use AMP's 504021-1 Fiber Optic Connectors ST Coupling Receptacle.

Plastic Fibers:	
Bending radius	35 mm minimum
Connectors available	ST to V-pin (Agilent E1705B) and ST to ST (Agilent E1705C)
Attenuation	approximately 190 dB/km
Glass Fibers:	
Bending radius	47 mm minimum
Connectors available	ST to V-pin (Agilent E1705E) and ST to ST (Agilent E1705F)
Attenuation	approximately 12 dB/km



Agilent Laser and Optics User's Manual Volume I

# Maintenance

7

General, 132 Procedures for Cleaning Optics, 132 Maintenance Procedures, 135



## General

Periodically inspect the laser head, optical components, receivers, and associated items, for indication of mechanical or electrical defect. Look for signs of overheating, corrosion, accumulations of dust, oil, loose electrical connections, or broken parts. Also check the Agilent 10780F Remote Receiver, Agilent E1708A Dynamic Remote Receiver, and the Agilent E1709A Remote High-Performance Receiver for loose fiber optic connections at both ends of the fiber.

Repair any obvious defect. If necessary, clean the unit with dry, clean compressed air or a vacuum cleaner.

CAUTION	Do not use compressed air on an Agilent 10719A, Agilent 10721A, Agilent 10735A, Agilent 10736A, or Agilent 10736A-001 interferometer. The units may be damaged by use of compressed air.
CAUTION	To avoid scratching an optical device during cleaning, use the optics cleaning procedures below.

Periodically you may wish to verify proper beam alignment. Refer to Chapter 4, "System Installation and Alignment," in this manual or the alignment procedure(s) for the optics in your measurement system for the appropriate procedure.

## **Procedures for Cleaning Optics**

### WARNING

The following optical cleaning procedures do not apply to the optics of the laser head. Cleaning the laser head optics is rarely needed and requires access to the laser head interior where high voltages can be present. All laser head maintenance should be performed by a qualified Agilent technician who is aware of the hazards involved.

### **Agilent Receivers**

Use a soft camel-hair lens brush or equivalent to remove dust from the optical surfaces. Dampen a few lens cleaning tissues with electronics grade methanol, shake off excessive methanol and wipe across the lens surface once. Use a fresh tissue dampened with methanol for each wipe. Allow the methanol to evaporate.

#### CAUTION

Do not use any solvent, for any purpose, on the Agilent 10780F, E1708A, or E1709A receivers' fiber-optic cable. Using a solvent on the fiber-optic cable may damage the cable.

The ends of the Agilent 10780F, E1708A, and E1709A receivers' fiber-optic cable may be cleaned with a clean lint-free cloth.

### Measurement optics and beam-directing optics

If the optical surfaces of an instrument are visibly dirty, the following cleaning procedures should be used.

The optics should be handled with care so nothing comes in contact with the optical surfaces. Fingerprints will collect dust and dirt which will attenuate and disperse the laser beam. Also, acids in fingerprints may etch glass or the optical coating. In general, preventing contamination of optics is preferable to cleaning them. Cleaning the optics should be avoided unless the signal intensity of the beam is noticeably reduced.

If cleaning the optics is required, be careful to avoid rubbing particles into the coated surfaces. Permanent reduction of signal intensity could result. If particles are observed on the optics surface, remove them by blowing off with clean pressurized air or (preferably) dry nitrogen. If these are unavailable, commercially available products such as Kodak<sup>®</sup> Laboratory Sprayer or Micro Duster TX 600 from the Texwipe Company<sup>®</sup> may be used.

#### CAUTION

Cleaning optics with tissues or pressurized air is recommended only for exposed glass surfaces that are easily accessible to the user. DO NOT TRY TO CLEAN ANY OPTICAL SURFACE LOCATED INSIDE AN OPTIC HOUSING. Some interferometers contain fragile optical components which are deliberately mounted internally for protection. DO NOT TRY TO DEFEAT THIS PROTECTION. Optical surfaces which cannot be easily viewed or reached should NEVER be cleaned, either with a tissue or with pressurized air.

Example 1:	The Agilent 10719A and Agilent 10721A interferometers have only ONE user-accessible optic—the external window facing the measurement and reference reflectors. This may be cleaned, if necessary, by wiping with lens tissue or cloth. DO NOT try to clean or blow into any other housing aperture, since this may cause damage to the internal optics.
Example 2:	The Agilent 10735A, Agilent 10736A, and Agilent 10736A-001 interferometers have NO user-accessible optics. DO NOT try to clean or blow into any housing aperture, since this may cause damage to the internal optics.

### Lens tissue

#### CAUTION

For an Agilent 10735A, Agilent 10736A, or Agilent 10736A-001 interferometer, you must not try to clean or blow into any housing aperture, since doing so may damage the optics.

For an Agilent 10719A or Agilent 10721A interferometer, the only opening you may try to clean without possibly damaging the internal optics is the window facing the measurement and reference reflectors. Some optics (see list below) are shipped with a package of lens tissue which is made specifically for cleaning optics. Use these tissues (or equivalent) with a pure industrial grade methanol in the following manner:

- 1 Fold the tissue into an approximate 1-inch (25 mm) square.
- 2 Wet the tissue with methanol (do not saturate) and gently wipe across the optical surfaces. Use only enough pressure to remove the contaminant.
- 3 Do not reuse the tissue.
- 4 For additional cleaning, repeat the process using a new tissue.

Except as described in the CAUTION above for the Agilent 10719A, Agilent 10721A, Agilent 10735A, Agilent 10736A, or Agilent 10736A-001 interferometers, which may be damaged by incorrect attempts at cleaning, for external optical surfaces that are hard to reach, the tissue may be held with a clamping tweezer such as a hemostatic forceps. Alternatively, a cotton-tipped swab may be used. Take care not to scratch the coated surface. Do not scrub the surface with a dry tissue.

### Alcohol

Avoid alcohol contamination with the following precautions:

- 1 Use only new, previously unopened containers. Alcohol absorbs water if left exposed to air. This will result in water spots when the alcohol evaporates.
- 2 Transfer the alcohol to a squeeze bottle that can be capped and made airtight.
- 3 Never transfer alcohol back into the original container.

## **Maintenance Procedures**

Each laser head and receiver are shipped with their own service manual, which contains the adjustments and checks required to keep each respective laser head and receiver at peak performance. Included in the manual are the test equipment required, equipment setups, and procedures to perform the adjustments.

### **Before and After Service Product Safety Check**

The following safety checks must be performed after any troubleshooting and repair procedures have been completed, to ensure the safe operation of the instrument.

#### WARNING

Resistance checks described below require that the power cord be connected to the instrument and that AC power be disconnected. Be sure that the power cord is not connected to power before performing any safety checks.

- 1 VISUAL INSPECTION. Visually inspect the interior of the serviced instrument for signs of abnormal internally generated heat, such as discolored printed circuit boards or components, damaged insulation, or evidence of arcing. Determine and remedy the cause of any such condition.
- 2 GROUND CONTINUITY TEST. Plug the power cord into the Agilent electronics. DO NOT CONNECT THE INSTRUMENT TO AC POWER. Using a suitable ohmmeter, check the resistance from the enclosure (chassis) to the ground pin on the power cord. The reading should be less than 1 ohm. Flex the power cord while making this measurement to determine whether intermittent discontinuities exist. The resistance check should be performed from the enclosure to the ground pin of the cord while flexing the interconnect cable.
- 3 Check any indicated front- or rear-panel ground terminals using the above procedures.
- 4 INSULATION RESISTANCE CHECK. Tie the line and neutral pins of the power cable together. Check resistance from the instrument enclosure (chassis) to line and neutral with the LINE switch ON and the power source disconnected. The minimum acceptable resistance is 2 Megohms. Replace any component that results in a failure.
- 5 POWER LINE MODULE CHECK. Check line fuse and line voltage selector in the electronics rear-panel power line module to verify that the correct fuse is installed and that the instrument is properly set for the AC source to be applied.



Agilent Laser and Optics User's Manual Volume I

# 8 Troubleshooting

Introduction, 138 Troubleshooting Assumptions, 139 Electrostatic Discharge (ESD), 140 Required Test Equipment, 140 Troubleshooting Information, 141 Before and After Service Product Safety Check, 151



## Introduction

This chapter provides information to help you find defective components in an Agilent laser measurement system when a problem occurs. It can help determine whether the problem source is in the system electronics, environmental sensor, laser head, receiver, or the optics.

Component-level troubleshooting and calibration should be performed by Agilent Technologies technicians only. However, component-level troubleshooting and calibration information is provided for selected assemblies. This chapter is structured as indicated in Table 7.

Instrument	Type of Information
Laser Heads	System-level troubleshooting for isolating the fault to the laser head
Agilent 10780C, 10780F, E1708A, or E1709A	System-level troubleshooting for isolating the fault to a receiver
Agilent 107XX Optics	System-level troubleshooting for isolating the fault to the optical assemblies. The Agilent 107XX optics are repairable only by Agilent Technologies.

Table 7Chapter content summary

Additional information is provided in the manuals that are supplied with each instrument.

## **Troubleshooting Assumptions**

The troubleshooting procedures assume that:

- 1 The system controller is operating properly. Before connecting the system controller to the Agilent electronics, check the controller by:
  - a Booting the unit up and verifying appropriate responses,
  - b Running your own known good programs, and
  - c Executing any controller diagnostics unique to your particular controller.
- 2 All system controls have been double-checked to verify that they are in the proper positions. This includes the correct setting of all circuit board address and test switches. (See "Preliminary Checks" (or similar information) in the troubleshooting chapter of your electronics manual.)
- 3 All system cabling is configured correctly and that all cables are making proper electrical connection.
- 4 The system optics are clean. Refer to Chapter 7, "Maintenance," in this manual.
- 5 Power to the system is removed before replacing any units or circuit boards.
- 6 You adhere to the precautions outlined in "Electrostatic Discharge (ESD)" section of this chapter.
- 7 The troubleshooting procedures cannot cover all possible malfunctions or combination of malfunctions. However, at the very minimum, these procedures will direct you to the general area of the problem.

#### WARNING

Use of controls, adjustments, or procedures other than those specified herein may result in hazardous laser light exposure or exposure to high voltages.

# **Electrostatic Discharge (ESD)**

Electronic components and assemblies can be permanently damaged by electrostatic discharge. To avoid damage caused by ESD, follow the following precautions:

- 1 Ensure that static-sensitive devices or assemblies are serviced at static-safe work stations providing the proper grounding for personnel (e.g., table mat with wrist strap).
- 2 Ensure that static-sensitive devices or assemblies are stored in static-shielding containers (e.g., antistatic poly bags).
- 3 Do not wear clothing subject to static charge build-up, such as wool or synthetic materials.
- 4 Do not handle components or assemblies in carpeted areas, Do not remove the component or assembly from its static protective container until you are ready to install it.
- 5 Avoid touching component leads or assembly edge connectors with your fingers.

## **Required Test Equipment**

The equipment required to maintain the laser heads and receivers is listed in Table 8. Other equipment may be substituted if it meets or exceeds the critical specifications listed in the table. Refer to the appropriate electronics manual for a list of test equipment required for electronics maintenance and the calibration of environmental sensors (Agilent 10751C or Agilent 10751D Air Sensor and 10757D, Agilent 10757E, or Agilent 10757F Material Temperature Sensor).

Table 8	Recommended test equipment
---------	----------------------------

Instrument Required	Characteristics	Model Number
Laser Power Meter	Range: 1 microwatt to 1 milliwatt Accuracy: ± 10%	Coherent Inc. ® Ultima Labmaster or equivalent
Digital Voltmeter	Range: $-15V$ to $+15V \pm 0.01$ Vdc NOTE: Accurary of $\pm 0.01$ Vdc required for voltage adjustments.	Agilent 34401A
Oscilloscope	Ability to display signals between dc and 100 MHz.	Agilent 54624A
Clip-on DC Milliammeter	DC Current Range: 1mA to 10A (fullscale) Accuracy: ±3% of full scale ±0.15 mA	Agilent 34401A

# **Troubleshooting Information**

The possible system problems that can occur can be divided into the following areas:

- Malfunction of the laser head.
- Malfunction of one or more receivers.
- Malfunction, misalignment, or improper application of the optical devices.
- Malfunction of the system controller or its improper programming.
- Malfunction of the Agilent system electronics.

If one of these areas is suspect as the source of the trouble, refer to the appropriate troubleshooting information and flowcharts (provided in this section) for that particular area.

## Laser Head troubleshooting

#### Agilent 5517A/B/BL/C/D/DL/FL Laser Head

Laser heads are listed here in the same order in which they are listed in Chapter 16, "Laser Heads," in Volume II of this manual.

Laser head adjustment procedures are given in the laser head's own operating and service manual.

The following symptoms indicate problems with the Agilent 5517A, Agilent 5517B, Agilent 5517BL, Agilent 5517C, Agilent 5517D, Agilent 5517DL, or Agilent 5517FL Laser Head. If one or more of these symptoms are observed, use the Troubleshooting Tree, Figure 44, to assist in determining if the laser head is actually at fault. Detailed repair procedures are outlined in the laser head's operating and service manual.

- No laser light being emitted from the laser head exit port.
- Low power output from the laser head.
- LASER ON indicator not lit.
- READY indicator does not illuminate as expected. Normally, the indicator will start to blink on and off within three minutes of applying power to the laser head. This indicates that the laser head is in the process of warming up. When the 5517A, 5517B, 5517BL, 5517C, 5517D, 5517DL, or 5517FLLaser Head is ready for use, the indicator assumes a steady on condition.
- Absence of reference signal or bad reference signal.
- Agilent 5517B/BL/C/D/DL/FL Laser Head's +15V POWER ON or -15V POWER ON indicator is not lit.

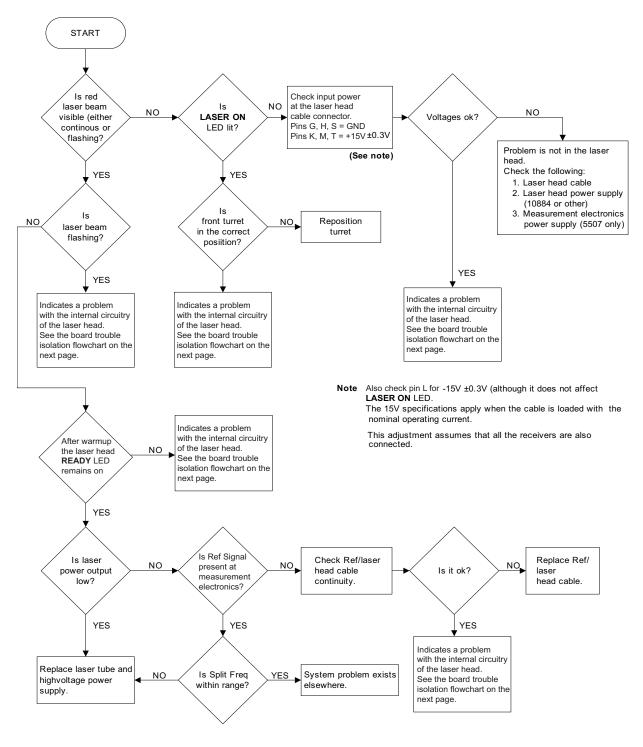


Figure 44 Agilent 5517A/B/C/D Laser Head—troubleshooting tree

#### Agilent 5519A/B Laser Head

See the *Agilent 5519A/B Laser Head Service Manual* for laser head troubleshooting information.

#### **Receiver troubleshooting**

#### Agilent 10780C, 10780F, E1708A, E1709A Receiver

NOTE	This section is basically written for troubleshooting the Agilent 10780C/F receiver, but many of the same techniques can be used to troubleshoot the Agilent E1708A or E1709A receiver. For troubleshooting information specific to the Agilent E1708A or E1709A receiver, see their respective operating manuals.
NOTE	Allow the laser head sufficient time to complete its tuning cycle prior to determining whether or not the Agilent 10780C, Agilent 10780F, Agilent E1708A, or Agilent E1709A receiver is working properly.

When the Agilent 10780C/F receiver photodetector receives an adequate laser beam signal, the LED indicator illuminates (located on the Receiver's top surface) and the DC voltage at the external beam monitor test point is greater than +0.7. See the "Alignment and Gain Adjustment Procedure" in Chapter 35, Receivers," in Volume II of this manual for procedures to adjust this test point voltage. The alignment and gain adjustment procedures for the Agilent E1708A or E1709A receiver can be found in their respective operating manuals.

If the MEASUREMENT SIGNAL ERROR indicator on the Agilent electronics illuminates, the problem may be with one of the system's measurement axis receivers. If a SYSTEM ERROR indicator illuminates and the system is equipped with a Wavelength Tracking Compensation system, the problem could be with the wavelength tracker axis receiver or the overall alignment of the Wavelength Tracking Compensation system components. By sending an error message query to the Agilent electronics via the system controller, the system will respond indicating which axis is generating the error message.

Improperly aligned optical devices in either a measurement or a wavelength tracking axis can also cause a receiver to appear bad. Check for this by either placing the receiver directly in the laser beam path from the laser head, or by reflecting the laser beam onto the receiver's photodetector using a retroreflector. This isolates all other optical devices from the system. Most systems contain more than one axis and, consequently, more than one receiver. If trouble is suspected with one particular receiver, exchange it with another receiver to verify the suspected malfunction. If you suspect problems with the alignment of a receiver, refer to Chapter 35, Receivers," and Chapter 5, "Measurement Optics (General Information)," in this manual for the appropriate alignment procedures.

A loose or broken fiber-optic connection at either the remote lens or electronics of the Agilent 10780F Remote Receiver, Agilent E1708A, or Agilent E1709A can also cause the receiver to appear bad.

The receiver LED indicator may remain on even if the beam between the interferometer and the retroreflector is blocked. This can occur occasionally with correct optical alignment if the measurement path is very short and few optical devices are used in the measurement path. If this situation occurs, refer to the receiver's operating and service manual.

The troubleshooting tree of Figure 45 will help you determine if the Agilent 10780C Receiver, Agilent 10780F Remote Receiver is faulty. Repair of the Agilent 10780C or Agilent 10780F is outlined in the *Agilent 10780C/F Operating and Service Manual*. Table 9 shows the Agilent 10780C/F Receiver signal chart.

Receiver Input Output	Signal Name		
J1(1)	MEAS		
J1(2)	MEAS		
J1(3)	+15V Return RET		
J1(4)	+15V		
Pin	Wire Color	Signal	
1	BLK	MEAS FREQ—	
2	WHT	MEAS FREQ	
3	WHT/GRA	+15V RETURN	
4	WHT/GRA/GRN	+15V	
NOTE: A dash (—) following a signal name indicates a negative-true signal.			

Table 9 Agilent 10780C or Agilent 10780F Receiver signal chart

The receivers should be inspected at least twice a year, depending on their operating environment. Inspect as follows:

- VISUAL INSPECTION Inspect the unit for indication of mechanical and electrical defects. Look for signs of overheating, corrosion, accumulations of dust, oil, loose electrical connections, or broken parts. Also check the Agilent 10780F Remote Receiver for loose fiber-optic connections at both ends of the fiber.
- REPAIR AND CLEANING Repair any obvious defects; and if necessary, clean the unit with dry, clean compressed air or a vacuum cleaner.

#### CAUTION

To avoid scratching the lens during cleaning, the following procedure is recommended.

Use a soft camel-hair lens brush or equivalent to remove dust from the optical surfaces. Dampen a few lens cleaning tissues with electronics grade methanol, shake off excessive methanol and wipe across the lens surface once. Use a fresh tissue dampened with methanol for each wipe. Allow the methanol to evaporate.

The ends of the Agilent 10780F, Agilent E1708A, or Agilent E1709A fiber-optic cable may be cleaned with a clean lint free cloth.

Periodically you may wish to verify proper beam alignment. Refer to Chapter 35, Receivers," and in Volume II refer to Chapter 4, "System Installation and Alignment," and Chapter 5, "Measurement Optics (General Information)," for procedures.

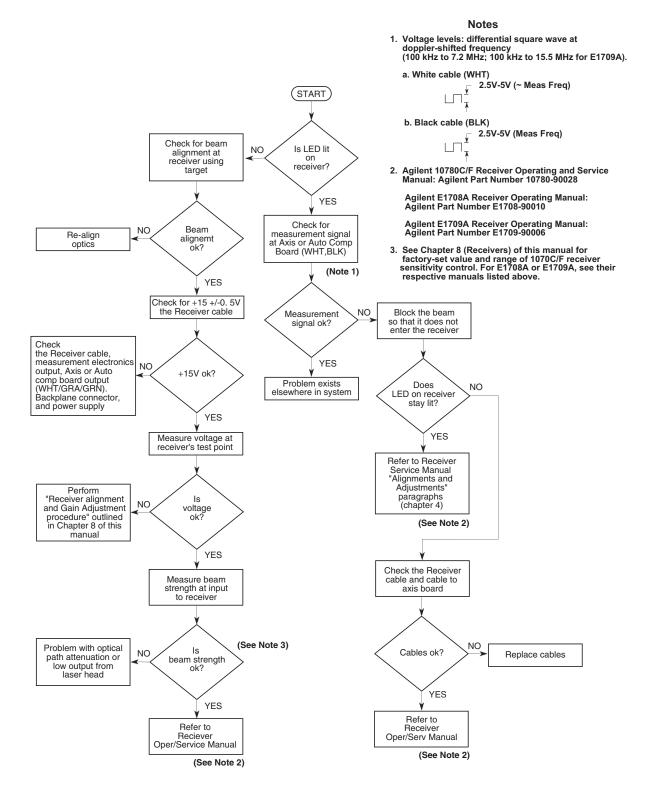


Figure 45 Agilent Receiver troubleshooting tree

#### Agilent 5519A/B Laser Head internal receiver

See the *Agilent 5519A/B Laser Head Service Manual* for internal receiver troubleshooting information.

### **Optical device troubleshooting**

Problems with the optical devices are usually caused by their misalignment. Refer to the alignment procedures in this manual for further information. Air turbulence caused by ventilation equipment or temperature gradients near the laser beam path can also cause measurement problems. If this is suspected, shield the area around the laser beam and optical devices with cardboard tubing, plastic sheet, or other suitable material. Some problems with sporadic counting and drift can be traced to air turbulence around the measurement path. This should be considered as a possibility before troubleshooting other parts of the system.

#### NOTE

If the problem is traced back to dirty optics, refer to "Procedures for Cleaning Measurement Optics", in Chapter 7, "Maintenance," of this manual, before you try to clean them.

Defective measurement optics should be returned to Agilent Technologies where they will be evaluated for repair. Follow the procedures outlined in Chapter 10, "Packaging for Storage or Shipment" of this manual for packaging methods and procedures.

Procedures for cleaning optics are given in Chapter 7, "Maintenance," of this manual.

### Agilent 10717A Wavelength Tracker troubleshooting

Troubleshooting the Agilent 10717A Wavelength Tracker involves proper interpretation of the Agilent laser system electronics front-panel annunciators, system- and board-level self tests, and knowing when the Wavelength Tracker requires realignment to the system optics. The main system problems that could occur include:

- Misalignment of the wavelength tracker, the receiver, the system optics, and system laser source
- Improper programming of system
- Malfunction of the receiver
- Malfunction of the Agilent system electronics (for example, the Agilent Automatic Compensation Board)

Troubleshooting trees (figures 45 and 46, respectively) will help you determine if the Agilent receiver or the Agilent 10717A Wavelength Tracker is faulty.

The front-panel LEDs, combined with the error messages listed in the appropriate electronics manuals, provide assistance with both programming and hardware problems. The SYSTEM ERROR LED illuminates when a problem occurs in the measurement or reference path of the Wavelength Tracker axis or when incorrect programming strings have been sent by the system controller. By sending an error message query to the Agilent electronics via the system controller, the system will respond indicating which board address is generating the error message, and provide a brief description of the error.

The Agilent 10717A Wavelength Tracker is an optical device and is prealigned at the factory. If found defective it should be returned to Agilent Technologies where it will be evaluated for repair. Follow the procedures outlined in Chapter 10, "Packaging for Storage or Shipment," of this manual for packaging methods and procedures.

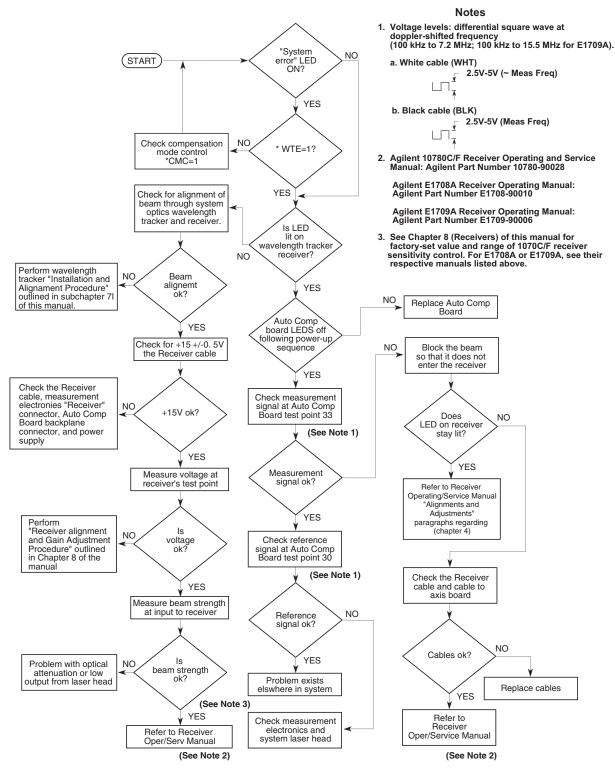


Figure 46 Agilent 10717A Wavelength Tracker troubleshooting tree

## **Before and After Service Product Safety Check**

The following safety checks must be performed after any troubleshooting and repair procedures have been completed to ensure the safe operation of the instrument.

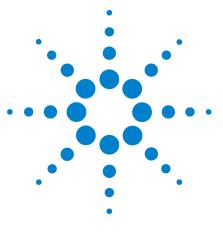
#### WARNING

Resistance checks described below require that the power cord be connected to the instrument and that AC power be disconnected. Be sure that the power cord is not connected to power before performing any safety checks.

- 1 VISUAL INSPECTION. Visually inspect the interior of the serviced instrument for signs of abnormal internally generated heat, such as discolored printed circuit boards or components, damaged insulation, or evidence of arcing. Determine and remedy the cause of any such condition.
- 2 GROUND CONTINUITY TEST. Plug the power cord into the Agilent electronics. DO NOT CONNECT THE INSTRUMENT TO AC POWER. Using a suitable ohmmeter, check the resistance from the enclosure (chassis) to the ground pin on the power cord. The reading should be less than 1 ohm. Flex the power cord while making this measurement to determine whether intermittent discontinuities exist. The resistance check should be performed from the enclosure to the ground pin of the cord while flexing the interconnect cable.
- 3 Check any indicated front or rear-panel ground terminals using the above procedures.
- 4 INSULATION RESISTANCE CHECK. Tie the line and neutral pins of the power cable together. Check resistance from the instrument enclosure (chassis) to line and neutral with the LINE switch ON and the power source disconnected. The minimum acceptable resistance is 2 Megohm. Replace any component that results in a failure.

POWER LINE MODULE CHECK. Check line fuse and line voltage selector in the electronics rear-panel power line module to verify that the correct fuse is installed and that the instrument is properly set for the AC source to be applied.

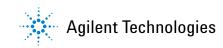
### 8 Troubleshooting



Agilent Laser and Optics User's Manual Volume I

# 9 Unpacking and Incoming Inspection

Introduction, 154 Unpacking and Incoming Inspection, 154 Warranty Claims, 154



# Introduction

This chapter provides information for unpacking and inspection, and warranty claims.

Information about laser tube shipment, tagging for service, and packaging for reshipment is presented in Chapter 10, "Packaging for Storage or Shipment," of this manual.

WARNING

To avoid hazardous electric shock, do not perform electrical tests when there are signs of shipping damage to any portion of the outer enclosure (covers, panels, meters).

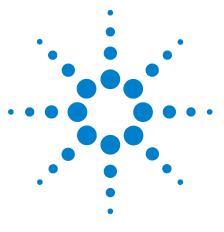
## **Unpacking and Incoming Inspection**

Inspect the shipping container for damage. If the shipping container or cushioning material is damaged, it should be kept until the contents of the shipment have been checked for completeness and the instrument has been checked mechanically and electrically.

If the contents are incomplete, if there is mechanical damage or defect, or if the instrument or some component fails, notify the nearest Agilent Technologies Office. If the shipping container is damaged, or if the cushioning material shows signs of stress, notify the carrier as well as the Agilent Technologies office. Keep the shipping materials for the carrier's inspection. The Agilent office will arrange for repair or replacement at Agilent's option without waiting for a claim settlement.

## **Warranty Claims**

Contact the nearest Agilent Sales and Service Office (see Certification and Warranty page at the front of this manual) for information relative to warranty claims.



Agilent Laser and Optics User's Manual Volume I

# 10 Packaging for Storage or Shipment

Laser Tube, 156 Tagging for Service, 156 Original Packaging, 156 Other Packaging, 156



## **Laser Tube**

The laser tube assembly should be shipped in an Agilent container designed for that purpose. In addition, the container must indicate that the laser tube contains magnetic material. To exchange the laser tube assembly, first order the replacement assembly and then upon receipt, return the old assembly in the same container. If it is necessary to ship a laser assembly, contact your nearest Agilent Sales and Service Office for an approved container.

## **Tagging for Service**

If a product is being returned to Agilent Technologies for service, please provide enough information to help us do what is needed and return the product to you. For best service results, be as explicit as possible when describing the assembly failure symptoms.

## **Original Packaging**

Containers and materials identical to those used in factory packaging are available through any Agilent Technologies office. If the instrument is being returned to Agilent for servicing, attach a blue tag indicating the type of service required, return address, model number, and full serial number. Also mark the container "FRAGILE" to ensure careful handling. The laser head container should indicate the instrument contains magnetic material. In any correspondence, refer to the instrument by model number and full serial number.

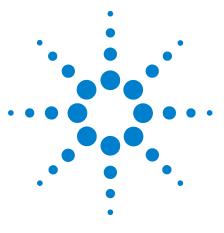
## **Other Packaging**

The following general instructions should be used for repacking system components with commercially available materials. These methods DO NOT apply to the laser tube assembly, or the Agilent 10735A or Agilent 10736A interferometers, which MUST be shipped in an Agilent approved container. If the laser assembly has not been removed from the laser head itself, the laser head may be packaged and shipped with the methods below.

1 Wrap the instrument in heavy paper or plastic. If the instrument is a circuit board, wrap it in anti-static material first, then add additional wrapping material. (If shipping to Agilent Technologies office or service center, attach a tag indicating the service required, return address, model number, and full serial number).

- 2 Use a strong shipping container. A double-wall carton made of 350-pound test material is adequate.
- 3 Use a layer of shock-absorbing material 70 to 100 mm (3 to 4 inches thick around all sides of the instrument to provide firm cushioning and prevent movement inside the container. Protect the front panel with cardboard.
- 4 Seal shipping container securely.
- 5 Mark shipping container "FRAGILE" to ensure careful handling. Indicate if magnetic material (such as a laser head) is enclosed.
- 6 In any correspondence, refer to instrument by model number and full serial number.

#### 10 Packaging for Storage or Shipment



Agilent Laser and Optics User's Manual Volume I

# 11 Principles of Operation

Introduction, 160 Measurement Technique, 161 Basic Measurement System, 163 Basic Agilent Laser Measurement System Components, 164



## Introduction

The measurements that an Agilent laser measurement system can make depend on the measurement optics (interferometers and retroreflectors) that are used.

The basic measurement made by all Agilent laser measurement systems is a linear measurement of the relative movement between an interferometer and its associated retroreflector, along the path of the laser beam. In most cases, the interferometer is the fixed optic and the retroreflector is the one that moves.

Agilent offers interferometers and retroreflectors that allow measurements of angles, flatness, and straightness to be made. However, all of these measurements represent special applications of the basic linear measurement. An angular measurement, for example, represents the difference in two linear measurements whose separation is precisely known.

The length standard for all of these measurements is the wavelength of laser light from the laser head. Relative motion between the interferometer and its retroreflector generates a series of interference fringes in the laser beam. The interference fringes are converted to electrical pulses in a receiver, and sent to the measurement electronics, which processes them as required to provide the desired measurement data.

The interferometric measurement system is sensitive enough that its measurements can be affected by changes in the measurement environment. These changes can affect both measurement accuracy and repeatability.

The wavelength of laser light, which is the length standard for measurements, can be affected by the characteristics of the environment between the interferometer and its associated measurement reflector. The process of determining the correct wavelength-of-light value for the measurement conditions is called compensation. Agilent offers devices (air sensor, wavelength tracker) which can be used to provide automatic compensation for the wavelength of light. Alternatively, wavelength-of-light compensation can be performed manually, by measuring the atmospheric temperature, pressure, and humidity, and calculating the compensation value or looking it up in a table. Additional information about wavelength-of-light compensation is provided in Chapter 13, "Wavelength-of-Light Compensation," of this manual.

Another environmental factor that can affect the measurement is the temperature of the material being measured. Agilent offers material temperature sensors that can enable automatic compensation for the effects of temperature changes. Material temperature compensation can also be performed manually, by measuring the material temperature and calculating the effect of the difference between the standard temperature and the temperature at the time of the measurement. Chapter 14, "Material Expansion Coefficients," in this manual provides expansion coefficient values for many commonly-used materials.

## **Measurement Technique**

#### Introduction

Agilent laser measurement systems measure displacement by:

- 1 generating a two-frequency laser beam.
- 2 sampling part of the beam, to determine the frequency difference between the two frequencies in the beam. This difference frequency is sent to the measurement system electronics as the Reference Frequency.
- 3 sending the two-frequency laser beam to an interferometer that separates the beam into two single-frequency beams. Each beam has one of the two frequencies of the original beam.
- 4 sending one interferometer output beam to a non-moving reference retroreflector, or a plane mirror, that returns it to the interferometer.
- 5 sending the second interferometer output beam to a measurement retroreflector, or a plane mirror, that returns it to the interferometer.
- 6 within the interferometer, combining the beams returned from the two retroreflectors to produce a difference frequency beam that is used as the interferometer's output.
- 7 sending the interferometer output to a receiver that converts the optical difference frequency from the interferometer to a series of electrical pulses at that frequency that is sent to the measurement system electronics for processing and any further use specified by the user and allowed by the electronics.

The main benefit of the two-frequency technique is that the distance information is carried on ac waveforms, or carriers, rather than in dc form. Since ac circuits are insensitive to changes in dc levels, a change in beam intensity cannot be interpreted as motion.

#### Creating the two-frequency laser beam

The ac signals representing distance change are analogous to the intermediate frequency carriers in FM heterodyne receivers. In the Agilent laser measurement system, the ac signal or "intermediate frequency" is produced by mixing two slightly different frequencies, near  $5 \times 1014$  Hz (500,000 GHz), differing by only a few megahertz.

Using different sources to generate the two frequencies would require ultra-stable sources and periodic calibration. However, a laser can be forced to output a laser beam composed of two frequencies simultaneously, by applying an axial magnetic field. The two resultant frequencies are very close together, but have opposite circular polarizations. Both frequencies are extremely stable and do not require recalibration. Waveplates within the laser head convert the circularly polarized beam components to orthogonally polarized components before the beam leaves the laser head. A polarizing beam splitter in the interferometer is used to separate the two beams.

#### Using the two-frequency laser beam at the interferometer

One of the laser frequency components  $(f_1)$  is used as the measuring beam and reflects from the external cube corner back to the beam splitter. Here the measuring beam mixes with the second or reference frequency  $(f_2)$  to produce fringe patterns. These patterns are composed of alternate light and dark bands caused by successive reinforcement and cancellation (interference) of the beams. If the movable cube corner reflector remains stationary, the interference rate (beat frequency) will be the exact difference between the laser's two frequencies, about 1.5 to 3 million fringes per second, depending on the laser head used.

When the cube corner moves, the frequency of the returning beam shifts up or down by  $(f_1 \pm \Delta f)$ , depending on the direction (and velocity) of the motion. A cube corner velocity of 300 millimeters per second (one-foot per-second) causes a frequency shift of approximately 1 MHz.

When a plane mirror interferometer is used, the measurement beam makes two passes to the measurement mirror. As a result, when the measurement mirror moves at 300 mm/second, the frequency shift seen in the measurement path is approximately 2 MHz.

The frequency shift is monitored by a photodetector and converted to an electrical signal ( $f_2 - (f_1 \pm \Delta f)$ ). A second photodetector inside the laser head monitors the fringe frequency before the paths are separated, and provides a reference signal that corresponds to zero motion ( $f_2 - f_1$ ).

### **Doppler frequency shifting**

Frequency shifting that results from (or indicates) relative motion between the source and receiver (observer) is known as Doppler shift. One example often used is the apparent change in pitch of a whistle or horn as the distance between the it and the listener changes. Another example is the red shift in the spectrums of stars, indicating that the universe is expanding.

The two frequencies from the photodetectors are sent to a special counter. The counter counts up on the Doppler-shifted signal from the retroreflector and down from the reference signal. With no retroreflector motion, the frequencies

are equal, and no net count is accumulated. When the retroreflector moves, the Doppler frequency increases or decreases to produce net positive or negative cumulative counts corresponding to the distance and direction traversed, in wavelengths of light.

## **Basic Measurement System**

A basic Agilent laser measurement system consists of: 1) a laser head, 2) an interferometer and its associated retroreflector, 3) a measurement receiver, and 4) measurement and control electronics. See Figure 47.

Because it is often not possible to line up the laser head output with the interferometer input aperture, the system will also include beam-directing optics.

Additionally, the system may also include environment sensing or wavelength tracking devices or both.

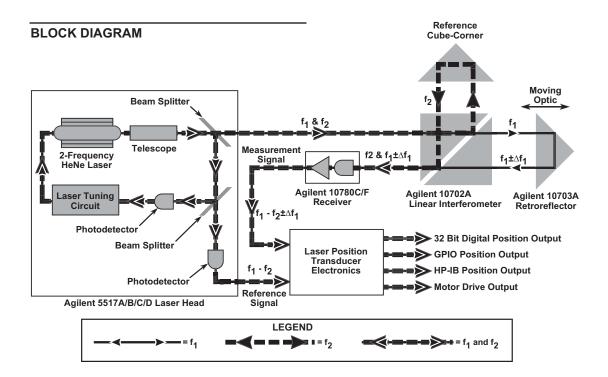


Figure 47 Typical (older) Agilent Laser Position Transducer block diagram

## **Basic Agilent Laser Measurement System Components**

The laser head serves as the light beam and reference frequency source.

The optics and the measurement receiver use the laser beam to generate the measurement signal. The reference and measurement signals, along with the environment sensor signals, are used by the measurement electronics to generate linear displacement information.

The system controller can read and display this information. In addition, the controller can send destination input data to the measurement electronics, which outputs a real-time error signal representing the difference between the destination and the actual position. This error signal can be used in servo electronics to drive a stage's positioning motors.

#### Laser head

A low-power helium-neon laser emits a coherent light beam composed of two slightly different optical frequencies,  $f_1$  and  $f_2$ , of orthogonal linear polarizations. (See Figure 47.) Before exiting the laser assembly, the beam passes through a beam splitter where a small fraction of the beam is sampled. This portion of the beam is used both to generate a reference frequency and to provide an error signal to the laser cavity tuning system. The difference in the amplitudes of  $f_1$  and  $f_2$  is used for tuning while the difference in frequency between  $f_1$  and  $f_2$  (between 1.5 MHz and 3.0 MHz, depending on the model of the laser head) is used for the reference signal.

The wavelength of light from the laser head is used as the length standard for Agilent laser measurement systems. The laser head generates a coherent (all light waves in phase), collimated (all waves traveling parallel to one another) light beam consisting of two orthogonally polarized frequency components. The laser measurement system uses this beam to generate measurement signals (MEASurement Frequency). In addition to this beam, the laser head generates an electrical reference signal (REFerence FREQuency).

#### **System optics**

The major portion of the beam passes out of the laser head to an interferometer. The interferometer is a polarizing beam splitter that reflects one polarization (frequency) and transmits the other. The beam splitter is oriented such that the reflected and transmitted beams are at right angles to each other. The reflected beam  $(f_2)$  is reflected off a fixed retroreflector or mirror, usually mounted directly on the interferometer. The transmitted frequency  $(f_1)$  passes through the interferometer and is reflected back to the interferometer by a movable retroreflector or plane mirror. If the distance between the interferometer and the movable retroreflector remains fixed, the difference frequency  $(f_2-f_1)$  equals the reference signal. Under these

conditions, the Agilent laser measurement system electronics detects no change in relative position of the interferometer and the movable retroreflector. When the movable retroreflector changes position relative to the fixed interferometer, a doppler frequency shift occurs. This Doppler-shifted frequency becomes  $f_1 \pm \Delta f_1$  depending on the direction of reflector movement. The two frequency components,  $f_1$  and  $f_2$ , exit the interferometer as a coincident beam.

One of the two frequency components is directed toward the object whose motion is being measured. There it is reflected by a mirror or retroreflector (cube-corner) and returned to the interferometer.

The other frequency component travels a fixed path through the cube corner mounted directly to the interferometer, where both components recombine into a single beam. Both cube-corner retroreflectors offset their corresponding beams and return them parallel to the incoming beam path. Small rotations or perpendicular movements will not affect the accuracy of the measurement.

Each laser measurement system axis must have an interferometer and retroreflector. Machine design considerations determine which type of interferometer is optimum. The choice of the interferometer for each axis usually specifies the retroreflector or plane mirror for that axis.

The Agilent 10717A Wavelength Tracker is an interferometer and etalon (fixed-length reference cavity) combination that measures changes in laser wavelength, not displacement. It measures apparent change in a fixed distance, which is interpreted as a variation in the laser wavelength.

For more detailed information on the individual optical components available from Agilent, refer to chapters 18 through 34 (the interferometers chapters), Chapter 17, "Beam-Directing Optics," and Chapter 36, "Accessories," in Volume II of this manual.

### Receiver

The coincident beam is directed to a receiver (e.g., Agilent 10780C or Agilent 10780F) where the two frequency components interfere (mix) at the receiver's polarizing plate. This produces a difference frequency which is detected by the receiver's photodetector and converted to an electrical signal. The receiver Circuitry then amplifies the signal which becomes the measurement frequency. Displacement information is obtained in the measurement electronics by a comparison of both the measurement and reference signals.

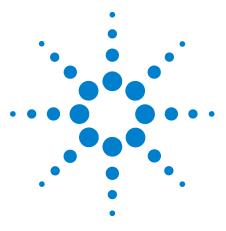
#### **Environment sensors**

As described at the beginning of this manual chapter, the laser measuring system is sensitive enough that its measurements can be affected by environmental conditions during the measurement.

The Agilent 10751C or Agilent 10751D Air Sensor can be used with measurement electronics to automatically and continuously provide compensation for changes in the wavelength of laser light resulting from changes in the atmospheric conditions at the time of the measurement.

The Agilent 10757D, Agilent 10757E, or Agilent 10757F Material Temperature Sensor can be used with measurement electronics to automatically and continuously enable changes in measurement information based on changes in the temperature of the item being measured.

The Agilent 10717A Wavelength Tracker, described in Chapter 24 in Volume II of this manual, is also an environment sensor.

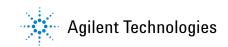


Agilent Laser and Optics User's Manual Volume I

# 12 Accuracy and Repeatability

Introduction, 168

The Components of System Accuracy and Repeatability, 168 Determining System Accuracy and Repeatability, 189 Examples — Determining System Accuracy and Repeatability, 190 Achieving Optimum System Accuracy and Repeatability, 208 Non-Uniform Environments, 214 References, 222



# Introduction

This chapter introduces the basic concepts, techniques, and principles that determine the overall measurement performance of Agilent laser measurement systems. Two examples of modeling a laser system's accuracy and repeatability are provided.

Understanding the error components in the laser interferometer system will help you use the modeling technique described in this chapter. The measurement accuracy and repeatability is determined by summing the error components in the system's error budgets. Before proceeding with the discussion of each component in the accuracy and repeatability error budgets, review the definitions of accuracy and repeatability given below.

- Accuracy: The maximum deviation of a measurement from a known standard or true value.
- **Repeatability:** The maximum deviation between measurements under the same conditions and with the same measuring instrument. This also refers to how stable the measurement will be over time.

# The Components of System Accuracy and Repeatability

The system measurement accuracy and repeatability error budgets share many of the same error components.

System measurement repeatability is divided into short-term and long-term repeatability. Short-term repeatability is the measurement stability over a period shorter than one hour; long-term repeatability is stability over a period longer than one hour. Error components that make up the accuracy and repeatability error budgets are shown in Table 10.

	System Error Budgets		
Error Components by Category	Accuracy	Long-Term Repeatability	Short-term Repeatability
Intrinsic			
Laser Wavelength	Х	Х	х
Electronics Error	х	Х	х
Optics Nonlinearity	х	Х	х
Environmental			
Atmospheric Compensation	х	Х	х
Material Thermal Expansion	х	Х	
Optics Thermal Drift	х	Х	
Installation			
Deadpath Error	х	Х	х
Abbé Error	х	х	
Cosine Error	Х		

Table 10 Error components for accuracy and long- and short-term repeatability error budgets

Both the accuracy and the repeatability error budgets have several components. Some of these components are affected by the operating environment, while others are affected by the system installation. The error components can be categorized as either proportional or fixed terms.

Proportional error terms are generally specified in parts-per-million (ppm). The resulting measurement error is a function of the distance measured by the interferometer system.

Fixed error terms are noncumulative. Fixed terms are given in units of length, such as nanometers or microns. The resulting measurement errors are not a function of the measured distance.

Environmental and installation error components are often the largest contributors to the error budgets. Be sure to keep them in mind when designing and installing the laser interferometer system. A more detailed discussion of these error components follows.

### Laser wavelength

An interferometer system generates optical fringes when relative movement occurs between the measurement optics of the system. Each fringe generated represents displacement by a fraction of the laser's wavelength. However, fringes are also generated if the laser wavelength changes, causing an apparent distance change measurement even when there is no actual displacement of an optic. This apparent movement is measurement error.

The laser source of any interferometer system has some type of frequency stabilization to maintain its wavelength accuracy and repeatability.

A laser interferometer system's accuracy is fundamentally based on the laser's wavelength accuracy.

The system's repeatability is based on the laser's wavelength stability.

Laser wavelength accuracy and stability are specified in parts-per-million (ppm) of the laser frequency. They are proportional errors; that is, the measurement error is a function of the distance measured. All laser sources for Agilent laser transducer systems have the same wavelength accuracy and stability specifications. These values are specified in a vacuum.

Lifetime wavelength accuracy for the laser heads is  $\pm 0.1$  ppm standard and  $\pm 0.02$  ppm with optional calibration.

Wavelength stability of the laser heads is typically  $\pm 0.02$  ppm over their lifetime and  $\pm 0.002$  ppm over one hour.

## **Electronics error**

Electronics error stems from the method used to extend basic optical measurement resolution in an interferometer system.

The basic resolution of an interferometer system is  $\lambda/2$  (when using cube-corner optics). The resolution can be electronically or optically extended beyond  $\lambda/2$ .

In an Agilent laser measurement system, the electronics error equals the uncertainty of the least resolution count. That is, electronic error equals the measurement resolution. It is the quantization error of the electronic counter in the system. Other methods of electronic resolution extension can cause jitter and nonlinearity in measurement data, thus adding other errors.

The electronics error term is a fixed error equal to the least resolution count on Agilent systems. When using an Agilent laser measurement system, there are three possible linear measurement resolutions, depending on the interferometer chosen.

Table 11 lists the measurement resolutions for each interferometer available with this system when used with:

- the Agilent 10885A PC Axis Board,
- the Agilent 10895A VME Laser Axis Board,
- the Agilent 10897B High Resolution VMEbus Laser Axis Board, or
- the Agilent 10898A High Resolution VMEbus Dual Laser Axis Board

Interferometer		Fundamental Optical Resolution	System Resolution (Note 1)	System Resolution (Note 2)
Agilent 10702A		λ/2 (316.5 nm, 12.5 μin)	λ/64 (10.0 nm, 0.4 µin)	λ/512 (1.2 nm, 0.047 μin)
Agilent 10705A		λ/2 (316.5 nm, 12.5 μin)	λ/64 (10.0 nm, 0.4 μin)	λ/512 (1.2 nm, 0.047 μin)
Agilent 10706A		λ/4 (158.2 nm, 6.2 μin)	λ/128 (5.0 nm, 0.2 μin)	λ/1024 (0.62 nm, 0.024 µin)
Agilent 10706B		λ/4 (158.2 nm, 6.2 μin)	λ/128 (5.0 nm, 0.2 μin)	λ/1024 (0.62 nm, 0.024 µin)
Agilent 10715A		λ/4 (158.2 nm, 6.2 μin)	λ/128 (5.0 nm, 0.2 μin)	λ/1024 (0.62 nm, 0.024 µin)
Agilent 10716A		λ/8 (79.1 nm, 3.1 μin)	λ/256 (2.5 nm, 0.1 μin)	λ/2048 (0.31 nm, 0.012 µin)
Agilent 10719A	Linear	λ/4 (158.2 nm, 6.2 μin)	λ/128 (5.0 nm, 0.2 μin)	λ/1024 (0.62 nm, 0.024 µin)
	Angular	(1.71 arcsec, 8.3 µrad)	(0.05 arcsec, 0.26 µrad)	(0.007 arcsec, 0.03 µrad)
Agilent 10721A	Linear	λ/4 (158.2 nm, 6.2 μin)	λ/128 (5.0 nm, 0.2 μin)	λ/1024 (0.62 nm, 0.024 µin)
	Angular	(2.56 arcsec, 12.4 µrad)	(0.08 arcsec, 0.39 µrad)	(0.01 arcsec, 0.05 µrad)
Agilent 10735A		Three axes, each the same as the Agilent 10706B. See listing above.		isting above.
	Linear		$\lambda/128$ on three axes	$\lambda/1024$ on three axes
	Yaw		0.04 arcsec, 0.2 µrad	0.005 arcsec, 0.025 µrad
	Pitch		0.05 arcsec, 0.24 µrad	0.006 arcsec, 0.03 µrad
Agilent 10736A		Three axes, each the same as the Agilent 10735A. See listing above.		
Agilent 10736A-001		Three axes, each the same as the Agilent 10735A. See listing above.		
Agilent 10766A		λ/2 (316.5 nm, 12.5 μin)	λ/64 (10.0 nm, 0.4 μin)	λ/512 (11.2 nm, 0.047 μin)
Agilent 10770A	Angular	(20.0 arcsec, 97.0 µrad)	(0.63 arcsec, 3.0 µrad)	(0.08 arcsec, 0.38 µrad)

 Table 11
 System measurement resolution for each interferometer

Notes:

1. The system resolution is based on using 32X electronic resolution extension. This is available with the Agilent 10885A and Agilent 10895A.

2. The system resolution is based on using 256X electronic resolution extension. This is available with the Agilent 10897B and Agilent 10898A electronics.

3. The Agilent 10719A interferometer makes a single measurement, which may be either linear or angular (optically subtracted), depending on the installation. The linear and angular measurements are mutually exclusive and therefore not simultaneous.

4. The Agilent 10721A interferometer makes a two adjacent linear measurements which can be subtracted electronically to give an angular measurement with a linear measurement simultaneously.

5. The Agilent 10735A, Agilent 10736A, and Agilent 10736A-001 interferometers, make linear and angular measurements, so they have both linear and angular resolution specifications.

## **Optics nonlinearity**

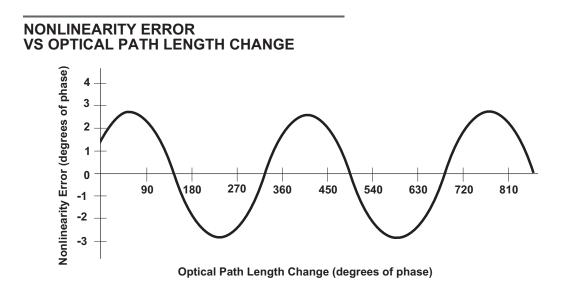
Optics nonlinearity occurs as a result of the optical leakage of one polarization component into the other.

The interferometer optical element in a laser interferometer system can contribute to measurement uncertainty because of its inability to perfectly separate the two laser beam components (vertical and horizontal polarizations).

Optics nonlinearity error is periodic, with a period of one wavelength of optical path change or a 360° phase shift between the reference and measurement frequencies. Nonlinearity caused by optical leakage affects all interferometer systems, whether they are single-frequency or two-frequency.

Leakage of one laser beam component into the other occurs for two reasons. First, the light leaving any laser source is not perfectly polarized linearly; instead, it is slightly elliptical. Second, the interferometer optical element is unable to perfectly separate the two laser beam components.

Figure 48 shows a computed error plot of nonlinearity versus optical path length change for worst-case conditions (when using a linear interferometer). The peak-to-peak phase error is 5.4°<sup>\*</sup>, corresponding to a worst case peak-to-peak error of 4.8 nanometers of distance. Using a statistical model, the RSS (Root Sum of Squares) value is ±4.2 nanometers worst case peak-to-peak, including the contribution from the laser head. This nonlinearity error is a fixed term and is different for each interferometer.





### **Atmospheric compensation**

The atmospheric compensation error term is usually the single largest component in an error budget. The magnitude of this error depends on the accuracy of the compensation method, the atmospheric conditions in which the laser system is operating, and how much the atmospheric conditions change during a measurement.

The laser wavelength is specified as the vacuum wavelength,  $\lambda_{V}$ .

In vacuum, the wavelength is constant (to the degree specified by the stability specification), but in an air atmosphere the wavelength depends on the index-of-refraction of the atmosphere.

Since most laser interferometer systems operate in air, it is necessary to correct for the difference between  $\lambda_V$  and the wavelength in air,  $\lambda_A$ . This correction is referred to as atmospheric or wavelength-of-light (WOL) compensation. The index-of-refraction, n, of air is related to  $\lambda_V$  and  $\lambda_A$  by:

$$n = \frac{\lambda_V}{\lambda_A} \tag{1}$$

Any change in air density, which is a function of air temperature, air pressure, humidity, and composition, affects the index-of-refraction. Thus, a change in air density alters the required compensation of the laser measurement. Without proper compensation, system accuracy and repeatability will be degraded. For example, assuming a standard and homogeneous air composition, a one ppm error will result from any one of the following conditions:

- a 1°C (1.8 °F) change in air temperature,
- a 2.5 mm (0.1 inch) of mercury change in air pressure,
- an 80% change in relative humidity.

The wavelength compensation number (WCN) is the inverse of the index-of-refraction, that is:

$$WCN = \frac{\lambda_A}{\lambda_V} \tag{2}$$

Since the laser interferometer system counts the number of wavelengths of distance traveled, actual displacement can be determined as follows:

Actual displacement = (wavelength counts) × WCN ×  $\lambda_V$  (3)

This equation shows that uncertainty in the wavelength compensation number directly affects the interferometer measurement. This error is a proportional term, and is specified in parts-per-million.

The wavelength compensation number can be derived by a direct measurement of index-of-refraction using a refractometer or by using empirical data.

Without a refractometer it is best simply to measure the air pressure, temperature, and relative humidity, and then relate this data to the refractive index using the formulas by Barrel & Sears<sup>\*</sup> or Edlen<sup>†</sup>. The accuracy and repeatability of the compensation number derived by the empirical method depends on the accuracy of the formula used and the ability to measure the atmospheric conditions.

<sup>\*</sup>Barrell, H. & Sears, J.E., (1939)Phil Trans. Roy. Society, A258, 1-64.

<sup>†</sup>Edlen, B., The Refractive Index of Air, Metrologia, 1966, 2, 71-80.

Birch K P, Downs MJ, Metrologia, 1993, 30, 155-162.

Birch K P, Downs MJ, Metrologia, 1994, 31, 315-316.

Estler, W Tyler, Applied Optics 24 #6, 1985, 808-815.

The empirical method suffers from the following disadvantages compared to using a refractometer:

- it is an indirect measurement, which is subject to sensor error,
- it is an approximation (good to only 0.05 ppm),
- it is slow in response, due to sensor time constants and calculation time,
- it requires periodic calibration of the sensors,
- it ignores air composition changes, such as:
  - Carbon dioxide and
  - Chemical vapors.

Agilent laser position transducer systems generally provide two methods of atmospheric compensation.

In the first method, an air sensor is available that: 1) measures air temperature and pressure, 2) allows a selectable humidity setting, and 3) calculates a compensation number for the system. This product, the Agilent 10751C/D Air Sensor, provides a compensation accuracy of  $\pm 1.4$  ppm and a repeatability better than  $\pm 1.4$  ppm, depending on the temperature range.

The second method of compensation uses a differential refractometer, the Agilent 10717A Wavelength Tracker. The wavelength tracker uses an optical technique to provide compensation repeatability as small as  $\pm 0.14$  ppm. Since it is a differential refractometer, only changes in the air's index-of-refraction are measured. This means the initial compensation number must be determined from another source, which also determines the compensation accuracy. One popular method for accurately determining the initial compensation number is to measure a known standard or artifact with the laser system on the machine. Alternatively, high-accuracy external sensors or the Agilent 10751C/D Air Sensor can be used to obtain the initial compensation value.

The repeatability of the Agilent 10717A Wavelength Tracker's compensation number is given by the equation:

$$Repeatability = \pm \left[ 0.067 ppm + \frac{0.06 ppm}{degrees C} \times \Delta T + \frac{0.002 ppm}{mmHg} \times \Delta P \right] (4)$$

This equation shows that the compensation number's repeatability is a function of ambient temperature and pressure. This temperature and pressure dependency is based on the materials used to construct the Agilent 10717A Wavelength Tracker.

Additional information about wavelength-of-light compensation is provided in Chapter 13, "Wavelength-of-Light Compensation," of this manual.

### Material thermal expansion

Since a part or machine's dimensions are a function of temperature, a correction for material expansion or contraction may be required. This correction relates the distance measurement back to a standard temperature of 20 °C (68 °F). To achieve this correction, the temperature of the part or machine (during the time of the measurement), and its coefficient of linear thermal expansion must be known.

The method of correction is to electronically change the effective laser wavelength (e.g., through the controller software) by an amount sufficient to correct for thermal expansion or contraction. This correction or compensation term is known as Material Temperature Compensation and is defined as:

Material Temperature Compensation =  $1 - \alpha (\Delta T)$  (5)

where:

 $\alpha$  = coefficient of linear thermal expansion

 $\Delta T = T - 20^{\circ}C$ 

Therefore, the compensated distance measurement (at standard temperature) is:

 $L_1 = L_2$  [Material Temperature Compensation] (6)

where:

 $L_1$  = length at 20°C

 $L_2$  = length at temperature T

Assuming a known coefficient of thermal expansion, the magnitude of this error is a function of the object's temperature and the temperature sensor's measurement accuracy and repeatability. This error term is also a proportional term specified in parts-per-million.

The material temperature sensor for Agilent laser systems is the Agilent 10757D/E/F Material Temperature Sensor. It has an accuracy of  $\pm 0.1^{\circ}$ C and a measurement repeatability better than  $\pm 0.1^{\circ}$ C.

Linear coefficients of expansion for various commonly used materials are presented in Chapter 14, "Material Expansion Coefficients," of this manual.

### **Optics thermal drift**

In a laser interferometer system, changes in temperature of some optical components during the measurement can cause measurement uncertainty. This effect occurs in the measurement optic (the interferometer) in the form of a change in optical path length with temperature. This change in optical path length appears as an apparent distance change. This optical path length change is caused by the two laser beam components (horizontal and vertical polarizations) passing through different amounts of glass, as shown in Figure 49.

With a conventional plane mirror interferometer, such as the Agilent 10706A, beam component  $f_A$  travels through more glass than does  $f_B$ . Beam component  $f_A$  makes twice as many trips through the polarizing beam splitter as does  $f_B$ . Component  $f_A$  also makes two round trips through the quarter-wave plate, whereas  $f_B$  does not pass through the quarter-wave plate at all.

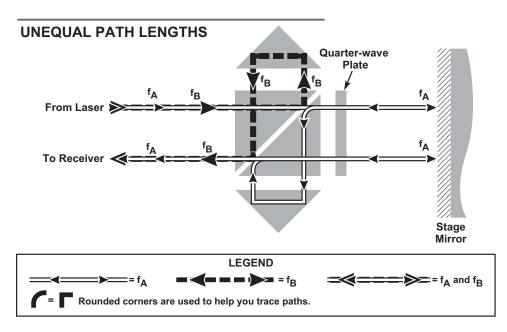


Figure 49 Conventional plane mirror interferometer with unequal path lengths that result in optics thermal drift

When a change in temperature occurs, the physical size of the optical elements changes, as does their index-of-refraction. Both changes contribute to an apparent change in distance. This type of interferometer has a typical thermal drift value of 0.5 micron per degree C. This measurement error is a fixed value and is only a function of the change in interferometer temperature, not the distance measured.

Optics thermal drift can be reduced by either controlling the temperature of the measurement environment or by using interferometers that are insensitive to temperature changes. To reduce the temperature sensitivity of an interferometer, the beam components need to travel through the same type and amount of glass. Several interferometers available for Agilent laser measurement systems significantly reduce the optics thermal drift error.

- The Agilent 10715A Differential Interferometer has a thermal drift on the order of fractions of a nanometer per  ${}^{\circ}C^{*}$ .
- The Agilent 10706B High Stability Plane Mirror Interferometer has a thermal drift, optics that of a conventional plane mirror interferometer, typically 0.04 micron/°C. Other interferometers incorporating a similar high-stability design include the Agilent 10716A, Agilent 10719A, Agilent 10721A, Agilent 10735A, and Agilent 10736A.

Figure 50 is an optical schematic of the Agilent 10706B High Stability Plane Mirror Interferometer. In the Agilent 10706B, the reference beam cube comer has been replaced by a quarter-wave plate with a high-reflectance coating on the back. This optical design allows the measurement and reference beams to have the same optical path lengths in the glass, essentially eliminating measurement errors caused by temperature changes of the optics.

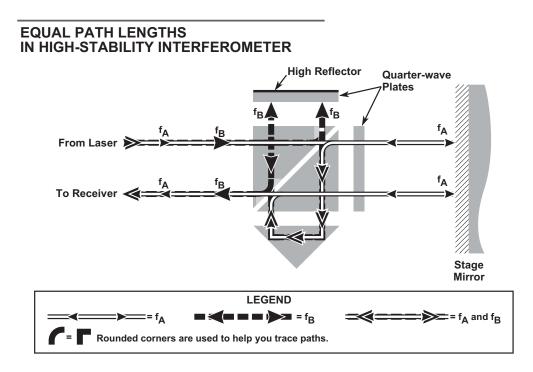


Figure 50 Agilent 10706B High Stability Plane Mirror Interferometer Beam Paths

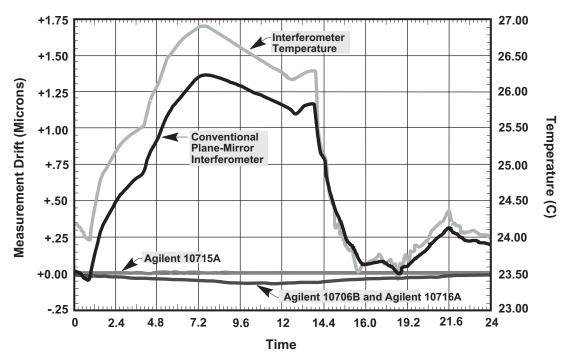
The optical path lengths for the two beams may differ slightly, due to the normal dimensional tolerances in the thicknesses of the quarter-wave plates and in the geometry of the beam splitter. These small variations result in the

\*Baldwin, D.R. & Siddall, G.J., A double pass attachment for the linear and plane mirror interferometer, Proc. SPIE, Vol. 480, p.78-83, 1984.

small thermal drift of the Agilent 10706B. Since either optical path length may be longer than the other, depending on the actual optical elements used, the thermal drift may be positive or negative.

Figure 51 is a plot of the thermal drift performance of the Agilent 10706B, Agilent 10716A, and Agilent 10715A interferometers as compared to a conventional plane mirror interferometer.

- The left vertical scale is thermal drift in microns.
- The right vertical scale is the interferometer's temperature in °C.
- The horizontal scale is time.
- The thermal drift of the conventional plane mirror interferometer (Agilent 10706A) closely tracks the optics temperature changes at a rate of approximately 0.5 micron per °C.
- The Agilent 10715A shows essentially zero drift.
- The Agilent 10706B and Agilent 10716A show much smaller drift than the conventional plane mirror interferometer, typically 0.04 micron per degree C.



#### MEASUREMENT DRIFT AND TEMPERATURE VS. TIME

Figure 51 Comparison of optics thermal drift between Interferometers

#### 12 Accuracy and Repeatability

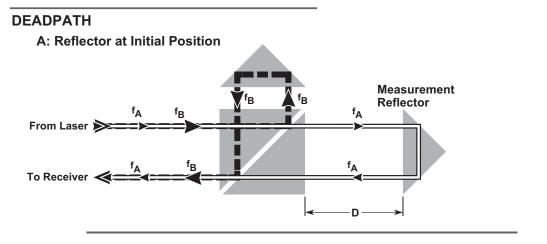
### **Deadpath error**

Deadpath error is caused by an uncompensated length of the laser beam between the interferometer and the measurement reflector, with the positioning stage or machine at its "zero" position (the position at which the laser system is reset).

The deadpath distance is the difference in the optical path lengths of the reference and measurement components of the laser beam at the zero position. If not properly compensated during changing environmental conditions, these unequal beam components can produce a measurement error.

Figure 52(A) shows the unequal path lengths for a conventional linear interferometer. The deadpath length is designated as "D". In this diagram, the reference component is  $f_B$ , and the measurement component is  $f_A$ . The  $f_A$  optical path is longer than the  $f_B$  path, by "D". Assume that the measurement reflector, a cube-corner in this example, moves the distance "L" (see Figure 52(B) to a new position and comes to rest.

Assume that, while the cube corner is at rest, the environmental conditions surrounding the laser beam change. The laser beam wavelength changes over the entire path (D + L) due to these environmental changes, and so should be compensated. Since a laser interferometer system measures only "wavelengths of motion", which involves only the distance "L", the system will not correct for the wavelength change over "D". This will result in an apparent shift in the zero position on the machine. This zero shift is deadpath error, and occurs whenever environmental conditions change during a measurement.



**B: After Reflector Movement** 

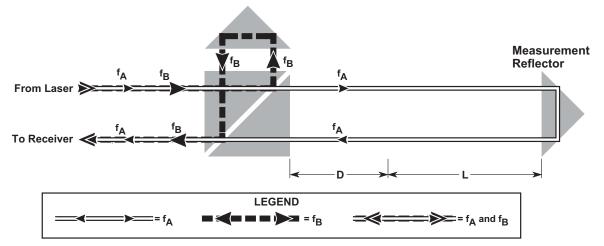


Figure 52 Deadpath caused by unequal lengths from initial point

Deadpath error can be represented as:

Deadpath Error = Deadpath distance  $\times \Delta WCN$  (7)

where:

 $\Delta$ WCN = Change in wavelength compensation number during the measurement time.

Deadpath effects should be considered when designing a laser interferometer into an application or when using it.

Table 12 lists the minimum-deadpath mirror position(s), and the deadpath values, for Agilent interferometers.

Interferometer	Mirror Position for Minimal Deadpath	Deadpath Value
Agilent 10702A	Zero-deadpath condition exists when the measurement cube corner is flush with the interferometer's measurement face.	Distance between interferometer measurement face and cube corner face at measurement "zero" position.
Agilent 10705A	Zero-deadpath condition exists when the measurement cube corner is flush with the interferometer's; measurement face.	Distance between interferometer measurement face and cube corner face at measurement "zero" position.
Agilent 10706A	Zero-deadpath condition cannot be achieved with this interferometer. Because of interferometer design, zero-deadpath would require that measurement reflector be inside the interferometer 7.62 mm (0.300 inch) behind the measurement face.	Distance between interferometer measurement face and cube corner face at measurement "zero" position plus 7.62 mm (0.300 inch).
Agilent 10706B	Zero-deadpath condition exists when the measurement mirror is flush with the interferometer's; measurement face.	Distance between interferometer measurement face and cube corner face at measurement "zero" position.
Agilent 10715A	Zero-deadpath condition cannot be achieved with this interferometer design because the reference and measurement mirrors cannot be coplanar.	Distance between front face of reference mirror and front face of measurement mirror.
Agilent 10716A	Zero-deadpath condition exists when the measurement mirror is flush with the interferometer's; measurement face.	Distance between interferometer measurement face and measurement mirror, at measurement "zero" position.
Agilent 10719A	Zero-deadpath condition exists when the measurement mirror is 19.05 mm (0.750 inch) farther from the interferometer's measurement face than the reference mirror is.	<ul> <li>M - R - 19.05 (metric),- or -</li> <li>M - R - 0.750 (English),</li> <li>- where:</li> <li>M = Measurement Mirror distance from interferometer*</li> <li>R = Reference Mirror distance from interferometer*</li> <li>*at measurement "zero" position</li> </ul>
Agilent 10721A	Zero-deadpath condition exists when the measurement mirror is 19.05 mm (0.750 inch) farther from the interferometer's measurement face than the reference mirror is.	<ul> <li>M - R - 19.05 (metric),- or -</li> <li>M - R - 0.750 (English),</li> <li>- where:</li> <li>M = Measurement Mirror distance from interferometer*</li> <li>R = Reference Mirror distance from interferometer*</li> <li>*at measurement "zero" position</li> </ul>

Table 12Deadpath	mirror positions and	values for Agilent	t interferometers
Table TEBeaupath		valabe for / ignori	

Interferometer	Mirror Position for Minimal Deadpath	Deadpath Value
Agilent 10735A	Zero-deadpath condition cannot be achieved with this interferometer. Because of interferometer design, zero-deadpath would require that measurement reflector be inside the interferometer, 6.59 mm (0.259 inch) behind the measurement face.	Distance between interferometer measurement face and cube corner face at measurement "zero" position plus 6.59 mm (0.259 inch).
Agilent 10736A	Zero-deadpath condition cannot be achieved with this interferometer. Because of interferometer design, zero-deadpath would require that measurement reflector be inside the interferometer, 6.59 mm (0.259 inch) behind the measurement face.	Distance between interferometer measurement face and cube corner face at measurement "zero" position plus 6.59 mm (0.259 inch).
Agilent 10736A-001	Zero-deadpath condition cannot be achieved with this interferometer. Because of interferometer design, zero-deadpath would require that measurement reflector be inside the interferometer. For measurement axis #1 or measurement axis #3, zero-deadpath would require that the measurement reflector be inside the interferometer 6.59 mm (0.259 inch) behind the measurement face. For the bent measurement axis (measurement axis #2), zero-deadpath would require that the measurement reflector be inside the interferometer, 34.42 mm (1.355 inches) behind the measurement face.	For measurement axis #1 or measurement axis #3, distance between interferometer measurement face and measurement mirror, at measurement "zero" position, plus 6.59 mm (0.259 inch) behind the measurement face. For the bent measurement axis (measurement axis #2, distance between interferometer's beam bender measurement face and measurement mirror, at measurement "zero" position, plus 34.42 mm (1.355 inches).
Agilent 10776A	Zero-deadpath condition exists when the measurement cube corner is flush with the interferometer's measurement face.	Distance between interferometer measurement face and cube corner face at measurement "zero" position.
Agilent 10770A	Zero-deadpath condition exists when the angular reflector face is parallel to the interferometer's measurement face.	Difference in beam path lengths between interferometer and angular reflector, at measurement "zero" position.
Agilent 10774A	When used with the straightness reflector, the reference and measurement beam paths are the same length in air.	Deadpath does not exist.
Agilent 10775A	When used with the straightness reflector, the reference and measurement beam paths are the same length in air.	Deadpath does not exist.

Table 12Deadpath mirror	positions and values for Agilent interferometers	(continued)	
		(	

During system design, there are two key approaches to minimizing deadpath effects.

• One approach is to locate the stationary optic (typically the interferometer) as close as possible to the "zero" point of the moving optic. The zero point is established at the time the laser system is reset.

This will minimize or eliminate deadpath in most applications. This is shown in Figure 53, which shows how to eliminate deadpath in a basic optical layout for an interferometer system.

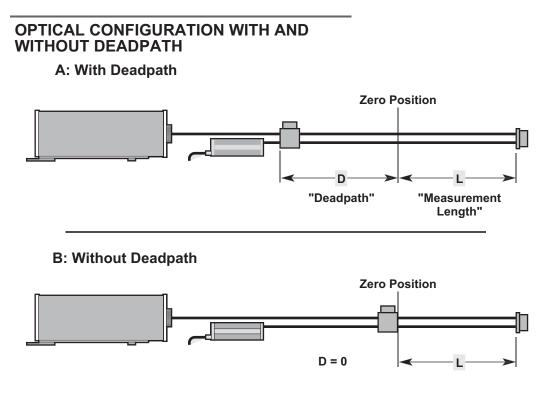


Figure 53 Optical configuration with and without deadpath

NOTE

It is important to understand that the zero-deadpath condition occurs when the reference and measurement optical paths have equal length. For some interferometers, this may NOT correspond simply to bringing the interferometer and measurement mirror as close as possible. For example, due to the differential design of the Agilent 10719A and Agilent 10721A interferometers, the zero-deadpath condition occurs when the mirror is 19 mm (0.750 inch) FARTHER from the interferometer than the reference mirror is located. This condition makes the reference and measurement path lengths equal because the reference beam travels an additional 19 mm (0.750 inch) inside the interferometer. • The second approach is to choose an interferometer model which permits the minimum deadpath in the installation, wherever possible. While Agilent interferometers can usually be installed with essentially zero deadpath, the application itself sometimes imposes constraints. For example, in some cases, the Agilent 10715A may be the interferometer of choice because it has a remote reference mirror which minimizes deadpath when the interferometer itself cannot be located at the zero point.

During use of the interferometer system, there are two alternative methods to minimize deadpath effects.

- The first method is to always move the moving optic (typically the measurement reflector) to the position where the deadpath distance is zero (that is, where measurement path length equals reference path length), before resetting the laser system. This aligns the machine's "zero" point to the zero-deadpath position. If you always do this, no further compensation will be required.
- The second method which you should use when it is not possible to align the machine's "zero" point to the zero-deadpath position at reset — is to provide deadpath compensation via software in the system controller.

Note that when using the Agilent 10719A in its angle-measuring configuration, the software correction is the only method possible since the measurement and reference path lengths are inherently unequal by 19.05 mm (0.750 inch).

By expanding Equation 3, the corrected actual displacement can be represented as:

Actual displacement = [(Accumulated Counts + Deadpath Counts):

$$\times \frac{\lambda v}{R} \times WCN_1 \Big] - Deadpath \, distance \tag{8}$$

"Accumulated counts" is the displacement measured in units of LRCs (Least Resolution Counts). "Deadpath counts" is the deadpath distance in terms of compensated LRCs (using the initial compensation number, WCN0) " $\lambda_V/R$ " is equal to the LRC in units of length, where "R" is the amount of resolution extension. The compensation number at the time of measurement is WCN<sub>1</sub>.

In most cases, when you enter a deadpath distance into the software, a positive value corresponds to the case in which the measurement path length is longer than the reference path length. However, for the Agilent 10719A and Agilent 10721A differential interferometers, the deadpath distance sign depends on the measurement mirror position during reset. For example, if the measurement and reference mirrors are located coplanar during reset, the deadpath distance is -19 mm (-0.750 inch).

Even with this correction, a small error still remains because of the repeatability of the compensation number determination. This deadpath correction error is given as:

Deadpath Correction Error = Deadpath Distance × Wavelength Compensation Number Repeatability (9)

The error in measuring the deadpath distance can generally be ignored if its measurement tolerance is within  $\pm 0.5$  mm. Deadpath error and deadpath correction error are both proportional values that are specified in parts-per-million. However, the measurement error is a function of deadpath distance, rather than the distance measured by the interferometer.

Using the Agilent 10717A Wavelength Tracker and software correction, the deadpath correction error will be less than  $\pm (0.14 \text{ ppm} \times \text{deadpath distance})$ .

### Abbé error

Abbé error was first described by Dr. Ernst Abbé of Zeiss: "If errors of parallax are to be avoided, the measuring system must be placed co-axially (in line with) the line in which displacement (giving length) is to be measured on the work-piece".

In simple terms, Abbé error occurs when the measuring point of interest is displaced from the actual measuring scale location and unwanted angular motion occurs in the positioning system.

Abbé error makes the indicated position either shorter or longer than the actual position, depending on the angular offset. The Abbé error is a fixed term and can be represented as:

Abbé error = offset distance × tangent of offset angle =  $A_0 \tan \theta$ 

Figure 54 shows an example of Abbé error, and illustrates the requirements for minimizing angular error and minimizing offset of the scale from the measurement path. In Figure 54(A), the carriage is positioned by a leadscrew and the measurement axis is at the leadscrew centerline. This figure illustrates the displacement (Abbé) error E, which is generated at the measurement probe tip due to unwanted angular motion ( $\theta$ ) of the carriage during the measurement. Figure 54(B) shows the same carriage motion as Figure 54(A), but with the measurement axis coincident with the probe path. Here, the measurement system measures the actual displacement, thus no Abbé error exists. In general, reducing the Abbé offset will reduce sensitivity to unwanted angular motions.

### ABBE OFFSET

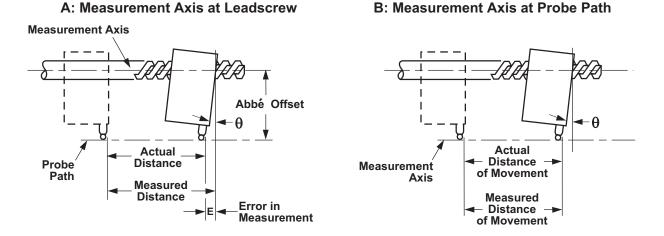


Figure 54 Abbé error

As a general rule, Abbé error is approximately 0.1 micron per 20 mm of offset for each arc-second of angular motion. Abbé error can occur with any type of displacement transducer.

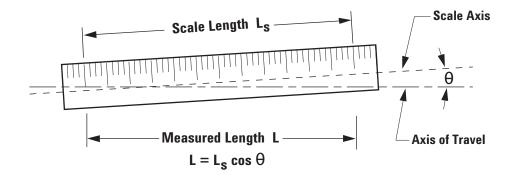
In high-accuracy applications where it is not possible to completely eliminate the Abbé effect, you may measure the unwanted angular displacement directly, and then correct for Abbé errors via software. A variety of interferometers can serve this purpose — particularly the Agilent 10719A (when used as an angle-measuring optic), the Agilent 10735A, or the Agilent 10736A, for plane mirror of X-Y stage applications.

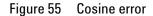
### **Cosine error**

Misalignment of the measurement axis (the laser beam) to the mechanical axis of motion results in an error between the measured distance and the actual distance traveled. This error is called cosine error, because its magnitude is proportional to the cosine of the angle of misalignment. Cosine error is common to all position transducers. If the laser alignment is unchanged over time, the cosine error will not change. Therefore, cosine error is part of the accuracy budget, but not part of the repeatability budget. Figure 55 illustrates cosine error, using a ruler as a scale, with an angle  $\theta$  between the measurement axis and the scale axis. Measured length, "L", is related to scale length, "Ls", by:

$$L = L_s \cos \theta \tag{11}$$

**COSINE ERROR** 





Cosine error is a proportional term; that is, the resulting measurement error is a function of the distance measured by the interferometer. Therefore, the cosine error can be represented, in parts-per-million, as:

Cosine error in ppm = 
$$(1 - \cos \theta) \times 10^6$$
 (12)

Cosine error can be eliminated by taking care to orient the measurement laser beam parallel to the actual axis of travel. Use the proper alignment procedures for each type of interferometer. For example:

- with interferometers using plane mirror reflectors (Agilent 10706A/B, Agilent 10715A, Agilent 10716A), the resulting cosine error is less than 0.05 ppm.
- with interferometers that use cube comer reflectors (Agilent 10702A, Agilent 10705A), the cosine error in parts-per-million is approximately equal to  $31250/L^2$ , where L is the measured distance in millimeters.

## **Determining System Accuracy and Repeatability**

The measurement accuracy and repeatability of a laser interferometer system are determined by summing all the error components previously discussed. The error components used to determine the measurement repeatability are a subset of the accuracy components. Table 13 shows the list of components for these error budgets and how the totals are determined. As shown in Table 13, the only differences between the two error budgets are the laser wavelength terms and the cosine error not being part of the repeatability error budget.

	Laser Interferometer System	
	Accuracy is the Sum of	Repeatability is the Sum of
Proportional Terms	Laser Wavelength Accuracy	Laser Wavelength Stability
	Atmospheric Compensation	Atmospheric Compensation
	Material Thermal Expansion	Material Thermal Expansion
	Cosine Error	not applicable
	Deadpath Error	Deadpath Error
Fixed Terms	Electronics Error (Resolution)	Electronics Error (Resolution)
	Optics Non-Linearity	Optics Non-Linearity
	Optics Thermal Drift	Optics Thermal Drift
	Abbé Error	Abbé Error

Table 13 Laser interferometer system accuracy and repeatability error

All these terms can be directly summed to determine the worst-case system accuracy and repeatability. However, taking the vector sum of the individual components results in a more realistic or typical system performance<sup>\*</sup>. Again, these components are categorized into proportional terms or fixed terms. The resulting measurement errors from proportional terms are a function of the distance measured. Fixed terms are noncumulative and the resulting measurement errors are not a function of the distance measured.

Repeatability error components can also be divided into short-term (< 1 hour) and long-term (> 1 hour) components. For short-term repeatability, only a subset of the total error components is included. Generally, the optics and material thermal effects are negligible over a short period of time, and these components are deleted from the short-term repeatability error budget. Additionally, short-term laser wavelength stability is used instead of long-term wavelength stability, and atmospheric changes, especially pressure, will also be smaller.

\*Steinmetz, C.R., Displacement Measurement Repeatability in Tens of Manometers with Laser Interferometry, Proc. SPIE, Vol. 921, p.406-420, 1988.

# **Examples** — Determining System Accuracy and Repeatability

The examples below illustrate the calculation of measurement accuracy and repeatability of Agilent laser measurement systems for two typical applications.

In the first example, the laser system is part of a precision coordinate measuring machine (CMM) and monitors the position of the touch probe on the machine. In this example, accuracy and long-term repeatability will be determined.

In the second example, the laser measurement system is built into an integrated circuit manufacturing system, such as a wafer stepper or inspection machine, and controls the position of the wafer stage. For this example, accuracy, long-term repeatability, and short-term repeatability will be determined. Short-term repeatability is calculated for the wafer stepper application because process time for wafer exposures is typically very short (< 2 minutes). Table 14 shows a list of parameters needed to calculate each error component.

System Error Component	Parameters
Laser Wavelength	Measurement Distance (L), Laser Specifications
Atmospheric Compensation	Measurement Distance (L), Environmental Conditions, Compensation Performance
Material Thermal Expansion	Measurement Distance (L), Material Temperature, Material
Cosine Error	Measurement Distance (L), Interferometer Type, Misalignment Angle
Deadpath Error	Deadpath Distance, Environmental Conditions, Compensation Performance
Electronics Error (Resolution)	Interferometer Type, Electronics
Optics Non-Linearity	Interferometer Type
Optics Thermal Drift	Interferometer Type, Temperature Changes
Abbé Error	Abbé Offset, Angular Changes

 Table 14
 Parameters needed to calculate each error component

# Precision Coordinate Measuring Machine (CMM) example

The typical configuration for this application is shown in Figure 56. It uses Agilent 10716A High Resolution interferometers and the Agilent 10717A Wavelength Tracker. This CMM has a working measurement volume of 1.0 m  $\times$  1.0 m  $\times$  1.0 m.

Dimensions: see figure below

Maximum distance measured (L): 1.0 m

Deadpath distance (D): 0.1 m

Cosine Error: 0.05 ppm (Agilent 10716A aligned according to procedure in this manual)

Nonlinearity: ±1.0 nm (Agilent 10716A)

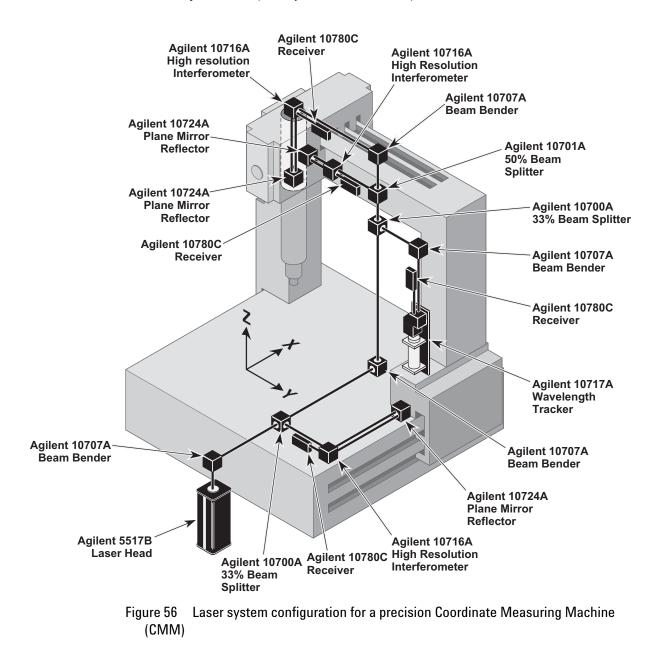
Abbé error: none (assume zero offset)

Measurement resolution: ±2.5 nanometers (Agilent 10716A)

#### ENVIRONMENT:

Temperature: 20 °C ±0.5° (temperature controlled environment)

**Pressure:** 760 mm Hg ±25 mm Hg (possible storm fronts during measurement, pressure not controlled) **Humidity:** 50% ±10% (humidity controlled environment)



A list of parameters needed to calculate the system's measurement accuracy and repeatability for this application is provided the following subsections. The laser head and optics' component specifications are taken from this manual, system resolution specifications for Agilent laser transducer electronics (Agilent 10885A, Agilent 10895A, Agilent 10897B, and Agilent 10898A) are taken from the manual of the respective electronic board, and the Agilent 10751C/D Air Sensor and Agilent 10757D/E/F Material Temperature Sensor environmental specifications are provided in this chapter.

Each error component is calculated individually and summed in the appropriate error budget to determine system accuracy and repeatability.

#### Laser wavelength error

When using a CMM, both accuracy and long-term repeatability need to be calculated.

Laser Wavelength Stability: ±0.02 ppm (long-term)

This translates to a maximum distance uncertainty of:

Laser Wavelength Stability Error =  $(1.0 \text{ m}) (\pm 0.02 \times 10^{-6})$ (long-term) =  $\pm 0.02$  micron

**Laser Wavelength Accuracy:** ±0.02 ppm (with optional calibration)

Laser Wavelength Accuracy Error =  $(1.0 \text{ m}) (\pm 0.02 \times 10^{-6})$ =  $\pm 0.02 \text{ micron}$ 

#### **Atmospheric compensation**

Since the wavelength tracker provides relative compensation information, the initial compensation number from another source determines the compensation accuracy. In this example, the initial compensation number is derived from measuring a known artifact or standard with the laser system on the machine. The accuracy of measuring the artifact or standard is the sum of the laser system measurement repeatability, machine repeatability and touch probe accuracy. It is assumed that no error is induced in measuring the artifact. Consequently, in this example, accuracy and repeatability of atmospheric compensation information will be equal.

Using Equation 4 (given earlier in this chapter) and the specified environmental conditions, accuracy and repeatability of compensation information from wavelength tracker can be determined. Compensation accuracy and repeatability =

$$\pm \left[ 0.067 ppm + \frac{0.06 ppm}{degree C} \times 0.5 degree C + \frac{0.002 ppm}{mm Hg} \times 25 mm Hg \right]$$
$$= \pm 0.15 ppm$$

At maximum distance the position uncertainty, due to compensation, will be:

Compensation Error =  $(1.0 \text{ m}) (\pm 0.15 \times 10^{-6}) = \pm 0.15 \text{ micron}.$ 

With no atmospheric compensation, the error would be  $\pm 9.0$  ppm. This translates to a position uncertainty, at the maximum distance of 1 m, of 9.0 microns.

#### Material thermal expansion

On a CMM, with a laser interferometer system used as the position scale, material compensation should be done to the measured part, not the machine. Therefore, the material temperature error term depends on the type of material being measured and the specifications of the temperature sensor. This can be a significant error if the temperature of the part is not tightly controlled or compensation is not adequate. For example, with a 0.5 m part made of steel ( $\alpha = 0.00 \text{ ppm/}^{\circ}\text{C}$ ) and using the Agilent 10757D/E/F Material Temperature Sensor, the resulting measurement accuracy and repeatability will be:

Measurement Accuracy =  $\alpha \times$  temperature sensor repeatability × part length =  $\frac{10.0 \, ppm}{degree \, C} (\pm 0.1 \, degree \, C \times 0.5 m)$ =  $\pm 0.5 \, \text{micron}$ 

The Agilent 10757D/C/E temperature sensor has a measurement repeatability equal to its accuracy.

Measurement Repeatability =  $\pm 0.5$  micron

Since this error is independent of the type of measurement scale but strongly dependent on the type of material and temperature sensor performance, specific errors will not be included in this example. However, this error should be included when calculating the error budget for an actual machine.

Material Thermal Expansion = 0 micron (assumed)

### **Deadpath error**

Deadpath error is a function of deadpath distance, method of compensation, and environmental conditions. With no compensation for deadpath, Equation 7 determines the error.

Deadpath Error =  $(0.1 \text{ m}) (\pm 9 \times 10^{-6}) = \pm 0.9 \text{ micron}$ 

With deadpath correction and using Wavelength Tracking Compensation, Equation 9 determines the error.

Deadpath correction error =  $(0.1 \text{ m}) (\pm 0.15 \times 10^{-6}) = \pm 0.015 \text{ micron}$ 

### **Electronics error**

With Agilent laser interferometer systems, the electronics error equals measurement resolution. When using the Agilent 10716A High Resolution Interferometer, system measurement resolution (for Agilent 10885A, Agilent 10895A, Agilent 10897B, or Agilent 10898A electronics) is:

Measurement Resolution = 0.0025 micron

### **Optics nonlinearity**

Nonlinearity when using the Agilent 10716A High Resolution Interferometer is  $\pm 0.001$  micron.

### **Optics thermal drift**

This error term should be included when determining long-term repeatability. The error depends on the degree of thermal cycling that the interferometer experiences. With the Agilent 10716A in this application, typical thermal drift will be:

 $Optics Thermal Drift = \frac{0.04 \ micron}{degree \ C} \times (\pm 0.5 \ degree \ C) \times \pm 0.02 \ micron$ 

#### Abbé error

Since this error term is independent of the type of measurement scale used, but strongly dependent on how the machine is designed and built, specific errors will not be included in this example. However, the errors should be included when calculating the error budget for an actual machine when the Abbé offset is known and angular errors can be measured or estimated.

Abbé Error = 0 micron (assumed)

### **Cosine error**

If the proper alignment procedure for the Agilent 10716A is followed, the worst-case cosine error is:

Cosine Error = ±0.05 ppm

Cosine Error (in microns) = ( $\pm 0.05$  ppm) (1.0 m) =  $\pm 0.05$  micron

### CMM system accuracy calculation

Now the appropriate components can be summed together to obtain system measurement accuracy and repeatability. Worst-case system accuracy and repeatability is determined by directly summing these components. However, a more realistic, but still conservative, system repeatability is the vector sum (RSS, Root Sum of Squares) of the individual components. System accuracy and repeatability will be calculated with and without atmospheric compensation to show the importance of compensating for changes in atmospheric conditions. The results are presented in Table 15.

	System Accuracy Calculation	
	With Atmospheric Compensation <u>+(</u> microns)	Without Atmospheric Compensation ±(microns)
Laser Wavelength Error	0.02	0.02
Compensation Error	0.15*	9.0*
Material Thermal Expansion	0.0	0.0
Deadpath Error	0.015*	0.90*
Electronics Error	0.0025	0.0025
Optics Non-Linearity	0.001	0.001
Optics Thermal Drift	0.02	0.02
Abbé Error	0.0	0.0
Cosine Error	0.05 #	0.05 #
Direct Sum Total	±0.26 micron	±9.99 microns
RSS sum where *'s are not independent and # is an offset.	±0.22 micron	±9.95 microns

Table 15 System accuracy with and without atmospheric compensation

The following equation is used to calculate the RSS sum:

RS sum = [(sum of squares of independent terms) + (sum of not independent terms<sup>2</sup>)]<sup>1/2</sup> + offset

Figure 57 graphically presents this accuracy data and shows the importance of using atmospheric compensation. Figure 58 shows in more detail the relative magnitude of each component when using atmospheric compensation.

#### WORST-CASE SYSTEM ACCURACY — CMM EXAMPLE

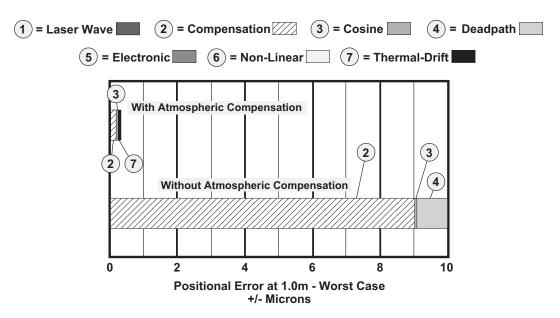
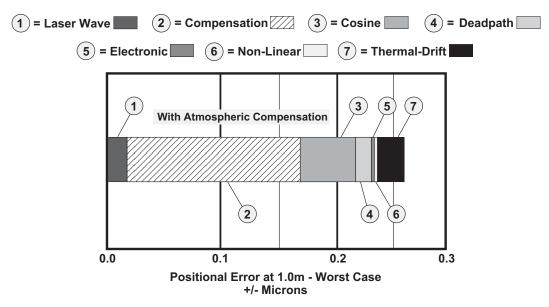
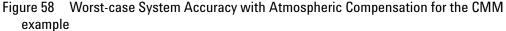


Figure 57 Worst-case System Accuracy with and without Atmospheric Compensation for the CMM example

#### WORST-CASE SYSTEM ACCURACY WITH ATMOSPHERIC COMPENSATION — CMM EXAMPLE





### CMM system repeatability calculation

Calculation of laser system long-term repeatability in this example is the same as system accuracy except that the cosine error term ( $\pm 0.05$  micron) is not included. Therefore, system repeatability in this example will be:

	-	Without Atmospheric Compensation
Direct Sum Total (Worst Case)	±0.21 micron	±9.94 microns
RSS sum (Typical)	±0.17 micron	±9.90 microns

Figure 59 is a graph of the worst-case repeatability. Again it shows the importance of atmospheric compensation. Figure 60 shows in more detail the worst-case repeatability with atmospheric compensation.

### WORST-CASE SYSTEM REPEATABILITY — CMM EXAMPLE

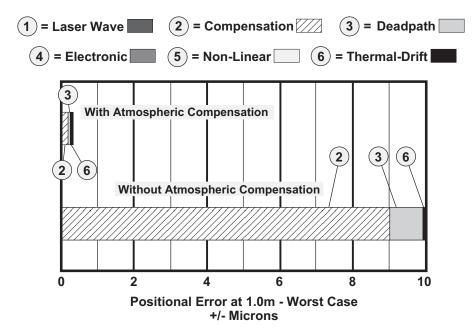


Figure 59 Worst-case System Repeatability with and without Atmospheric Compensation for the CMM example

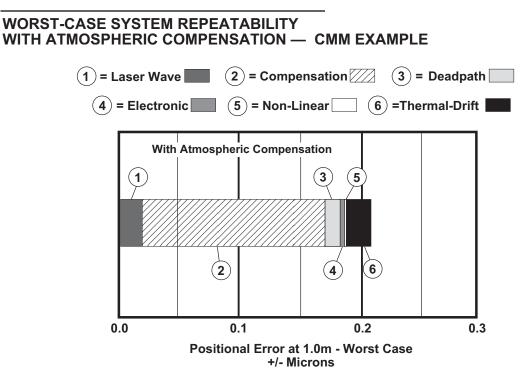


Figure 60 Worst-case System Repeatability with Atmospheric Compensation for the CMM example

### IC Wafer Stepper example

In this example, the laser system is built into an Integrated Circuit Wafer Stepper and controls the position of the wafer stage. A typical configuration for this application is shown in Figure 61. It uses Agilent 10706B High Stability Plane Mirror Interferometers and an Agilent 10717A Wavelength Tracker. Following is a list of parameters needed to calculate the system accuracy and repeatability. The laser head and optics' component specifications are taken from this manual, system resolution specifications for Agilent laser transducer electronics (Agilent 10885A, Agilent 10895A, Agilent 10897B, and Agilent 10898A) are taken from the manual of the respective electronic board, and the Agilent 10751C/D Air Sensor and Agilent 10757D/E/F Material Temperature Sensor environmental specifications are provided in this chapter. Dimensions: see figure below Maximum distance measured (L): 0.2 m Deadpath distance (D): 0.1 m Cosine Error: 0.05 ppm (Agilent 10706B aligned according to procedure in this manual) Nonlinearity: ±2.2 nm (Agilent 10706B) Abbé error: none (assume zero offset) Measurement resolution: ±5 nanometers (Agilent 10706B) ENVIRONMENT: Temperature: 20° C ±0.1° (temperature controlled environment) Pressure: 760 mm Hg ±25 mm Hg (possible storm fronts during measurement, pressure not controlled) Humidity: 50% ±10% (humidity controlled environment)

# LASER SYSTEM CONFIGURATION ON I.C. WAFER STEPPER

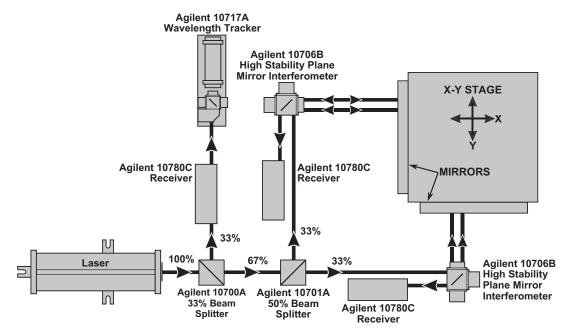


Figure 61 Laser System Configuration for an Integrated Circuit Wafer Stepper

Each error component will be calculated individually and then summed to determine system repeatability.

#### Laser wavelength error

The time required for an operation by IC fabrication equipment is often only a few minutes. Thus, accuracy, long-term stability, and short-term stability need to be calculated.

Laser Wavelength Stability: ±0.002 ppm (short-term)

This translates to a maximum distance error of:

Laser Wavelength Stability Error =  $\pm 0.2 \text{ m} (\pm 0.002 \times 10^{-6})$ (short- term) =  $\pm 0.0004 \text{ micron}$ 

Laser Wavelength Stability: ±0.02 ppm (long-term)

Laser Wavelength Stability Error =  $0.2 \text{ m} (\pm 0.02 \times 10^{-6})$ (long-term) =  $\pm 0.004 \text{ micron}$ 

Laser Wavelength Accuracy: ±0.02 ppm (with optional calibration)

Laser Wavelength Accuracy Error =  $0.2 \text{ m} (\pm 0.02 \times 10^{-6})$ =  $\pm 0.004 \text{ micron}$ 

#### **Atmospheric compensation**

Since the wavelength tracker provides relative compensation information, the initial compensation number from another source determines the compensation accuracy. In this example, the initial compensation number is obtained by measuring a known artifact or standard with the laser system. The accuracy of measuring the artifact is the sum of the laser system measurement repeatability, machine repeatability, and the accuracy of the alignment mark sensing system. It is assumed that no error is induced in measuring the artifact on the machine. Consequently, in this example accuracy and repeatability of the atmospheric compensation information will be equal.

Using Equation 4 and the specified environmental conditions, accuracy and repeatability of compensation information from wavelength tracker can be determined.

Compensation accuracy and repeatability =

$$\pm \left[ 0.067 ppm + \frac{0.06 ppm}{degree C} \times 0.1 \ degree \ C + \frac{0.002 ppm}{mm \ Hg} \times 25 \ mm \ Hg \right]$$
$$= \pm 0.14 \text{ ppm}$$

At maximum distance, the position error, due to compensation, will be:

Compensation Error =  $(0.2 \text{ m} \times \pm 0.14 \times 10^{-6}) = \pm 0.028 \text{ micron}$ 

With no atmospheric compensation, the error would be  $\pm 9.0$  ppm. This translates into a position error of 1.8 microns.

### Material thermal expansion

This error depends on the machine design and the position that is measured or controlled. On a wafer stepper, the wafer is positioned relative to the optical column. If the measurement axes are placed to allow measurements between the wafer and optical column (for example, using an Agilent 10719A or Agilent 10721A differential interferometer), material temperature effects may be ignored. This assumes the material expansion in the measurement path is equal to that in the reference path.

Material Thermal Expansion = 0 micron (assumed)

### **Deadpath error**

Deadpath error is a function of deadpath distance, method of compensation, and environmental conditions. With no compensation for deadpath, Equation 7 determines the error.

Deadpath Error =  $(0.1 \text{ m}) \times (\pm 0.9 \times 10^{-6}) = \pm 0.9 \text{ micron}$ 

With deadpath correction and the use of the wavelength tracker, Equation 9 determines the error.

Deadpath correction error =  $(0.1 \text{ m}) \times (\pm 0.14 \times 10^{-6}) = \pm 0.014 \text{ micron}$ 

### **Electronics error**

With Agilent laser interferometer systems, the electronics error equals the measurement resolution. When using the Agilent 10706B High Stability Plane Mirror Interferometer, system measurement resolution (for the Agilent 10885A, Agilent 10895A, Agilent 10897B, or Agilent 10898A electronics) is:

Measurement Resolution = 0.005 micron

### **Optics nonlinearity**

Nonlinearity when using the Agilent 10706B High Stability Plane Mirror Interferometer is ±0.0022 micron.

### **Optics thermal drift**

Because the measurement repeatability of this piece of equipment is important, the effects of thermal changes of the interferometer should be included. With the Agilent 10706B High Stability Plane Mirror Interferometer, typical thermal drift will be:

 $Optics \ Thermal \ Drift = \frac{0.04 \ micron}{degree \ C} \times (\pm 0.1 \ degree \ C) = \pm 0.004 \ micron$ 

### Abbé error

In X-Y stage applications, it is usually easy to have the interferometer measurement axis in line with the wafer. Therefore, Abbé offset will be zero and no Abbé error will occur.

Abbé Error = 0 micron

### **Cosine error**

If the proper alignment procedure for the Agilent 10706B High Stability Plane Mirror Interferometer is followed, the worst-case cosine error is:

Cosine Error =  $\pm 0.05$  ppm

Cosine Error (in microns) = ±0.05 ppm × 0.2 m = ±0.01 micron

### **IC Stepper System accuracy calculation**

Now you can sum the appropriate components together to obtain system measurement accuracy and repeatability. Worst-case system accuracy and repeatability is determined by directly summing these components. However, a more realistic, but still conservative, system repeatability is the vector sum (RSS, Root Sum of Squares) of the individual components. System accuracy and repeatability will be calculated with and without atmospheric compensation to show the importance of compensating for changes in atmospheric conditions. The results are presented in Table 16.

	System Accuracy Calculation	
	With Atmospheric Compensation ±(microns)	Without Atmospheric Compensation ±(microns)
Laser Wavelength Error	0.004	0.004
Compensation Error	0.028*	1.8*
Material Thermal Expansion	0.0	0.0
Deadpath Error	0.014*	0.90*
Electronics Error	0.005	0.005
Optics Non-Linearity	0.0022	0.0022
Optics Thermal Drift	0.004	0.004
Abbé Error	0.0	0.0
Cosine Error	0.01 #	0.01 #

 Table 16
 IC Stepper system accuracy with and without atmospheric compensation

#### 12 Accuracy and Repeatability

Table 16 IC St	epper system accuracy	y with and without at	tmospheric compensation
----------------	-----------------------	-----------------------	-------------------------

	System Accuracy Calculation	
Direct Sum Total	±0.067 micron	±2.725 microns
RSS sum where *'s are not independent and # is an offset.	±0.053 micron	±2.710 microns

Use the following equation to calculate the RSS sum:

RS sum = [(sum of squares of independent terms) +

 $(\text{sum of not independent terms}^2)^{\frac{1}{2}} + \text{offset}$ 

Figure 62 graphically presents this accuracy data and shows the importance of using atmospheric compensation. Figure 63 shows in more detail the relative magnitude of each component when using atmospheric compensation.

### WORST-CASE SYSTEM ACCURACY - I.C. WAFER STEPPER

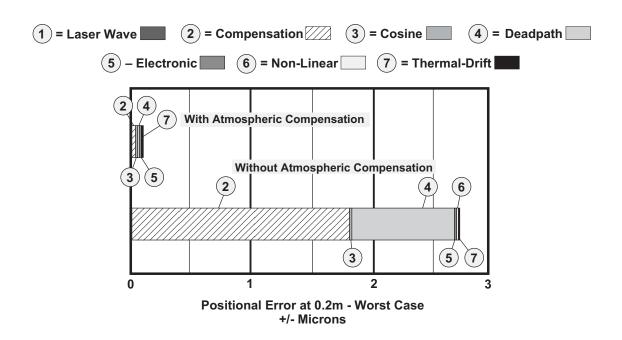
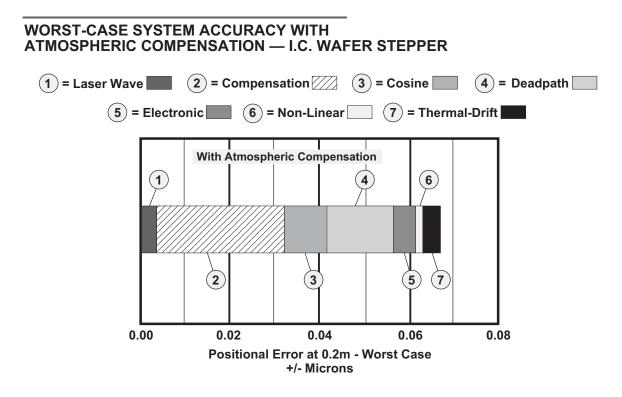


Figure 62 Worst-case System Accuracy with and without Atmospheric Compensation for the Wafer Stepper example



#### Figure 63 Worst-case System Accuracy with Atmospheric Compensation for the Wafer Stepper example

Another potential source of error that should be included in the total accuracy budget is the flatness of the measurement mirrors. In X-Y stage applications, long mirrors are attached to two sides of the stage, as shown in Figure 61. Because the mirrors are not perfectly flat, a measurement change occurs in one axis as the other axis is moved. Since a mirror flatness of  $\lambda/20$  is recommended for correct operation of the laser system, this would induce a maximum measurement error of 0.03 micron. To compensate for this measurement error, map the mirror flatness, then make the correction via software in the controller.

### IC Stepper system repeatability calculations

**Long-term repeatability** Calculation of laser system long-term repeatability in this example is the same as system accuracy, except that the cosine error term ( $\pm 0.01$  micron) is not included. Therefore, laser system long-term repeatability will be:

	With Atmospheric Compensation	Without Atmospheric Compensation
Direct Sum Total (Worst Case)	±0.057 micron	±2.715 microns
RSS sum (Typical)	±0.043 micron	±2.710 microns

Figure 64 is a graph of the worst-case long-term repeatability. Again, the importance of atmospheric compensation is shown. Figure 65 shows in more detail the worst-case long-term repeatability with atmospheric compensation.

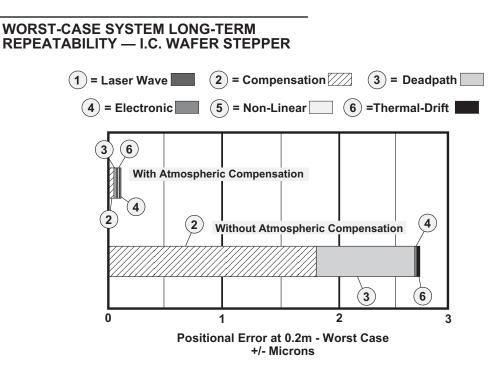
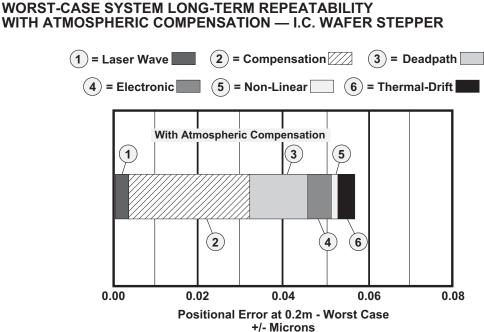


Figure 64 Worst-case System Long-term Repeatability with and without Atmospheric Compensation for the Wafer Stepper example



# WITH ATMOSPHERIC COMPENSATION — I.C. WAFER STEPPER

Figure 65 Worst-case System Long-term Repeatability with Atmospheric Compensation for the Wafer Stepper example

**Short-term repeatability** In this example, calculation of system short-term repeatability is the same as long-term repeatability except: 1) long-term laser wavelength error is replaced by short-term error, and 2) optics thermal drift is not included. The atmospheric compensation error is assumed to be the same. However, under normal operating conditions, atmospheric pressure changes would generally be substantially less than those used in this example for the short periods of interest in IC fabrication.

	With Atmospheric Compensation	Without Atmospheric Compensation
Direct Sum Total (Worst Case)	±0.050 micron	±2.708 microns
RSS sum (Typical)	±0.042 micron	±2.700 microns

As seen from these values, the difference between system long-term and short-term repeatability is only a few nanometers. If the assumed short-term environmental changes (especially atmospheric pressure) are much smaller, then short-term repeatability will be significantly smaller.

# **Achieving Optimum System Accuracy and Repeatability**

To achieve the best measurement accuracy and repeatability from a laser interferometer system in your application:

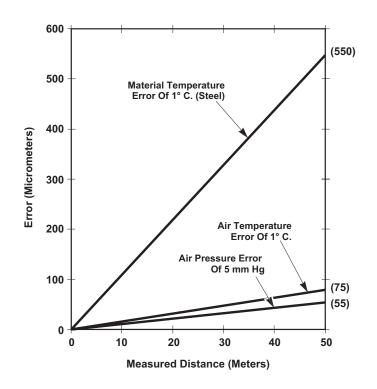
- 1 Whenever possible, make the measurements in a tightly-controlled, stable environment. Also, use the appropriate compensation methods to correct for atmospheric and material temperature effects.
- 2 When designing a machine to use a laser interferometer system, minimize both deadpath distances and Abbé offsets. If a deadpath exists on the machine, correct for it during measurements.
- 3 For each measurement axis, be sure to properly align optical components during installation to minimize the amount of cosine error.
- 4 Use the proper components for the particular application. If significant changes in environmental conditions are expected, use automatic compensation and interferometers with minimal thermal drift.

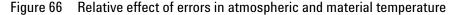
Additional details are presented below.

### **Minimizing environmental effects**

The relative importance of typical atmospheric effects and material temperature errors is shown in Figure 66. Measurement errors due to material temperature errors are especially important in many applications. Ideally, all distance measurements with the laser system would be made in a temperature-controlled room held at exactly 20°C (68° F), the standard temperature. Then the machine or part would be at its "true" size and the wavelength compensation number determined earlier could be used directly.

#### RELATIVE EFFECT OF ERRORS





Laser measurement errors from environmental effects can be corrected by using a combined compensation term called the "Total Compensation Number" or "TCN". It contains a Wavelength-of-Light compensation term (WCN) and a Material Temperature compensation term (MTC). These terms were described individually earlier in this chapter. The WCN is Equation 2, and the MTC is Equation 5. The TCN is determined from the WCN and MTC as follows:

$$TCN = WCN \times MTC$$
(13)

Expanding the WCN and MTC terms, we get:



The Wavelength-of-Light term compensates for changes in the laser wavelength. The material temperature term corrects the measurement back to standard temperature. Recall from the earlier section on atmospheric compensation that the laser position transducer counts the number of wavelengths of motion traveled. This measurement can then be corrected for atmospheric effects by multiplying the distance by a correction factor, the WCN. The result was given in Equation 3:

Actual Displacement (true position) = (Wavelength counts) × WCN × vacuum Wavelength (3)

We can now combine the compensation for both atmospheric and material temperature effects and calculate the "true" length of the object at standard  $20^{\circ}$  C temperature. Using equations (3) and (13) we get:

```
Actual Length = (Wavelength counts) × TCN
× vacuum Wavelength (15)
```

### Laser compensation capability

The laser system electronics can accept a manually-entered Total Compensation Number (TCN) or automatically determine the TCN, if a compensation board is installed.

### **Manual compensation**

For manual compensation, the Total Compensation Number (TCN) is entered through the system controller to the Agilent laser electronics. The TCN can be calculated via Equation 13 or 14. See Chapter 13, "Wavelength-of-Light Compensation," for Wavelength Compensation numbers and the method to calculate them manually. See Chapter 14, "Material Expansion Coefficients," for information about Material Temperature compensation numbers.

Manual compensation can also be done without deriving or looking up the factors, by using the appropriate Agilent automatic compensation board for the Agilent laser electronics. The compensation board computes compensation factors from the environmental data (atmosphere and machine or part temperature) entered manually through the controller to the Agilent electronics.

### Automatic compensation

With most Agilent laser electronics, the necessary information for wavelength compensation can be obtained automatically by using the appropriate Agilent automatic compensator board and environmental sensors. WOL compensation is provided by using either the Agilent 10751C/D Air Sensor to measure air temperature, pressure, and humidity, or the Agilent 10717A Wavelength Tracker to measure the laser wavelength change directly. The Agilent 10757D/E/F Material Temperature Sensor provides the temperature

data for the "Material Temperature" term. The Agilent automatic compensation board automatically provides an updated total compensation number (TCN).

The Agilent 10717A Wavelength Tracker and its accompanying Agilent 10780C, Agilent 10780F, Agilent E1708A, or Agilent E1709A receiver provide the Agilent automatic compensation board with information indicating any changes in the laser wavelength. Unlike the air sensor, the wavelength tracker measures relative (differential) changes in the laser wavelength with respect to an initial value. The absolute accuracy is dependent on this initial value. Some methods of determining an initial compensation number are by:

- using an Agilent 10751C/D Air Sensor.
- using look-up tables (such as those in Chapter 13, "Wavelength-of-Light Compensation," of this manual).
- measuring temperature, pressure and humidity, and then inputting these values into the automatic compensation board.
- measuring a known "standard" length.

To calculate the initial compensation number by measuring a known standard or artifact, use the following formula:

Compensation	Measured length (from laser system on machine)							
Number =	Actual length (from a "Standards" laboratory)							
NOTE	If relative compensation is satisfactory for your application, the values of initial compensation may be used. See the laser elec documentation for your system for details.							

## **Sensor placement**

To correct for the effects of air conditions on the laser reading, place the Agilent 10717A Wavelength Tracker or Agilent 10751C/D Air Sensor where it can accurately monitor the conditions influencing the laser beam. Mount the sensor as close as possible to the measurement path, so it monitors the condition of these laser beams.

### Agilent 10717A Wavelength Tracker

When you use the wavelength tracker, mount the unit on a stable surface so that alignment is maintained.

### Agilent 10751C/D Air Sensor

The air sensor should not be placed directly below the measurement beam path because the heat from the air sensor will affect the laser beam. The Agilent 10751C/D Air Sensor base contains a magnet to aid in securing it to magnetic materials. For permanent mounting, fasten the sensor using the #10-32 tapped hole on the bottom of the unit.

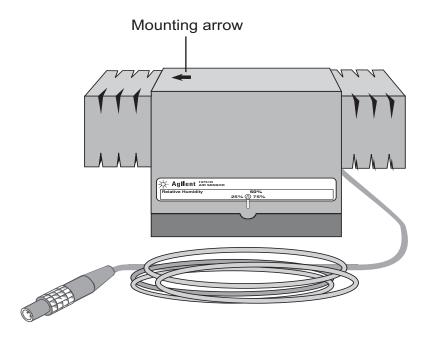


Figure 67 Air sensor orientation (Agilent 10751D shown)

NOTE

The Air Sensor should be mounted with its arrow pointing up, to maximize accuracy, as shown in Figure 67.

### Agilent 10757D/E/F Material Temperature Sensor

When monitoring material temperature to account for material expansion, the Agilent 10757D/E/F Material Temperature Sensor should be placed on the part of the machine closest to the workpiece.

The material temperature sensor contains a magnet to aid in securing it to ferrous materials. For permanent mounting, a clamp can be used to secure it. If two material temperature sensors are used, they should be placed to determine the average temperature of the workpiece. After attaching a probe to the workpiece, allow at least 10 minutes for the probe temperature to stabilize at the workpiece temperature.

# **WOL** compensation method comparison

The method of atmospheric (WOL) compensation used is important in determining the overall laser system measurement accuracy. Table 17 summarizes the laser system accuracy for various methods of atmospheric compensation as a function of different atmospheric conditions.

Table 17 Laser system measurement accuracy comparison\*

Environment:											
Pressure: 760 mm Hg ±25 mm Hg											
Relative Humidity: 50% ±10%											
Temperature Control	±0.1°C	±1.0°C	±5.0°C								
No Compensation† (at 20°C)	±9.0 ppm	±9.9 ppm	±14.0 ppm								
Compensation using Agilent 10751C/D Air Sensor (at 20° C)	±1.4 ppm	±1.5 ppm (typical)	±1.6 ppm								
Wavelength Tracking Compensation‡	±0.15 ppm	±0.19 ppm	±0.44 ppm								
Measurement in Vacuum	±0.1 ppm	±0.1 ppm	±0.1 ppm								
* These accuracy specifications include the l interferometer nonlinearity terms.	aser head term, but	exclude electronics a	accuracy and								
† No compensation means that no correction in compensation number occurs during environmental changes.											
‡ System accuracy equals these values (me compensation value.	asurement repeatab	ility) plus accuracy o	f initial								

# **Non-Uniform Environments**

Compensation for environmental effects is practical only when the material being measured is at a constant temperature, and when the medium through which the measurement laser beam passes is not disturbed (such as by air turbulence).

### **Changing temperature conditions**

Material temperature compensation is accurate only when the part and the machine are at thermal equilibrium with their surroundings. Changing temperature can change thermal gradients in both the machine and the part. In this case, the primary machine errors are due to complex bending effects which distort machine geometry, in addition to simple thermal expansion. These effects are extremely difficult, if not impossible, to describe mathematically.

Changing temperatures also affect the measurement optics, resulting in optics thermal drift as described earlier in this chapter. Therefore, if a machine is operated in a poor environment, its accuracy may be limited by its own geometry, thermal expansion, and optics thermal drift. In this case, the most practical solution is to improve the environment and use optics that are thermally stable.

### Air turbulence

Air Turbulence is an important factor to be considered during installation of a laser system. It is usually caused by variations in air temperature. The major effect of air turbulence is reduction of amount of signal at the receiver. This reduction is due to either physical deflection of the laser beam or degradation of the beam's coherence. Excessive air turbulence may cause complete loss of measurement signal. This loss of signal will be detected by the Agilent electronics which will output an error signal.

One application where serious consideration must be given to air turbulence is a temperature-controlled environment. Although it would appear that such an environment would be ideal, temperature-controlled areas often exhibit greater air turbulence than non-controlled areas. This turbulence is caused by incomplete mixing of new air from the temperature control unit with existing air, creating thermal gradients or pockets. Although such environments are good for a machine's thermal stability, the short term fluctuations can cause measurement signal degradation in the laser system.

#### **Reducing air turbulence**

In an uncontrolled environment, the effects of air turbulence can be minimized by protecting the laser beam with some type of cover. Since this would normally be done for protection against beam interruption, air turbulence effects will usually not be a significant installation factor in a typical environment.

Protection against air turbulence problems which occur in a controlled environment depends largely on the specific application. For systems such as integrated circuit lithography equipment in small closely-controlled enclosures, it may be sufficient to provide constant air flow over the measurement paths. In other cases, such as large coordinate measuring machines, protecting the laser beams with covers prevents air turbulence effects from interfering with the measurement.

### Avoiding thermal gradients

One source of air turbulence, which can affect both the laser system and also the accuracy of the machine itself, is thermal gradients created by localized heat sources (e.g., motors, electromagnetics, lamps, etc.) located on or near the machine. You should shield the measurement path from these types of heat sources. A key benefit of the Agilent 10780F, Agilent E1708A, and Agilent E1709A remote receivers is that they allow remote mounting of the receiver electronics, eliminating its 2 watts of heat from the measurement area. The remote (fiber-optic) pickup is entirely passive and dissipates no heat.

A local heat source which can affect the laser system enough to cause measurement signal loss also tends to degrade the geometric accuracy of the machine through warping or bending. Therefore, you should consider thermally isolating the heat source from the machine as well as the measurement path.

### **Optics installation effects**

When planning the installation of the laser head and optics on a specific machine, important points to remember are:

- Install the interferometer and retroreflector to minimize deadpath errors.
- Align the laser beam path parallel to the axis of motion to minimize cosine errors.
- Select the measurement paths to minimize Abbé error.
- Use thermally stable optics.

These effects are not a concern for the optical axis used for the Agilent 10717A Wavelength Tracker. The components of the wavelength tracker are aligned at the factory to minimize any cosine or Abbé errors.

In many cases, it may not be possible to completely eliminate these sources of error, but every effort should be made to minimize them. The paragraphs below discuss methods of installing and compensating for these errors.

### Minimizing deadpath errors

Deadpath error is an error introduced due to an uncompensated length of laser light between the interferometer and the retroreflector when the machine is at its "zero" position.

Deadpath is the difference in optical path lengths between the reference and measurement components of the beam when the positioning stage or machine is at its zero position, as defined by the machine's coordinate system. Unequal beam components produce an optical path length difference that will not be properly compensated during changing environmental conditions, resulting in a measurement error. The optical path can differ due to unequal path lengths or different optics (thickness or composition) in the beam path.

Deadpath error can be minimized in most applications by a combination of the following:

- Minimize the distance "D". Mount the interferometer as close to the retroreflector as possible when the machine is at its zero position as defined by its own coordinate system. This minimizes the unequal path length cases.
- Minimize unequal path treatments as much as possible. Minimize the number of optics, such as windows, used in the beam path.
- Use an Agilent 10715A Differential Interferometer or Agilent 10706B High Stability Plane Mirror Interferometer instead of the Agilent 10706A Plane Mirror Interferometer. Some unequal path treatment cannot be avoided with the Agilent 10706A Plane Mirror Interferometer. The other interferometers have negligible difference in their treatments. Figure 49 shows that component  $f_A$  travels through more glass than does  $f_B$ . It makes twice as many trips through the interferometer as does  $f_A$ , and also two round trips through the quarter-wave plate. This unequal treatment of  $f_A$  and  $f_B$ , causes deadpath errors under changing conditions.
- Correct the residual distance "D" in software in the controller.
- Equalize the path lengths of  $f_B$  and  $f_A$  by moving the reference cube-corner a distance "D" from the interferometer. (See Figure 68). Assuming the atmospheric conditions are equivalent and the distances between the cube-corners and the interferometer are equal, this configuration would not have deadpath errors due to unequal path lengths. Take care when using this method of reducing deadpath, because any drift in the position of the reference cube-corner will also show up as a measurement error. This drift can result from non-rigid mounting and thermal expansion, for example.

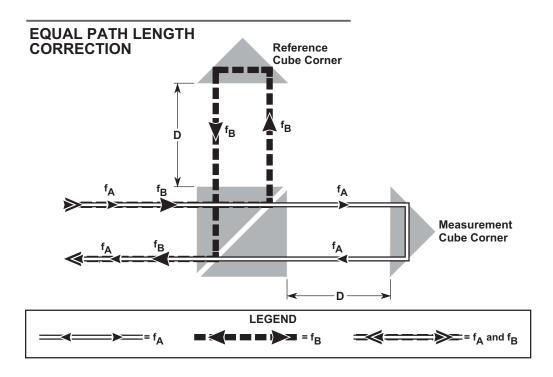


Figure 68 Equal path length correction

### **Compensation for deadpath errors**

Correction for deadpath error (unequal path length) is necessary if there is a change in the laser wavelength due to environmental conditions. Compensation for deadpath error can be done by correcting for the deadpath distance "D" in software in the controller. In this case, the general relation:

True Position = Wavelength counts due to motion × vacuum wavelength × TCN

is expanded to be:

True Position = [(Accumulated Counts + Deadpath Counts) × Wavelength Conversion Factor × TCN] - (Deadpath in selected units)

Accumulated raw counts is the actual output from the electronics rather than the number of wavelengths.

For the Agilent 10716A interferometer, a displacement count equals  $\lambda/256$ , where  $\lambda$  is the wavelength of the laser in air, for Agilent laser electronics.

When using one of the interferometers listed below, an actual displacement count is equal to  $\lambda/(4 \times$  Electronics Resolution Extension Factor), where  $\lambda$  is the wavelength of the laser in air, for Agilent laser electronics:

- Agilent 10706A/B Plane Mirror Interferometer
- Agilent 10715A Differential Interferometer
- Agilent 10719A One-Axis Differential Interferometer
- Agilent 10721A Two-Axis Differential Interferometer
- Agilent 10735A Three-Axis Differential Interferometer
- Agilent 10736A Three-Axis Differential Interferometer
- Agilent 10736A-001 Three-Axis Differential Interferometer with Beam Bender
- Agilent E1826E/F/G One-Axis Plane Mirror Interferometer
- Agilent E1827A Two-Axis Interferometer
- Agilent E1837A Three-Axis interferometer
- Agilent Z4399A Three-Axis interferometer
- Agilent Z4422B Three-Axis interferometer
- Agilent Z4420B Five-Axis interferometer
- Agilent Z4421B Five-Axis interferometer

For the interferometers listed below, a displacement count equals  $\lambda/(2 \times$  Electronics Resolution Extension Factor).

- Agilent 10702A Linear Interferometer
- Agilent 10766A Linear Interferometer
- Agilent 10705A Single Beam Interferometer

Electronics Resolution Extension factors (ERX in equations below) are as follows:

- 32 for 10885, 10887, 10895, 10896
- 64 for 10889
- 256 for 10897 and 10898
- 512 for N1231A
- 1024 for N1231B

Deadpath counts is the deadpath length, "D", in terms of counts. These counts have to be appropriate for the optics being used.

You must input the terms "Deadpath Counts" and "deadpath in selected units" with the correct conversion factor. These terms can be determined as follows:

For  $\lambda/8$  optics:

Deadpath Counts = 
$$\frac{\text{ERX} \times 1.26384033 \times 10^{4}}{\text{Initial TCN}}$$

For  $\lambda/4$  optics:

Deadpath Counts = 
$$\frac{\text{ERX x 6.31920164 x 10}^3}{\text{Initial TCN}}$$

For  $\lambda/2$  optics:

Deadpath Counts = 
$$\frac{\text{ERX} \times 3.15960082 \times 10^{-3}}{\text{Initial TCN}}$$

where D is the deadpath distance measured in *millimeters*.

The wavelength conversion factor is also dependent on which measurement optics are used.

For  $\lambda/8$  optics:

Wavelength Conversion Factor = 
$$\frac{7.91239193}{\text{ERX}} \times 10^{-5} \frac{\text{millimeters}}{\text{count}}$$

For  $\lambda/4$  optics:

Wavelength Conversion Factor = 
$$\frac{1.58247839}{\text{ERX}} \times 10^{-4} \frac{\text{millimeters}}{\text{count}}$$

For  $\lambda/2$  optics:

Wavelength Conversion Factor = 
$$\frac{3.16495677}{ERX} \times 10^{-4} \frac{\text{millimeters}}{\text{count}}$$

The deadpath distance (D) need not be measured with precision. The error in measuring "D" simply shows up as an uncompensated deadpath ( $\Delta$ D). This value would be much smaller than the error due to D.

The ability to correct for deadpath error in software does not eliminate the necessity of minimizing deadpath for proper location of the interferometer wherever possible. If the deadpath (D) is large compared to the distance traveled (L), then the predominant error is a zero shift due to uncertainty in determining the change in air wavelength and this error cannot be eliminated in software.

### **Minimizing Abbé error**

Abbé offset errors occurs when the measuring point of interest is displaced from the actual measuring scale location and there are angular errors in the positioning system. A very important advantage of laser systems is that the Abbé error evident in almost all positioning systems is very easily reduced.

Abbé offset error will make the indicated position either shorter or longer than the actual position, depending on the angular offset. The amount of measurement error resulting from Abbé offset is:

Offset distance × tangent of offset angle

Figure 54 illustrates Abbé error and demonstrates the requirement for minimizing angular error and placement of the measurement path. In Figure 54(A), the measurement axis is coincident with the leadscrew centerline and is measuring a displacement of the carriage at the leadscrew. This figure illustrates the displacement error E which is generated at the measurement probe tip due to angular motion ( $\theta$ ) of the carriage. Figure 54(B) shows the same carriage motion as Figure 54(A) but with the measurement axis coincident with the probe path. In this case, the measurement system measures the actual displacement and there is no offset error.

NOTE

A helpful rule of thumb for approximating the error attributable to angular motion is that for each arcsecond of angular motion, the error introduced is approximately 0.1 micron per 20 mm of offset (5 microinches per inch of offset).

When considering a specific application, make every effort to direct the measurement path as close as possible to the actual work area where the measurement process takes place. In Figure 69, a machine slide is shown with the interferometer and retroreflector placed to minimize Abbé error. The measurement axis is placed at approximately the same level as the work table and is also measuring down the center of the machine slide.

### MINIMIZE ABBÉ ERROR

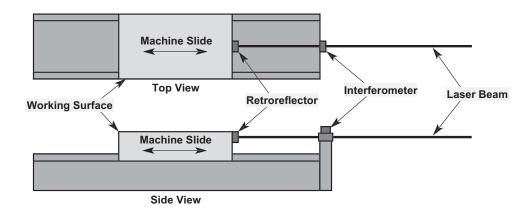


Figure 69 Positioning of measurement axis to minimize Abbé error

For X-Y stage applications, the laser system can minimize Abbé errors. Plane mirror interferometers used with plane mirrors, mounted at 90° to each other on the top edges of an X-Y stage, create a very accurate positioning system which eliminates Abbé error. Figure 70 shows a typical installation for an X-Y stage. The principal advantage of this type of positioning system is that the measurement in both X and Y axes takes place at the work surface plane. If there are angular errors in the cross slides of the stage, any displacement of the work surface due to these errors is measured by the laser.

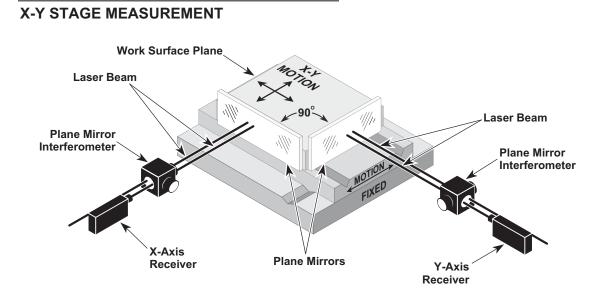
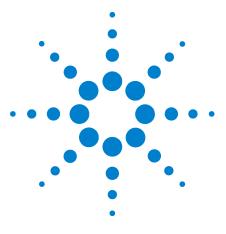


Figure 70 X-Y Stage measurement with Agilent 10706A Plane Mirror Interferometer

# References

- 1 Quenelle, R.C., *Nonlinearity in Interferometer Measurements*, Agilent Technologies Journal, p. 1 0, April 1983.
- 2 Barrell, H. & Sears, J.E., (1939)Phil Trans. Roy. Society, A258, 1-64.
- 3 Edlen, B., The Refractive Index of Air, Metrologia, 1966, 2, 71-80.
- 4 Birch K P, Downs MJ, Metrologia, 1993, 30, 155-162.
- 5 Birch K P, Downs MJ, Metrologia, 1994, 31, 315-316.
- 6 Estler, W Tyler, Applied Optics 24 #6, 1985, 808-815.
- 7 Baldwin, D.R. & Siddall, G.J., A double pass attachment for the linear and plane mirror interferometer, Proc. SPIE, Vol. 480, p.78-83,1984.
- 8 Steinmetz, C.R., Displacement Measurement Repeatability in Tens of Manometers with Laser Interferometry, Proc. SPIE, Vol. 92 1, p.406-420, 1988.



Agilent Laser and Optics User's Manual Volume I

# 13 Wavelength-of-Light Compensation

Introduction, 224

"Absolute" Pressure Versus "Barometric" Pressure, 224 Calculation of Exact Wavelength-of-Light (WOL) Compensation Factor, 225 Wavelength-of-Light (WOL) Compensation Tables, 227



# Introduction

This chapter provides the tables (tables 18 to 67) of Wavelength-of-Light (WOL) compensation values for different environmental conditions, and step-by-step instruction on how to calculate the compensation factor if your system operates in an environment other than those covered by the tables.

# "Absolute" Pressure Versus "Barometric" Pressure

The ambient pressure used in determining your compensation factor must be "absolute" pressure, not the "barometric"" pressure (which is usually absolute pressure that has been "corrected to sea level").

"Barometric pressure", as defined, here, is the absolute pressure that would be measured at a given location, if that location was at sea level and the weather conditions were the same. Suppose, for example, that you were in Denver (Colorado, U.S.A.) at a time when the weather report said the barometric pressure was "762 mm" (30.00 inches) of mercury. Since Denver's altitude is about 1.5 km (5000 feet), the absolute air pressure there and then would be closer to 635 mm (25 inches) of mercury.

To measure pressure, you need an absolute pressure indicator, which is equivalent to a barometer that has not been corrected to sea level. When such a pressure indicator is not readily available, you can make a reasonable approximation to absolute pressure by reducing the barometric pressure obtained from the nearest weather station (at the local airport, for instance) by 2.5 mm (0.1 inch) of mercury of each 30 meters (100 feet) of altitude. That is -

$$P_A = P_B - \frac{\text{Altitude}}{30} \times 2.5$$
  $P_A = P_B - \frac{\text{Altitude}}{100} \times 0.1$   
For Metric Units For English Units

where PA is the absolute pressure, and PB is the barometric pressure.

Note that the altitude of the weather station is not considered here, since the number they report has already been corrected to sea level by the station.

# Calculation of Exact Wavelength-of-Light (WOL) Compensation Factor

If the Laser Position Transducer is being operated in an environment that is not included in the compensation factor tables in this manual, you can calculate the exact compensation factor to an accuracy of 0.1 ppm by using the following formulas.

#### CAUTION

The accuracy of your Laser Position Transducer is a function of your ability to provide it with the correct compensation factor for your measurement conditions. When determining the compensation factor by calculation rather than by using the compensation factor tables, the results you get depends on the resolution of the equipment on which you make your calculation and on your ability to operate it without error. You will be working with numbers that are very small and numbers that are very large; even the smallest error can have a significant effect on the accuracy of your answer, and any error is extremely difficult to detect or trace. We strongly suggest that you make a "practice" run, using values from any of the compensation factor tables, to get a feeling for what is required.

In the formulas below –

- T = Air Temperature
- P = Air Pressure
- H = Relative Humidity
- C = Compensation Factor, to be entered into the controller.

$$C = \frac{10^6}{N + 10^6}$$

where "N" is given in Metric and English systems by -

Metric: T in degrees Celsius, P in millimeters of mercury, H in %

$$N = 0.3836391P \times \left[\frac{1+10^{-6}(0.817-0.0133T)}{1+0.0036610T}\right] - 3.033 \times 10^{-3} \times H \times e^{0.05762T}$$

English: T in degrees Fahrenheit, P in inches of mercury, H in %

$$N = 9.74443P \times \left[\frac{1+10^{-6}P(26.7-0.187T)}{0.934915+0.00203389T}\right] - 1.089 \times 10^{-3} \times H \times e^{0.032015T}$$

#### **EXAMPLE:**

Using the "Standard" conditions, -

Humidity = 50% = "H"

Pressure (absolute) = 760 mm Hg = "P"

Temperature = 20° C = "T"

We will calculate the compensation factor, using the Metric formula for finding "N", and showing all our work.

0.0133T = 0.266000000	(#1)
0.817 - (#1) = 0.551000000	(#2)
$P \ge 10^{-6} \times (#2) = 0.000418760$	(#3)
1 + (#3) = 1.000418760	(#4) (Save)
0.0036610T = 0.073220000	(#5)
1 + (#5) = 1.073220000	(#6)
(#4)(#6) = 0.0932165591	(#7)
$0.3836391 \times P \times (\#7) = 271.7875292$	(#8) (Save)
$e^{0.057627T} = 3.66224916$	(#9)
H x (#9) = 158.3112458	(#10)
$3.033 \ge 10^{-3} \times (\#10) = 0.480158009$	(#11) (Save)
(#8) –(#11) = 271.3963612	(#12)
$(\#12) + 10^6 = 1000271.307$	(#13)
$C = \frac{10^6}{(\#13)} = 0.999728766$	(#14)

For comparison, the answer we were looking for in this example just happens to be "0.9997288".

# Wavelength-of-Light (WOL) Compensation Tables

This chapter contains tables of WOL compensation values for a variety of operating conditions. The tables are divided into two groups; the Metric group (Tables 18 through 42), and the English group (Tables 43 through 67). Each group of tables (Metric or English is organized as follows:

Table 18 and Table 43 are wide-range charts, offering coarse compensation numbers for non precision measurements.

Tables 19 through 42, and Tables 44 through 67 are more detailed charts, progressing from "low" to "high" altitudes, and from "low" to "high" temperature and humidity.

To locate the appropriate table for your application, read the table heading for the percent humidity, pressure, and temperature range. The precise compensation number can be found where the temperature and pressure columns intersect.

The compensation numbers in Tables 18 through 67 represent the last four digits of a seven-digit fraction of the form "0.999abcd". The wavelength-of-light (WOL) compensation number is entered in the form "0.999abcd", where "abcd" is found in the tables.

Table 18 Metric—Wide-Range	
(Temp = 2 to 50° C, Press = 525 to 800 mm, 50% Humidity)	

							Г	EMPE	RATUF	RE IN D	EGRE	ES CEL	.SIUS					
		2.O	5.0	8.0	11.0	14.0	17.0	20.0	23.0	26.0	29.0	32.0	35.0	38.0	41.0	44.0	47.0	50.0
DANOME I RIC PRESSURE IN MILLIMETERS OF MERCURY	80950 77850 777550 777550 7777550 7777777777	695732 99991309487654 7704877700654 77118021098777118021098777777777777777777777777777777777777	6900463109866654 97004631098675531109867654 970046310987771135765322779336685321098675557109865543210 9765476532109867577777777777777777777777777777777777		7070977146319986532291097737402177777777777777777777777777777777777	701224864221977777777777777777777777777777777777	71150865311975311977777777777777777777777777777	711820863119753319753319753319757777777777777777	7192		772268300755297741963185307556636877777777777777777777777777777777	7279 7296 7314 7331 7348 7365 7382 7382 7399	7773345963377777777777777777777777777777777777	77777777777777777777777777777777777777	7364 7381 7397	77777777777777777777777777777777777777	74437777777777777777777777777777777777	744818 744818 7461 75336 755912 777777777777777777777777777777777777

TEMPERATURE IN DEGREES CELSIUS													
5.5 6.0 6.5 7.0 7.5 8.0 8.5 9.0 9.5 10.0 10.5 11	.0 11.5 12.0 12.5	13.0											
5.5         6.0         6.5         7.0         7.5         8.0         8.5         9.0         9.5         10.0         10.5         11           6991         7002         7003	50         7055         7061         7064         7065           54         7059         7064         7065           58         7063         7068         7075           58         7063         7076         7077           65         7070         7075         7086           69         7074         7077         7083         7086           70         7077         7083         7089         7092           70         7092         7097         7102           91         7096         7101         7106           92         7097         7012         7112           93         7087         7092         7097         7122           94         7103         7105         7112         7112           705         7111         7116         7124         7123           705         7113         7123         7122         7127         7132           7114         7112         7113         7133         7138         7143           7133         7133         7138         7143         7143           7140         7145         7160         7165	7071           7075           70782           70869           7087           7080           70104           7104           7104           7107           7104           7107           7115           7122           7123           71337           7141           71529           7163           7170           7174           7177											

#### Table 19 Metric—Low Alt, Low Temp, Low Humidity (Temp = 5 to 13° C, Press = 720 to 800 mm, 20% Humidity)

.

**.** -

-

788         7080
723 7358 7362 7367 7372 7376 7381 7385 7390 7395 7399 7404 7408 7413 7417 7422 7426 7430

Table 20	Metric—Low Alt, Low-Mid Temp, Low Humidity
(Temp	= 13.5 to 21.5° C, Press = 720 to 800 mm, 20% Humidity)

Laser and Optics User's Manual, Vol. I

						٦	EMPE	RATU	RE IN C	EGRE	ES CEI	SIUS					
	22.0	22.5	23.0	23.5	24.0	24.5	25.0	25.5	26.0	26.5	27.0	27.5	28.0	28.5	29.0	29.5	30.0
8090 7998 7997 7995 7995 7995 7995 7995 7887 7897 7887 788	7442	7446	$\begin{array}{c} 77788259926930704771787777777777777777777777777777777$	$\begin{array}{c} 777777777777777777777777777777777777$	7184 7188 7191	$\begin{array}{c} 893660207777220104777777777777777777777777777$	7194 7198 7201 7205	7199           7202           7206           7209           7216           7216           7223           7223           7234           7234           7241           7244           7244           7251	7204 7207 7211 7214 7218 7221 7225 7228 7228 7232	7208 7212 7215 7229 7229 7229 7229 7229 7223 7236 7240 7240 7243 7250 7254	1 7213 7217 7220 7224 7227 7231 7234 7238 7238 7238 7238 7244 7248 7251	7218 7221 7225 7228 7232 7235 7235 7239 7242 7246 7249	<ul> <li>7223</li> <li>7226</li> <li>7233</li> <li>7236</li> <li>7240</li> <li>7243</li> <li>7243</li> <li>7247</li> <li>7250</li> <li>7254</li> <li>7257</li> <li>7261</li> </ul>	7227 7231 7234 7238 7241 7245 7248 7248 7252	$\begin{array}{c} 7232\\7235922449\\722469\\722350\\722449\\7225603704\\7722850\\722469\\722663704\\772280\\722772280\\722772280\\722772280\\73308\\733125\\733226\\73336\\733537\\73366\\73377338\\73395\\739$	$\begin{array}{c} 723370\\ 7722447040\\ 7225547\\ 77226148\\ 7225547\\ 77226614\\ 88922370\\ 7722661\\ 722782959\\ 7229592\\ 7229592\\ 7229592\\ 7230069\\ 733120\\ 73332237\\ 7333414\\ 733561\\ 733561\\ 73377\\ 733561\\ 733999$	$\begin{array}{c} 7238\\ 72441\\ 7245\\ 7245\\ 72559\\ 72759\\ 72559\\ 72759\\ 72559\\ 72759\\ 72759\\ 72759\\ 72759\\ 72759\\ 72759\\ 73104\\ 73117\\ 7324\\ 73355\\ 73255\\ 73592\\ 73559\\ 7359\\ 73559\\ $

#### Table 21 Metric—Low Alt, Mid Temp, Low Humidity (Temp = 22 to 30° C, Press = 720 to 800 mm, 20% Humidity)

TEMPERATURE IN DEGREES CELSIUS																	
	30.5	31.0	31.5	32.0	32.5	33.0	33.5	34.0	34.5	35.0	35.5	36.0	36.5	37.0	37.5	38.0	38.5
87777777777777777777777777777777777777	$\begin{array}{l} 5 & 264936003704704704704708802158225922693333334693360370470147077777777777777777777777777777$	$\begin{array}{c} 0 & 711481571488582259926693693160360337044714777777777777777777777777777777$	$\begin{array}{llllllllllllllllllllllllllllllllllll$	$\begin{array}{llllllllllllllllllllllllllllllllllll$	$\begin{array}{llllllllllllllllllllllllllllllllllll$	$\begin{array}{llllllllllllllllllllllllllllllllllll$	3 777777777777777777777777777777777777	$\begin{array}{c} 3 \\ 7777777777777777777777777777777777$	3 777777777777777777777777777777777777	$\begin{array}{c} 0 & 4771498144815822822582559266926693669366936936003600370237047144547147777777777777777777777777777$	$\begin{array}{llllllllllllllllllllllllllllllllllll$	7293 7296 7300 7303 7307 7310 7313 7313	5 8114815825815825825925926926926936936936036077777777777777777777777777	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 5 & 770313700377\\ 77332270447\\ 773333444704\\ 773333404470\\ 773333404470\\ 773333404470\\ 773333404470\\ 773333404470\\ 77333344470\\ 77333344470\\ 77333344470\\ 777777777777777777777777777777777$	$\begin{array}{c} 0  1148155813881155825582592599259925992592692692692692692692692669366936693600360037027777777777777777777777777777$	$\begin{array}{r} 38.5\\ 7316\\ 7319\\ 7329\\ 7322\\ 7336\\ 7349\\ 7352\\ 7336\\ 7359\\ 7356\\ 7359\\ 7356\\ 7379\\ 7356\\ 7379\\ 7356\\ 7379\\ 7396\\ 7379\\ 7396\\ 7379\\ 7396\\ 7379\\ 7396\\ 7379\\ 7396\\ 73739\\ 7396\\ 7400\\ 7410\\ 7422\\ 7433\\ 7440\\ 7422\\ 7443\\ 7440\\ 7447\\ 7450\\ 7466\\ 7470\\ 7467\\ 7470\\ 7457\\ 7551\\ 7551\\ 7551\\ 7551\\ 7554\\ 7551\\ 7554\\ 7551\\ 7554\\ 7551\\ 7554\\ 7551\\ 7554\\ 7551\\ 7554\\ 7551\\ 7554\\ 7551\\ 7554\\ 7556\\ 7557\\ 7556$
-											,	,	1000	1312	010	1991	1000

Table 22	Metric—Low Alt, High-Mid Temp, Low Humidity
(Temp	= 30.5 to 38.5° C, Press = 720 to 800 mm, 20% Humidity)

Laser and Optics User's Manual, Vol. I

**BAROMETRIC PRESSURE IN MILLIMETERS OF MERCURY** 

	TEMPERATURE IN DEGREES CELSIUS														_		
	5.0	5.5	6.0	6.5	7.0	7.5	8.0	8.5	9.0	9.5	10.0	10.5	11.0	11.5	12.0	12.5	13.0
719 718777777777777777777777777777777777	$\begin{array}{c} 3 & 8155936004815593704825593704825993704826937148125936004821593600482159360048215936004825593707777777777777777777777777777777777$	$\begin{array}{c} 3 & 2290004711593600484159360481759386004715938600471593600471593600471593600477777777777777777777777777777777777$	$\begin{array}{c} & 7777777777777777777$	$\begin{array}{c} 3 & 26003711582260371558260037715882960037715882960037115826037177777777777777777777777777777777777$	$\begin{array}{c} & 77777777777777777777777777777777777$	$\begin{array}{c} 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 $	$\circ  7332223333445259370488159902604471215592377777777777777777777777777777777777$	$\circ 777777777777777777777777777777777777$	> 777777777777777777777777777777777777	$\begin{array}{c} 5 \\ 3333446037777777777777777777777777777777$	1  77777777777777777777777777777777777	7341	1  77777777777777777777777777777777777	$\begin{array}{c} 1 \\ 7777777777777777777777777777777777$	$\begin{array}{c} 1\\ 7&7&7&7&7&7&7&7&7&7&7&7&7&7&7&7&7&7&7&$	$\begin{array}{c} 1 \\ 7777777777777777777777777777777777$	13.0 7364877777777777777777777777777777777777

#### Table 23 Metric—High Alt, Low Temp, Low Humidity (Temp = 5 to 13° C, Press = 640 to 720 mm, 20% Humidity)

															······		
	720 7369 7373 7378 7383 7387 7392 7396 7401 7405 7410 7415 7410 7415 7410																
							16.5	17.0	17.5	18.0	18.5	19.0	19.5	20.0	20.5	21.0	21.5
71987765432109887654321098876543210988765654321098876554321098876543210988765432109887654321098876543210988765654321098876565656565656565656565656565656565656	$\begin{array}{c} 926 \\$	7373 7377	1 777777777777777777777777777777777777	7383 7386 7390 7393 7397 7401 7404 7408	3       7387         5       7394         7398       7398         74009       74136         7423       7423         7423       7427         7434       7434	5 16.0 7392 7395 7395 7403 7406 7410 7410 7410 7417 7421 7421 7424	16.5 7396 7400 7404 7404 7407 7411 7414	17.0 7401	17.5 7405 7409	18.0 7410 7413 7417 7421 7424	18.5 7414 7418 7422 7425 7429 7429 7432 7436 7443 7443 7443	19.0 7419 7422 7426 7430 7437 7437 7440 7444	7423 7427 7430	7428 7431 7435 7439	7432 7436 7439 7443 7447 7450 7454 7454 7454 7454 7461 7464	77777777777777777777777777777777777777	2 777777777777777777777777777777777777

Table 24 Metric—High Alt, Low-Mid Temp, Low Humidity (Temp = 13.5 to 21.5° C, Press = 640 to 720 mm, 20% Humidity)

٠.

	720 7446 7450 7454 7450 7462 7467 7472 7472 7476 7400 7405 7400 7400 7400 7400																
	22.0	22.5	23.0	23.5	24.0	24.5	25.0	25.5	26.0	26.5	27.0	27.5	28.0	28.5	29.0	29.5	30.0
$\begin{array}{c} 7219\\ 7117\\ 7115\\ 7117\\ 7117\\ 7117\\ 7117\\ 7109\\ 86996\\ 699432\\ 66996\\ 66996\\ 66996\\ 66996\\ 66996\\ 66996\\ 66996\\ 66966\\ 666\\ 6666\\ 6$	$\begin{array}{c} 744493777777777777777777$	77777777777777777777777777777777777777	4484665826936003704714825926936934603704815825926936047148815825926603704714888159926936037077777777777777777777777777777777	7459 7462 7466 7469 7473 7476 7480 7483 7483	7463 7467	$\begin{array}{c} 77477815920693600370477777777777777777777777777777777$		7476 7480 7483 7487 7490 7494 7497 7501	7480 7484 7487	2 744895992692693600370471481558255555555555555555555555555555555	$\begin{array}{c} 0 & 9269936003700471488155555566697360039704784895555555555555555555555555555555555$	7493 7497 7500 7504		2 5 5 5 5 5 5 5 5 5 5 5 5 5		2 75512227148158255926693769386007148148158259366936097177777777777777777777777777777777777	$\begin{array}{c} 7514\\ 7521\\ 7522\\ 7522\\ 7522\\ 7522\\ 7532\\ 7532\\ 7532\\ 7540\\ 7540\\ 7556\\ 7559\\ 7556\\ 7559\\ 7556\\ 7559\\ 7556\\ 7559\\ 7556\\ 7559\\ 7556\\ 7559\\ 7556\\ 7559\\ 7556\\ 7559\\ 7560\\ 7573\\ 7560\\ 757\\ 7584\\ 7590\\ 7560\\ 7560\\ 7560\\ 7615\\ 7622\\ 7625\\ 7622\\ 7639\\ 7664\\ 7669\\ 7663\\ 7669\\ 7663\\ 7669\\ 7669\\ 7669\\ 7669\\ 7669\\ 7669\\ 7669\\ 7669\\ 7669\\ 7669\\ 7669\\ 7669\\ 7669\\ 7669\\ 7673\\ 7769\\ 7769\\ 7769\\ 7769\\ 7769\\ 7769\\ 7770\\ 7773\\ 7770\\ 7773\\ 7773\\ 7776\\ 7773\\ 7776\\ 7773\\ 7776\\ 7773\\ 77781\\ 7778\\ 7778\\ 7778\\ 7778\\ 7778\\ 7779\\ 7788\\ 7791\\ 7788\\$

Table 25	Metric—High Alt, Mid Temp, Low Humidity
(Temp	= 22 to 30° C, Press = 640 to 720 mm, 20% Humidity)

TEMPERATURE IN DEGREES CELSIUS           30.5         31.0         31.5         32.0         32.5         34.0         34.5         35.0         36.5         37.0         37.5         38.0         38.5           720         7519         7523         7527         7531         7535         7544         7544         7542         7546																	
	30.5	31.0	31.5	32.0	32.5	33.0	33.5	34.0	34.5	35.0	35.5	36.0	36.5	37.0	37.5	38.0	38.5
691 69898 6887 6886 6887 6886 6887 6886 6887 6886 6887 6886 6887 6886 6887 6887 6886 6887 6887 6887 6886 6887 6887 6677 6676 6668 6666 6665 66558 65554 6555 65554 66558 65554 66558 65554 66558 65554 66558 65554 66558 66554 66556 66556 66556 66556 66556 66556 66556 66556 66556 66556 66556 66556 66556 66556 66556 66556 66556 66556 66556 66566 66566 66566 66566 66566 66566 66566 66566 66566 66566 66566 66566 66566 66566 66566 66566 66566 665666 665666 665666 665666 665666 665666 665666666	759225369357775577777777777777777777777777777	- 777777777777777777777777777777777777	7527 7530	77777777777777777777777777777777777777	7553446926693600370555563600370777777777777777777777	9360370377777777777777777777777777777777	75547 77555471481 75554717815858915825992 7775556714889158859589259259259259259259259259259259259259259	755586158259269269260293692602693 75555865777755889269260293620020 775555566577775588926926029362000 77565577775588926926029362000 77776662260336037777666200 77766688814814 7777777777777777777777777777777	77777777777777777777777777777777777777	3 55566736083704704704711447174777777777777777777777	7560			7572 7576 7579 7583	3 7558890370377776641704 777558850370037776641704 77766401704 77766401704 7766401704 7766401704 77766401705 77766401705 7776660 7776660 77777777777777777777	$\begin{array}{c} 3 \\ 7558999714851248384155581559166675825892592592592592259259266926926936936036033603370777777777777777777777$	38.5 75858 759587 759587 76015 760115 76025 76625 77625 76625 77625 77625 77625 77625 77777 777777777777777777777777777

Table 26	Metric—High Alt, High-Mid Temp, Low Humidity
(Tem)	o = 30.5 to 38.5° C, Press = 640 to 720 mm, 20% Humidity)

	S.0         5.5         6.0         6.5         7.0         7.5         8.0         8.5         9.0         9.5         10.0         10.5         11.0         11.5         12.0         12.5         13.0           800         6887         6887         6887         7004         7004         7020         7025         7031         7036         7041         7042         7057         7057																
	5.0	5.5	6.0	6.5	7.0	7.5	8.0	8.5	9.0	9.5	10.0	10.5	11.0	11.5	12.0	12.5	13.0
800 799 798 7997 7987 7997 7987 7887 788	$\begin{array}{c} \textbf{69995} \\ \textbf{6995} \\ \textbf{69995} \\ \textbf{6995} \\ \textbf{69995} \\ \textbf{6995} \\ \textbf{695} $	$\begin{array}{c} & 9996\\ & 9990048\\ & 9700048\\ & 77001937700382\\ & 77001937700382\\ & 77001937700483\\ & 7700193770049\\ & 7700193770049\\ & 7700193770049\\ & 770077700880\\ & 7700780082\\ & 7700777700887\\ & 77007809982\\ & 770077777777777777777777777777777777$	$\begin{array}{l} 69008\\ 990209337770248\\ 70039970177770248\\ 700366990037710248\\ 700366990037770248\\ 7003669900377700888826\\ 700777008888266090037711118226603717171188260037700888826000377101115822600377111158260037717220282160337712223159246049737722282871592260237712222375222315924604973772228847157114826003771205826003777222231592460497772228287157212223772222315924604977722282460497772228246049777222826049777222237522237522237522237522237522237522237572222375222377222237722223777222884715711282600377120582260582460477722282377722288471571128260377722223777222237522237772228847157212268927772228246047777777772228237772228237772228847157712058226058260927772228847157777777722282377722284260477777777777777777777777777777777777$	$\begin{array}{c} 70001\\ 7001159\\ 22600347\\ 7003347\\ 700556\\ 7000159\\ 203041\\ 700492\\ 7003347\\ 700556\\ 70077\\ 70077\\ 700526\\ 8860947\\ 11110092\\ 61092\\ 11112\\ 10092\\ 11112\\ 10092\\ 11112\\ 10092\\ 11112\\ 10092\\ 11112\\ 10092\\ 11112\\ 10092\\ 10092\\ 11112\\ 10092\\ 10002\\ 10002\\ 10002\\ 10002\\ 10002\\ 10002\\ 10002\\ 10002\\ 10002\\ 10$	$\begin{array}{c} 99360294\\ 700160244\\ 7003939346\\ 700548\\ 700548915\\ 700770026659\\ 700554\\ 700554\\ 700554\\ 700564\\ 7007700288915\\ 70077008888\\ 152920047\\ 711225933600\\ 71114859260047\\ 1159222004\\ 712225260337\\ 7222526037\\ 72222337\\ 72222337\\ 72222337\\ 72222337\\ 72222337\\ 72222337\\ 72222337\\ 72222337\\ 72222337\\ 72222337\\ 72222337\\ 72222337\\ 72222337\\ 72222337\\ 72222337\\ 72222337\\ 72222337\\ 72222337\\ 72222337\\ 722337\\ 723337\\ 723337\\ 7233337\\ 723337\\ 7233337\\ 72333337\\ 723337\\ 72337$	$\begin{array}{c} 1 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\$	$\begin{array}{c} 0 & 0.477\\ 7.002315822(6) & 0.0477\\ 7.005682\\ 7.002315822(6) & 0.0277\\ 7.005682\\ 7.002315822(6) & 0.0277\\ 7.006682\\ 7.0076992\\ 7.00994\\ 7.00984\\ 7.00$	$\begin{array}{c} 70239\\ 70236\\ 7003360\\ 7003360\\ 7003360\\ 700559\\ 700559\\ 700559\\ 700559\\ 700747\\ 700559\\ 700747\\ 700559\\ 700747\\ 70085\\ 700747\\ 70085\\ 700747\\ 70085\\ 700747\\ 70085\\ 700747\\ 70085\\ 700747\\ 70085\\ 700747\\ 70085\\ 700747\\ 70085\\ 700747\\ 70085\\ 700747\\ 70085\\ 700747\\ 70085\\ 700747\\ 70085\\ 700747\\ 70085\\ 700747\\ 70085\\ 700747\\ 70085\\ 700747\\ 70085\\ 70077\\ 70077\\ 70085\\ 70077\\ 700085\\ 70077\\ 70085\\ 70077\\ 70085\\ 70077\\$	3 7077777777777777777777777777777777777	$\begin{array}{c} & & & & & & & & & & & & & & & & & & &$	$\begin{array}{c} 0 \\ 415 \\ 970 \\ 492 \\ 600 \\ 777 \\ 700 \\ 500 \\ 700 \\ 777 \\ 700 \\ 7$	$\begin{array}{c} 7777777777777777777$	$\begin{array}{c} 1\\ 7055637777777777777777777777777777777777$	$\begin{array}{c} 1\\ 77777777777777777777777777777777777$	$\begin{array}{c} 12 \\ -0 \\ -0 \\ -0 \\ -0 \\ -0 \\ -0 \\ -0 \\ -$	$\begin{array}{c} 12.5\\ 70681\\ 70779\\ 70993\\ 70093\\ 71104\\ 711123\\ 6204\\ 711123\\ 71$	$\begin{array}{c} 7073\\ 7070\\ 7084\\ 7091\\ 7084\\ 7091\\ 7099\\ 7102\\ 7102\\ 7102\\ 7102\\ 7102\\ 7102\\ 7102\\ 7112\\ 7122\\ 7223\\ 7223\\ 7223\\ 7223\\ 7224\\ 7225\\ 7226\\ 7227\\ 7227\\ 7227\\ 7227\\ 7226\\ 7227\\ 7226\\ 7227\\ 7227\\ 7226\\ 7227\\ 7226\\ 7226\\ 7227\\ 7226\\ 7227\\ 7226\\ 7226\\ 7226\\ 7227\\ 7226\\ 7226\\ 7227\\ 7226\\ 7227\\ 7226\\ 7226\\ 7227\\ 7226\\ 7226\\ 7227\\ 7226\\ 7227\\ 7226\\ 7226\\ 7226\\ 7227\\ 7226\\ 7226\\ 7226\\ 7226\\ 7226\\ 7227\\ 7226\\ 7226\\ 7226\\ 7226\\ 7226\\ 7227\\ 7226\\ 7227\\ 7226$ 7226

Table 27 Metric—Low Alt, Low Temp, Med Humidity (Temp = 5 to 13° C, Press = 720 to 800 mm, 50% Humidity)

13.5	14.0	14.5	15.0	15.5	16.0	16.5	17.0	17.5	18.0	18.5	19.0	19.5	20.0	20.5	21.0	21.5
13.5 800 7078 799 7082 797 7089 796 7098 796 7098 795 7096 794 7100 792 7107 791 7115 789 7118 788 7122 787 7126 786 7129 785 7133 784 7137 782 7144 781 7148 780 7151 779 7155 777 7162 776 7160 775 7170 774 7173 772 7180 775 7170 774 7173 772 7188 769 7191 766 7202 765 7206 764 7210 761 7221 761 7221 762 726 763 7219 765 7208 765 7208 767 729 766 7202 765 7207 761 7221 761 7221 761 7221 762 726 763 7219 763 7228 755 7243 754 7246 755 7243 754 7276 746 7276 747 727 751 728 753 725 756 7239 754 7248 753 725 756 7239 753 725 756 726 748 726 748 726 748 7276 748 726 748 7276 748 7277 751 7308 737 7308 736 7319 733 732 731 7330 732 7367 732 7367 733 7367 732 7367 732 7367 732 7367 731 7367 732 7367 731 73767 732 7367 732 7367 732 7367 732 7367 732 7367 732 7367 731 7367 732 7367 731 7367 732 7367 731 7367 732 7367 731 7367 731 7367 732 7367 731 7367 732 7367 731 7367 736 7367 737 7367 737 7367 737 7367 737 7367 737 7367 737 7367 737 7367 737 7367 737 7376 737 7367 737 7376 737 7377 737 7377	$\begin{array}{c} 1 \\ 4 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7$	$\begin{array}{c} 1\\ 7,70909937777777777777777777777777777777$	$\begin{array}{c} 0 & 47777777777777777777777777777777777$	$\begin{array}{c} 5 & 90260037777777777777777777777777777777777$	$\begin{array}{c} 0 & 4811522699370777777777777777777777777$	$\begin{array}{l} \text{1} \\ \text{77112047} \\ \text{7711314493} \\ 77112066371485926003704812592269377722557158604717773334448255926603771485920104812592262326937722227769360477773333444825592660377714859201048125922623660277772226277693604777777777777777777777777777777777777$	$\begin{array}{c} 0 & 481777777777777777777$	$\begin{array}{c} 5 & 933704\\ 7 & 7122704\\ 7 & 777777777777777777777777777777777$	$\begin{array}{c} 0 & 4882\\ 7771335260648936004711482592260212\\ 777225286080471133226033704481558266936047\\ 77777777777777777777777777777777777$	$\begin{array}{c} 5 & 93370447\\ 777777777777777777777777777777777$	$\begin{array}{c} 0 \\ 7711445\\ 7711456\\ 7711456\\ 7711456\\ 7711456\\ 7711456\\ 7711456\\ 7711456\\ 7711456\\ 771177\\ 771777\\ 777777\\ 7777777777777$	$\begin{array}{l} \begin{array}{l} & & & \\ & & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & & \\ & & & \\ & & & & \\ & & & & \\ & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & \\ & & & & & & $	$\begin{array}{c} 0 \\ 771755592\\ 7717777777777777777777777777777777777$	$\begin{array}{c} 5 \\ 0 \\ 771750 \\ 771777777777777777777777777777777777$	0 558259269947115825937044714882659269777777777777777777777777777777777	$\begin{array}{c} 21.\\ & 5\\ & 7160\\ & 7167\\ & 7177\\ & 7185\\ & 7195\\ & 72069\\ & 7217\\ & 722069\\ & 72211\\ & 722247\\ & 72241\\ & 722526\\ & 722318\\ & 722526\\ & 72277\\ & 722526\\ & 72277\\ & 722526\\ & 72277\\ & 722526\\ & 72277\\ & 722526\\ & 72277\\ & 722526\\ & 72277\\ & 722526\\ & 72277\\ & 722526\\ & 72277\\ & 722526\\ & 72277\\ & 722526\\ & 72277\\ & 722526\\ & 72277\\ & 72281\\ & 722526\\ & 72277\\ & 72256\\ & 72277\\ & 72256\\ & 72277\\ & 72256\\ & 72277\\ & 72257\\ & 72256\\ & 72277\\ & 72256\\ & 72277\\ & 72256\\ & 72277\\ & 72256\\ & 72777\\ & 722841\\ & 72256\\ & 72777\\ & 72384\\ & 73377\\ & 73366\\ & 73377\\ & 73364\\ & 73355\\ & 73377\\ & 73384\\ & 73355\\ & 73377\\ & 73384\\ & 73377\\ & 73384\\ & 73377\\ & 73384\\ & 73377\\ & 73384\\ & 73377\\ & 73384\\ & 73377\\ & 7336\\ & 74426\\ & 74437\\ & 74444\\ & 7$

Table 28	Metric—Low Alt, Low-Mid Temp, Med Humidity
(Temp	= 13.5 to 21.5° C, Press = 720 to 800 mm, 50% Humidity)

•••

						I	EMPE	RATUF	RE IN D	EGREI	ES CEL	SIUS					
	22.0	22.5	23.0	23.5	24.0	24.5	25.0	25.5	26.0	26.5	27.0	27.5	28.0	28.5	29.0	29.5	30.0
800 7998 7995 7993 7995 7885 887 7777777777777777777777777	7438 7442 7445	$\begin{array}{c} 777777777777777777777777777777777777$	$\begin{array}{c} 777777777777777777777777777777777777$	7183 7187 7190 7194 7197 7201 7204 7208 7211 7208 7211 7208 7212 7225 7229 7225 7229 7232 7232 7232 7232 7232 7232	84813999269364023714448155926693760277777777777777777777777777777777777	7196 7200 7203 7207	7198 7201	$\begin{array}{l} 9936(2) \\ 9936(2) \\ 7772211704777777777777777777777777777777$	$\begin{array}{c} 777777777777777777777777777777777777$	$\begin{array}{c} 926933704471454865775926936003777777777777777777777777777777777$	7217 7221 7224 7228 7231	$\begin{array}{l}9226936037777777777777777777777777777777777$	7227 7231 7234 7237	$\begin{array}{l} 822339260370477144714899158259269360370477144714899158269360370477144714899269360370477144714815826037047714471481582603704771447146582757777777777777777777777777777777777$	7233 7237 7240 7244 7247 7251 7254 7258	$\begin{array}{c} 3822539266693600471\\ 77777777777777777777777777777777777$	$\begin{array}{c} 72436\\ 7255037\\ 72255037\\ 722557\\ 722557\\ 722557\\ 722557\\ 722557\\ 722557\\ 72277\\ 72277\\ 72277\\ 72277\\ 72277\\ 72277\\ 72277\\ 72277\\ 72277\\ 72277\\ 72277\\ 723360\\ 192269\\ 723360\\ 192269\\ 723360\\ 72377\\ 73377\\ 733550\\ 73377\\ 73366\\ 744336\\ 74457\\ 744557\\ 74458\\ 7445999\\ 744556\\ 71464\\ 888825\\ 59926\\ $

Table 29	Metric—Low Alt, Mid Temp, Med Humidity
(Temp	o = 22 to 30° C, Press = 720 to 800 mm, 50% Humidity)

						1	EMPE	RATUR	RE IN D	EGRE	ES CEL	.SIUS					<u></u>
	30.5	31.0	31.5	32.0	32.5	33.0	33.5	34.0	34.5	35.0	35.5	36.0	36.5	37.0	37.5	38.0	38.5
800 799 798 797 795 794 795 791 785 787 786 787 787 787 787 787 787 787 787	$\begin{array}{c} 77725522522522289993693603137047737333714\\ 7722552522522277792286993693603137047333714\\ 7732552522777977777777777777777777777777$	7256 7259 7263	777777777777777777777777777777777777	269926936037047047133815582592693603704704777777777777777778252592693603704704777777777777777777777777777777	7270 7274 7277	$\begin{array}{c} 777777777777777777777777777777777777$	7280 7283 7287 7290 7294 7297 7300 7304 7307	$\begin{array}{l} 81588915822592209330012527777777777777777777777777777777777$	6936036003703777777777777777777777777777	$\begin{array}{l} 9148815811581582582589266926938893600360137023704447147815815815825925926926926926933003603677777777777777777777777777777$	59206926936936936036037037777777777777777777777	7304 7307	5825825925925926693693693603603777777777777777777777777	$\begin{array}{c} 1036603703703703704770471487194891441222813581312227037077777777777777777777777777777$	$\begin{array}{c} 18222231558158255825582558259259226926926926926936693660360037037777777777777777777777$	$\begin{array}{c} 9226936934693\\ 332229336936603660037600377777777777777777777$	7327773314 77337777777777777777777777777777

#### Table 30 Metric—Low Alt, High-Mid Temp, Med Humidity (Temp = 30.5 to 38.5° C, Press = 720 to 800 mm, 50% Humidity)

-

#### Table 31 Metric—High Alt, Low Temp, Med Humidity (Temp = 5 to 13° C, Press = 640 to 720 mm, 50% Humidity)

	13.5	14.0	14.5	15.0	15.5	16.0	16.5	17.0	17.5	18.0	18.5	19.0	19.5	20.0	20.5	21.0	21.5
720	7371	7375	7380	7385	7389	7394	7399	7403	7408	7412	7417	7422	7426	7431	7435	7440	7444
719 718	7374 7378	7379 7383	7384 7387	7388 7392	7393 7397	7398 7401	7402 7406	7407 7410	7411 7415	7416 7420	7421 7424	7425 7429	7430 7433	7434 7438	7439 7442	7443 7447	7448 7451
717 716	7382 7385	7386 7390	7391 7395	7396 7399	7400 7404	7405 7408	7409 7413	7414 7418	7419 7422	7423 7427	7428 7431	7432 7436	7437 7440	7441 7445	7446 7449	7450 7454	7455 7458
715 714	7389 7393	7394 7397	7398 7402	7403 7407	7407 7411	7412 7416	7417 7420	7421 7425	7426 7429	7430 7434	7435 7439	7439 7443	7444 7448	7449 7452	7453	7458	7462
713 712	7396	7401	7406	7410	7415	7419	7424	7429	7433	7438	7442	7447	7451	7456	7457 7460	7461 7465	7466 7469
711	7400 7404	7405 7408	7409 7413	7414 7417	7418 7422	7423 7427	7428 7431	7432 7436	7437 7440	7441 7445	7446 7449	7450 7454	7455 7458	7459 7463	7464 7467	7468 7472	7473 7476
710 709	7407 7411	7412 7416	7416 7420	7421 7425	7426 7429	7430 7434	7435 7438	7439 7443	7444 7447	7448 7452	7453 7457	7457 7461	7462 7466	7466 7470	7471 7474	7475 7479	7480 7483
708 707	7415 7418	7419 7423	7424 7427	7428 7432	7433 7437	7437 7441	7442 7446	7447 7450	7451 7455	7456 7459	7460 7464	7465 7468	7469 7473	7474 7477	7478 7482	7482 7486	7487
706 705	7422 7426	7426 7430	7431 7435	7436 7439	7440 7444	7445 7448	7449 7453	7454 7457	7458 7462	7463 7466	7467 7471	7472 7475	7476 7480	7481 7484	7485 7489	7490 7493	7490 7494
704 703	7429 7433	7434 7437	7438 7442	7443 7447	7447 7451	7452 7456	7457 7460	7461 7465	7466	7470	7474	7479	7483	7488	7492	7497	7498 7501
702	7436	7441	7446	7450	7455	7459	7464	7468	7469 7473	7474 7477	7478 7482	7483 7486	7487 7491	7491 7495	7496 7499	7500 7504	7505 7508
701 700	7440 7444	7445 7448	7449 7453	7454 7457	7458 7462	7463 7466	7467 7471	7472 7475	7476 7480	7481 7484	7485 7489	7490 7493	7494 7498	7499 7502	7503 7507	7507 7511	7512 7515
699 698	7447 7451	7452 7456	7457 7460	7461 7465	7466 7469	7470 7474	7475 7478	7479 7483	7484 7487	7488 7492	7492 7496	7497 7500	7501 7505	7506 7509	7510 7514	7515 7518	7519 7522
697 696	7455 7458	7459 7463	7464 7467	7468 7472	7473 7477	7477 7481	7482 7485	7486 7490	7491 7494	7495 7499	7500 7503	7504 7508	7508 7512	7513 7516	7517 7521	7522	7526 7530 7533
695 694	7462 7466	7467 7470	7471 7475	7476 7479	7480 7484	7485 7488	7489 7493	7494 7497	7498 7502	7502	7507	7511	7516	7520	7524 7528	7525	7533
693	7469	7474	7478	7483	7487	7492	7496	7501	7505	7506 7510 7513	7510 7514 7518	7515 7518	7519 7523	7524 7527	7532	7532 7536	7537 7540
692 691	7473 7477	7478 7481	7482 7486	7487 7490	7491 7495	7495 7499	7500 7504	7504 7508	7509 7512	7517	7518 7521 7525	7522 7526	7526 7530	7531 7534	7535 7539	7539 7543 7547	7544 7547
690 689	7480 7484	7485 7489	7489 7493	7494 7497	7498 7502	7503 7506	7507 7511	7512 7515	7516 7520	7520 7524	7525 7528	7529 7533	7534 7537	7538 7541	7542 7546	7547 7550	7551 7554
688 687	7488 7491	7492 7496	7497 7500	7501 7505	7506 7509	7510 7514	7514 7518	7519 7522	7523 7527	7528	7528 7532 7536 7539	7533 7536 7540	7541 7544	7545 7549	7546 7549 7553	7554 7557	7558 7562
686 685	7495 7499	7499 7503	7504 7508	7508 7512	7513 7516	7517 7521	7522 7525	7526 7530	7530 7534	7531 7535 7538	7539 7543	7544 7547	7548 7551	7552 7556	7557 7560	7561 7564	7565 7569
684 683	7502 7506	7507 7510	7511 7515	7516 7519	7520 7524	7524 7528	7529 7533	7533 7537	7538 7541	7542 7546	7546 7550	7551 7554	7555 7559	7559 7563	7564	7568 7572	7572
682 681	7510 7513	7514 7518	7519 7522	7523 7527	7527 7531	7532 7535	7536	7541	7545	7549	7554	7558	7562	7567	7567 7571	7575	7576 7579
680	7517	7521	7526	7530	7535	7539	7540 7543	7544 7548	7548 7552	7553 7556	7557 7561	7561 7565	7566 7569	7570 7574	7574 7578	7579 7582	7583 7587
679 678	7521 7524	7525 7529	7529 7533	7534 7537	7538 7542	7543 7546	7547 7551	7551 7555	7552 7556 7559	7560 7564	7564 7568	7569 7572	7573 7577	7577 7581	7582 7585	7586 7589	7590 7594
677 676	7528 7532	7532 7536	7537 7540	7541 7545	7546 7549	7550 7553	7554 7558	7559 7562	7563 7567	7567 7571	7572 7575	7576 7579	7580 7584	7584 7588	7589 75 <b>9</b> 2	7593 7596	7597 7601
675 674	7535 7539	7540 7543	7544 7548	7548 7552	7553 7556	7557 7561	7561 7565	7566 7569	7570 7574	7574 7578	7579 7582	7583 7587	7587 7591	7592 7595	7596 7599	7600 7604	7604 7608
673 672	7543 7546	7547 7551	7551 7555	7556 7559	7560 7564	7564 7568	7569 7572	7573 7577	7577 7581	7582 7585	7586 7590	7590 7594	7594 7598	7599 7602	7603 7607	7607 7611	7611
671 670	7550 7554	7554 7558	7559 7562	7563 7567	7567 7571	7572 7575	7576 7580	7580 7584	7585 7588	7589 7592	7593 7597	7597 7601	7602 7605	7606 7609	7610 7614	7614 7618	7615 7619 7622
669 668	7557 7561	7562 7565	7566 7570	7570 7574	7575 7578	7579 7582	7583 7587	7587	7592	7596	7600	7605	7609	7613	7617	7621	7626
667	7564	7569	7573	7578	7582	7586	7590	7591 7595	7592 7595 7599	7600 7603	7604 7607	7608 7612	7612 7616	7617 7620	7621 7624	7625 7629	7629 7633
666 665	7568 7572	7572 7576	7577 7580	7581 7585	7585 7589	7590 7593	7594 7598	7598 7602	7603 7606	7607 7610	7611 7615	7615 7619	7620 <b>762</b> 3	7624 7627	7628 7632	7632 7636	7636 7640
664 663	7575 7579	7580 7583	7584 7588	7588 7592	7593 7596	7597 7601	7601 7605	7606 7609	7610 7613	7614 7618	7618 7622	7622 7626	7627 7630	7631 7634	7635 7639	7639 7643	7643 7647
662 661	7583 7586	7587 7591	7591 7595	7596 7599	7600 7604	7604 7608	7609 7612	7613 7616	7617 7621	7621 7625	7622 7625 7629	7630 7633	7634 7637	7638 7642	7642 7646	7646 7650	7651 7654
660 659 658	7590 7594	7594 7598	7599 7602	7603 7607	7607 7611	7611 7615	7616 7619	7620 7624	7624 7628	7628 7632	7633 7636	7637 7640	7641 7645	7645 7649	7649 7653	7654	7658
658 657	7597 7601	7602 7605	7606 7610	7610 7614	7615 7618	7619 7622	7623	7627	7631	7636	7640	7644	7648	7652	7656	7657 7661	7661 7665
656	7605	7609	7613	7618	7622	7626	7627 7630	7631 7634	7635 7639	7639 7643	7643 7647	7648 7651	7652 7655	7656 7659	7660 7664	7664 7668	7668 7672
655 654	7608 7612	7613 7616	7617 7621	7621 7625	7625 7629	7630 7633	7634 7637	7638 7642	7642 7646	7646 7650	7651 7654	7655 7658	7659 7663	7663 7667	7667 7671	7671 7675	7675 7679
653 652	7616 7619	7620 7624	7624 7628	7628 7632	7633 7636	7637 7641	7641 7645	7645 7649	7649 7653	7654 7657	7658 7661	7662 7666	7666 7670	7670 7674	7674 7678	7678 7682	7683 7686
651 650	7623 7627	7627 7631	7631 7635	7636 7639	7640 7644	7644 7648	7648 7652	7653 7656	7657 7660	7661 7664	7665 7669	7669 7673	7673 7677	7677 7681	7681 7685	7686 7689	7690 7693
649 648	7630 7634	7635 7638	7639 7642	7643 7647	7647 7651	7651 7655	7656 7659	7660 7663	7664 7667	7668 7672	7672 7676	7676 7680	7680 7684	7685 7688	7689 7692	7693 7696	7697 7700
647 646	7638 7641	7642 7645	7646	7650 7654	7654 7658	7659 7662	7663 7666	7667	7671	7675	7679	7683	7688	7692	7696	7700	7704
645	7645	7649	7653	7658	7662	7666	7670	7671 7674	7675 7678	7679 7682	7683	7687 7691	7691 7695	7695 7699	7699 7703	7703 7707	7707 7711
644 643	7649 7652	7653	7657 7661	7661 7665	7665 7669	7670 7673	7674 7677	7678 7681	7682 7686	7686 7690	7690 7694	7694 7698	7698 7702	7702 7706	7706 7710	7711 7714	7715 7718
642 641	7656 7660	7660 7664	7664 7668	7668 7672	7673 7676	7677 7680	7681 7685	7685 7689	7689 7693	7693 7697	7697 7701	7701 7705	7705 7709	7710 7713	7714 7717	7718 7721	7722 7725
640	7663	7667	7672	7676	7680	7684	7688	7692	7696	7700	7705	7709	7713	7717	7721	7725	7729

Table 32	Metric—High Alt, Low-Mid Temp, Med Humidity
(Tem)	p = 13.5 to 21.5° C, Press = 640 to 720 mm, 50% Humidity)

•

22.0         22.5         23.0         23.5         24.0         24.5         25.0         25.0         26.0         27.0         27.0         28.0 <th< th=""></th<>
719         7452         7457         7461         7465         7463         7483         7483         7487         7480         7500
658         7669         7673         7677         7681         7689         7698         7702         7706         7710         7714         7718         7722         7726         7733         7733         7733         7733         7733         7733         7733         7733         7737         774         7716         7701         7701         7701         7701         7711         7721         7725         7729         7733         7733         7733         7737         774         655         7680         7684         7682         7692         7696         7700         7701         7712         7725         7729         7733         7734         7744         7744         654         7681         7692         7696         7700         7711         7712         7724         7728         7732         7733         7743         7747         7755         652         7690         7698         7702         7710         7712         7723         7731         7735         7739         7743         7743         7747         7755         651         7691         7698         7702         7710         7712         7723         7731         7735         7739         7743         7743 </th

Table 33 Metric—High Alt, Mid Temp, Med Humidity (Temp = 22 to 30° C, Press = 640 to 720 mm, 50% Humidity)

						٦	EMPE	RATU	RE IN D	EGRE	ES CEI	SIUS					
	30.5	31.0	31.5	32.0	32.5	33.0	33.5	5 34.0	34.5	35.0	35.5	36.0	36.5	37.0	37.5	38.0	38.5
71777777777777777777777777777777777777		22259256936036037777777777777777777777777777777	2933037777777777777777777777777777777777	5 $5$ $5$ $5$ $5$ $5$ $5$ $5$ $5$ $5$	75555823099360037707777777777777777777777777777	775556693603703704777777777777777777777777777777	5557778560370 7755560370 7755560370 7775555777858998158998 7775555777858998158998 7775555777858998158998 7777777777558998158998 7777777777777777777777777777777777	7554           7554           7551           7561           7561           7578           7578           7578           7585           7582           7592           7598           7582           7598           7598           7605           7612           7612	7558 7562 7565 7569 7572 7575 7579 7586 7589 7589 7593 7593	7563 7566 7570 7573 7576 7580 7583 7587 7583	3         7567           5         7570           3         7577           5         7584           6         75914           75914         75914           75914         7604           7611         7615           7622         7632           7635         7635           7635         7635	7571 7575 7578 7582 7585 7588 7588 7588 7592 7595 7598	7576 75782 7582 7582 7589 7593 7593 7599 7599 7600 7600 7613	7588037707777777777777777777777777777777	$\begin{array}{c} 7588\\ 848\\ 7559948014\\ 848\\ 77559948014\\ 848\\ 77559948014\\ 848\\ 77559948014\\ 848\\ 7766181\\ 816228\\ 84864558225\\ 77666258225\\ 77777777777777777777777777777777777$	755992659269269266936669369367777777777777777777	7593 7593 7600 7603 7603 7613 7620 7620 7622 7620 7622 7620 7620 7620

Table 34	Metric—High Alt, High-Mid Temp, Med Humidity	
(Temp	= 30.5 to 38.5° C, Press = 640 to 720 mm, 50% Humidity)	

						т	EMPE	RATUR	E IN DI	EGREE	ES CEL	SIUS					
	5.0	5.5	6.0	6.5	7.0	7.5	8.0	8.5	9.0	9.5	10.0	10.5	11.0	11.5	- 12.0	12.5	13.0
800 799 798 797 795 794 795 794 788 787 788 787 788 787 788 787 788 787 788 787 788 787 788 787 788 787 788 787 778 778 778 778 778 7777 776 776	$\begin{array}{c} 6988\\ 6996\\ 6996\\ 7000\\ 7001\\ 7015\\ 7019\\ 7026\\ 7034\\ 7037\\ 7045\\ 7056\\ 7070\\ 7064\\ 7068\\ 7071\\ 7064\\ 7068\\ 7071\\ 7066\\ 7070\\ 7068\\ 7071\\ 7068\\ 7071\\ 7068\\ 7071\\ 7068\\ 7071\\ 7068\\ 7071\\ 7128\\ 7225\\ 7226\\ 726\\ 7$	$\begin{array}{c} 69998\\ 9998000599360024\\ 7700224\\ 70024\\ 70$	9937770118226933711448256603717777777777777777777777777777777777	7001260 700247 700247 700247 700551 700565 70057 70077 70057 7007 70057 70057 70057 70057 70057 70057 70057 70057 70057 70057 70057 70057 70057 70057 70057 70057 70057 70057 70077 70057 70077 70077 70077 70077 70077 70077 70077 70077 70077 70077 70077 70077 70077 700777 700777 700777777	70148257770681577706815770081570081577008157700815700815700815700815700820000000000000000000000000000000000	$\begin{array}{c} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 $	$\begin{array}{c} 2 \\ 7 \\ 0 \\ 2 \\ 1 \\ 5 \\ 7 \\ 0 \\ 0 \\ 2 \\ 2 \\ 0 \\ 0 \\ 2 \\ 0 \\ 0 \\ 0$	$\begin{array}{c} 777777777777777777777777777777777777$	$\begin{array}{c} 226034037714\\ 70054832592360443714\\ 7005488925999360004\\ 7111225922607377700844\\ 711122592260737777777777777777777777777777777777$	77777777777777777777777777777777777777	$\begin{array}{c} 0&37\\00450488715815926926927777777777777777777777777777777$	$\begin{array}{c} 1 \\ 7777777777777777777777777777777777$	$\begin{array}{c} 0.5777777777777777777777777777777777777$	$\begin{array}{c} & 9 \\ 9 \\ 9 \\ 9 \\ 0 \\ 0 \\ 6 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0$	$\begin{array}{c} & & & & & & & & & & & & & & & & & & &$	$\begin{array}{c} 1 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\$	13.0 707582 70869 70977082 708693770982 7104 7104 711159260 71104 71115971260 71115971260 71115971260 71115971260 71115971260 71115971260 71115971260 71115971260 71115971260 71115971260 71115971260 71115971260 71115971260 71115971260 71115971260 71115971260 71115971260 71115971260 71115971260 711159771260 711159771260 711159771260 711159771260 711159771260 711159771260 711159771260 711159771260 711159771260 711159771260 711159771260 711159771260 711159771260 711159771260 7111597771260 712077771260 712077771260 712077772254 722597772258 72260 7227772260 773009777320 773009777320 773009777320 7730097773333977333977333977333977333977333977333977333977335777360 77360

Table 35 Metric—Low Alt, Low Temp, High Humidity (Temp = 5 to 13° C, Press = 720 to 800 mm, 80% Humidity)

	TEMPERATURE IN DEGREES CELSIUS           13.5         14.0         14.5         15.0         15.5         16.0         16.5         17.0         17.5         18.0         18.5         19.0         19.5         20.0         20.5         21.0         2																
	13.5	14.0	14.5	15.0	15.5	16.0	16.5	17.0	17.5	18.0	18.5	19.0	19.5	20.0	20.5	21.0	21.5
800 7998 7997 7994 7995 7994 7999 7887 7888 7889 7887 7888 7889 7887 7775 7777 7777	7310 7314 7318 7321 7325 7329 7322 7336 7340 7343 7347	77777777777777777777777777777777777777	$\begin{array}{c} 777777777777777777777777777777777777$	$\begin{array}{c} 709933777777777777777777777777777777777$	77771123604777777777777777777777777777777777777	$\begin{array}{c} 7777777777777777777$	$\begin{array}{c} 7.77777777777777777777777777777777777$	7308 7312 7315 7319 7323 7326 7330 7333 7337	$\begin{array}{c} 777733360377777777777777777777777777777$	77777777777777777777777777777777777777	77777777777777777777777777777777777777	$\begin{array}{c} 77714482\\ 7771455592660737707777777777777777777777777777777$	$\begin{array}{c} 777777777777777777777777777777777777$	$\begin{array}{c} 777777777777777777777777777777777777$	$\begin{array}{c} 7777777777777777777$	$\begin{array}{c} 777777777777777777777777777777777777$	$\begin{array}{c} 71636\\ 71777\\ 7188\\ 7187\\ 7188\\ 7187\\ 7188\\ 7197\\ 7188\\ 7197\\ 7209\\ 72209\\ 72216\\ 72209\\ 72216\\ 72227\\ 722304\\ 72255\\ 72259\\ 72259\\ 72259\\ 72259\\ 72255\\ 72259\\ 72255\\ 72259\\ 72255\\ 72259\\ 72266\\ 7227\\ 72280\\ 72280\\ 72298\\ 72298\\ 7305\\ 73337\\ 73319\\ 7335\\ 73358\\ 7366\\ 7369\\ 73337\\ 73387\\ 73387\\ 73387\\ 73387\\ 73383\\ 73394\\ 7415\\ 73394\\ 74427\\ 74427\\ 74447\\ 74477\\ 74447\\ 74477$

Table 36 Metric—Low Alt, Low-Mid Temp, High Humidity (Temp = 13.5 to 21.5° C, Press = 720 to 800 mm, 80% Humidity)

						1	EMPE	RATUF	RE IN D	EGREE	ES CEL	.sius				_	
	22.0	22.5	23.0	23.5	24.0	24.5	25.0	25.5	26.0	26.5	27.0	27.5	28.0	28.5	29.0	29.5	30.0
800 7998 7977 7955 7992 7898 7887 7885 7884 7885 7884 7885 7884 7885 7885	$\begin{array}{c} 7771782699360037048122582339226937022118122582926936003711188689360037077777777777777777777777777777777$	777777777777777777777777777777777777	7181 7185 7189	777777777777777777777777777777777777	$\begin{array}{c} 7717777777777777777777777777777777777$	777777777777777777777777777777777777	$\begin{array}{c} 777777777777777777777777777777777777$	$\begin{array}{c} 777777777777777777777777777777777777$	$\begin{array}{c} 2212222334377777777777777777777777777777$	$\begin{array}{c} 217047114852559266936037048890477777777777777777777777777777777$	7222	7227 7230 7234 7237	$\begin{array}{c} 22232445926936007778047777777777777777777777777777777$	7237 7240 7243 7247 7250 7254 7257 7261 7264 7268	$\begin{array}{c} 7724482559266693760047718481582259266936004771848158259266693600477777777777777777777777777777777777$	$\begin{array}{c} 722555(04477815828992259777777777777777777777777777777$	77777777777777777777777777777777777777

Table 37 Metric—Low Alt, Mid Temp, High Humidity (Temp = 22 to 30° C, Press = 720 to 800 mm, 80% Humidity)

						Т	EMPE	RATUF	RE IN D	EGREI	ES CEL	.SIUS					
	30.5	31.0	31.5	32.0	32.5	33.0	33.5	34.0	34.5	35.0	35.5	36.0	36.5	37.0	37.5	38.0	38.5
8099779965 7799779957799210 779987788797779921 7788777887777777777777777777777777777	$\begin{array}{c} 7253\\ 7256\\ 72263\\ 7267\\ 72274\\ 72281\\ 72284\\ 72294\\ 73058\\ 23232\\ 73319\\ 2259\\ 73312\\ 733232\\ 733232\\ 733232\\ 73356\\ 73356\\ 7337\\ 73356\\ 7337\\ 73356\\ 7337\\ 73356\\ 7337\\ 7336\\ 7337\\ 7336\\ 7337\\ 7336\\ 7337\\ 7336\\ 7415\\ 74225\\ 74225\\ 7445\\ 745\\ 7$	22677792288892693603360370471447147177777777777777777777777777	7266 7270 7273 7277 7280 7283 7287 7290 7294 7297	7271 7275	7772890336077047717777777777777777777777777777777	$\begin{array}{c} 77289 \\ 77289 \\ 9582 \\ 77777777777777777777777777777777777$	$\begin{array}{c} 83693600377777777777777777777777777777777$	7291 7294 7298 7301 7305	$\begin{array}{c} 9369320060036003300477777777777777777777777777$	$\begin{array}{c} 9714481482584584258259269269269269269936093704441262377777777777777777777777777777777777$	7306 7309 7313 7316 7319	7311 7314 7318 7321 7324	7316 7319 7322 7326 7329		7326 7329 7332 7336 7339 7342 7346 7349	71447147717777777777777777777777777777	77777777777777777777777777777777777777

Table 38	Metric—Low Alt, High-Mid Temp, High Humidity
(Temp	= 30.5 to 38.5° C, Press = 720 to 800 mm, 80% Humidity)

						٦	EMPE	RATUR	RE IN D	EGREI	ES CEL	SIUS	,				
	5.0	5.5	6.0	6.5	7.0	7.5	8.0	8.5	9.0	9.5	10.0	10.5	11.0	11.5	12.0	12.5	13.0
$\begin{array}{c} 72198\\ 771165\\ 771165\\ 77112\\ 77116\\ 7712\\ 7712\\ 7712\\ 7712\\ 77000\\ 7700\\ 7700\\ 770$	$\begin{array}{c} 72994\\ 77291\\ 7730159\\ 7731204\\ 7733204\\ 773204\\ 773204\\ 773204\\ 773206\\ 7752020\\ 7752000\\ 7752000\\ 7752000\\ 7752000\\ 7752000\\ 7752000\\ 7752000\\ 7752000\\ 7752000\\ 77520000\\ 77520000\\ 77520000\\ 77520000\\ 77520000\\ 77520000\\ 77520000\\ 77520000\\ 77520000\\ 77520000\\ 77520000\\ 77520000\\ 77520000\\ 77520000\\ 775200000\\ 775200000\\ 775200000\\ 775200000\\ 775200000\\ 7752000000\\ 7752000000\\ 7752000000\\ 775200000000\\ 775200000000000000\\ 775200000000000000000000000000000000000$	$\begin{array}{c} 777777777777777777777777777777777777$	777777777777777777777777777777777777		$\begin{array}{c} 3314\\ 773322582600377158282600371158260037115826003717777777777777777777777777777777777$	582(2603714826037177777777777777777777777777777777777	$\begin{array}{c} 22373333344937514482693370482593704823333346667714484558165926603717777777777777777777777777777777777$	7328 7332 7336 7339 7343 7343 7347	7333 7337 7340 7344	$\begin{array}{c} 33844593560481559260047115824027114882593777777777777777777777777777777777777$	7343 7346 7350 7354 7358 7361	7348 7351	7352 7356 7360 7363 7367 7371 7375 7378 7378 7382 7382	7357 7361 7365	$\begin{array}{c} 777777777777777777777777777777777777$	777777777777777777777777777777777777	$\begin{array}{c} 73759\\ 73773880\\ 7377394\\ 74058\\ 7379394\\ 744159\\ 744159\\ 74425\\ 74425\\ 74425\\ 74425\\ 74425\\ 74425\\ 74425\\ 74425\\ 74458\\ 74458\\ 74458\\ 74458\\ 74458\\ 74458\\ 74458\\ 74458\\ 7455\\ 75558\\ 7558\\ 7558\\ 7558\\ 7558\\ 7558\\ 7558\\ 7558\\ 7558\\ 7558\\ 7558\\ 7558\\ 777\\ 7558\\ 756$

Table 39 Metric—High Alt, Low Temp, High Humidity (Temp = 5 to 13° C, Press = 640 to 720 mm, 80% Humidity)

**BAROMETRIC PRESSURE IN MILLIMETERS OF MERCURY** 

Table 40	Metric—High Alt, Low-Mid Temp, High Humidity
(Temp	= 13.5 to 21.5° C, Press = 640 to 720 mm, 80% Humidity)

720       7452       7457       7461       7466       7470       7475       7479       7484       7488       7493       7497       7502       7506       7511       7516       7520       7         719       7455       7460       7465       7469       7474       7478       7483       7487       7492       7496       7501       7510       7511       7511       7512       7522       7527       7         718       7463       7477       7482       7486       7491       7495       7500       7501       7513       7518       7522       7527       7         716       7466       7471       7475       7480       7484       7489       7497       7501       7510       7511       7516       7520       7527       7528       7533       7537       7517       7524       7528       7533       7533       7537       7517       7522       7528       7533       7533			TEMPERATUR	E IN DEGREES CELSIUS	
719       7455       7460       7469       7474       7478       7483       7492       7496       7501       7505       7510	22.0 22.5	5 23.0 23.5 24	.0 24.5 25.0 25.5	26.0 26.5 27.0 27.5 28.	0 28.5 29.0 29.5 30.0
684       7544       7558       7558       7558       7558       7558       7558       7558       7558       7558       7558       7559       7560       7600       7601       7607       7607       7579       7588       7588       7589	720 $7452$ $7457$ $719$ $7452$ $7467$ $718$ $7457$ $7466$ $717$ $7463$ $7467$ $713$ $7477$ $7477$ $713$ $7477$ $7487$ $713$ $7477$ $7488$ $712$ $7487$ $7492$ $709$ $7491$ $7492$ $709$ $7495$ $7492$ $707$ $7492$ $7505$ $706$ $7495$ $7505$ $706$ $7505$ $7510$ $707$ $7519$ $7527$ $7519$ $7527$ $7531$ $702$ $7516$ $7522$ $701$ $7519$ $7524$ $7527$ $7534$ $7532$ $697$ $7534$ $7532$ $697$ $7534$ $7556$ $691$ $7555$ $7556$ $694$ $7544$ $7549$ $693$ $7558$ $7566$ $691$ $7557$ $7559$ $690$ $7558$ $7566$ $691$ $7557$ $7595$ $690$ $7574$ $7555$ $693$ $7548$ $7522$ $7557$ $7595$ $6607$ $681$ $7560$ $7574$ $684$ $7583$ $7884$ $683$ $7583$ $7884$ $683$ $7583$ $7884$ $683$ $7583$ $7826$ $677$ $7619$ $7622$ $677$ $7612$ $7610$ $7676$ $7630$ $677$ $7612$ $7612$ $7617$ $7622$	7         7461         7466         74           7         7461         7468         7473         74           7         7462         7473         74           1         7468         7473         74           1         7475         7480         74           1         7475         7480         74           1         7479         7483         74           1         7480         7490         74           5         7489         7494         74           7479         7483         7497         75           6         7500         7505         75           74707         7480         7494         74           7489         7494         74         747           7489         7494         74         7508         7507           6         7501         7515         7507         7512         752           6         7511         7512         752         7533         755           7         7521         7527         755         7550         7557           7         7521         7527         755         7550	7475         7479         7484           7478         7487         7487           7478         7486         7497           7482         7486         7491           7478         7487         7497           7485         7490         7494           7487         7483         7493           7487         7493         7493           7487         7497         7501           7503         7507         7512           7503         7507         7512           7514         7518         7522           7526         7529         7533           7531         7536         7540           7542         7553         7553           7559         7564         7551           7570         7571         7575           7577         7581         7582           7587         7592         7564           7587         7592         7564           7587         7592         7561           7587         7592         7561           7587         7592         7561           7587         7592         7560	7488         7497         7502         7500           7492         7496         7501         7505         7511           7495         7500         7504         7505         7511           7502         7507         7511         7516         752           7506         7511         7518         7523         752           7507         7511         7516         7521         7523         7533           7523         7528         7533         7533         7533         7533           7523         7528         7533         7544         7544         7544           7534         7535         7557         7564         7557         7564           7541         7558         7566         7566         7567         7566           7541         7542         7546         7557         7567         7566           7558         7560         7566         7566         7567         7567           7562         7566         7577         7587         7587         7587           7562         7560         7567         7587         7587         7587           7572         7577 <td< td=""><td>6         7511         7516         7520         7523           7518         7522         7527         7531           7521         7520         7530         7535           7522         7520         7530         7535           7522         7533         7542         7533           7535         7540         7544         7542           7537         7542         7553         7554           7538         7540         7544         7556           7540         7556         7563         7563           7560         7561         7563         7563           7577         7587         7587         7587           7577         7581         7587         7583           9         7563         7566         7567           7571         7578         7583         7597           3         7577         7581         7587           7581         7582         7587         7583           7587         7588         7593         7597           3         7577         7581         7587           7587         7588         7593           75</td></td<>	6         7511         7516         7520         7523           7518         7522         7527         7531           7521         7520         7530         7535           7522         7520         7530         7535           7522         7533         7542         7533           7535         7540         7544         7542           7537         7542         7553         7554           7538         7540         7544         7556           7540         7556         7563         7563           7560         7561         7563         7563           7577         7587         7587         7587           7577         7581         7587         7583           9         7563         7566         7567           7571         7578         7583         7597           3         7577         7581         7587           7581         7582         7587         7583           7587         7588         7593         7597           3         7577         7581         7587           7587         7588         7593           75

Table 41 Metric—High Alt, Mid Temp, High Humidity (Temp = 22 to 30° C, Press = 640 to 720 mm, 80% Humidity)

**BAROMETRIC PRESSURE IN MILLIMETERS OF MERCURY** 

						٦	EMPE	RATUF	RE IN D	EGRE	ES CEL	SIUS					
	30.5	31.0	31.5	32.0	32.5	33.0	33.5	34.0	34.5	35.0	35.5	36.0	36.5	37.0	37.5	38.0	38.5
209876543210987	$\begin{array}{c} 92693603704771488155555566661612226936033603704771488815555755555555555555555555555555$	4704714815815825926992699269360093602223334447148148148148148148148148158259269 5554445555555555555555555555555555555	7541 7545 7552 7552 7555 7555 7556 7556 7556 755	754693 75555603 7755566703 75570 75570 75570 75584 75581 75581 75581 7594	7550 7554 7557	2582592592693603704777777777777777777777777777777777	7556 7559 7563 7566	77777777777777777777777777777777777777	55277777777777777777777777777777777777	77777777777777777777777777777777777777	7574 7577 7581	7579 7582 7585 7589 7592 7595	7583 7586 7590 7593 7597 7600 7603	7588 7591 7594 7598 7601	3 777777777777777777777777777777777777	3 777777777777777777777777777777777777	38.3 766048 7766118 77662158 77662158 777777777777777777777777777777777777

Table 42	Metric—High Alt, High-Mid Temp, High Humidity
(Temp	= 30.5 to 38.5° C, Press = 640 to 720 mm, 80% Humidity)

Table 43	English—Wide Range
(Temp	= 40 to 120° F, Press = 20 to 31 inches, 50% Humidity)

						TE	MPER/	ATURE	IN DEC	REES	FAHR		г				
	40.0	45.0	50.0	55.0	60.0	65.0	70.0	75.0	80.0	85.0	90.0	95.0	100.0	105.0	110.0	115.0	120.0
$\begin{array}{c} 31.00\\ 30.80\\ 30.40\\ 30.40\\ 30.80\\ 30.40\\ 29.80\\ 29.40\\ 29.80\\ 29.40\\ 29.80\\ 28.80\\ 28.80\\ 28.80\\ 27.60\\ 27.60\\ 27.60\\ 27.60\\ 27.60\\ 26.60\\ 25.40\\ 25.40\\ 24.80\\ 23.80\\ 22$	$\begin{array}{c} 700488\\ 700876\\ 7116832\\ 722409\\ 72257987\\ 7222409\\ 72257987\\ 733575\\ 733575\\ 733575\\ 734132\\ 745709\\ 7556024\\ 777586\\ 777716\\ 58054\\ 777916\\ 58732\\ 77989\\ 12027\\ 7985287\\ 77968\\ 80276\\ 808\\ 8065\\ 808\\ 8065\\ 808\\ 8065\\ 808\\ 8065\\ 806$	7078 7097 7116	$\begin{array}{c} 70897\\ 711454\\ 7720387755\\ 7225775214335219\\ 7335219\\ 7335219\\ 7335219\\ 7335219\\ 7335219\\ 74465321\\ 7555776557\\ 75557766353\\ 7777788221\\ 7789165\\ 7891654\\ 799512\\ 799109\\ 8004665\\ 8123\\ 8004665\\ 8123\\ 8004665\\ 8123\\ 8004665\\ 8123\\ 8004665\\ 8123\\ 8004665\\ 8123\\ 8004665\\ 8123\\ 8004665\\ 8123\\ 8004665\\ 8123\\ 8004665\\ 8123\\ 8004665\\ 8123\\ 8004665\\ 8123\\ 8004665\\ 8123\\ 8004665\\ 8123\\ 8004665\\ 8123\\ 8004665\\ 8123\\ 8004665\\ 8123\\ 8004665\\ 8123\\ 81$	$\begin{array}{c} 71135\\ 7117322\\ 722248655\\ 7228042\\ 7332410\\ 733241\\ 74397\\ 752248655\\ 74332410\\ 75583\\ 74337\\ 74343\\ 74790\\ 75583\\ 76202\\ 775823\\ 76202\\ 777751\\ 788265\\ 777755\\ 788265\\ 777755\\ 777755\\ 777755\\ 777755\\ 777755\\ 777755\\ 777755\\ 777755\\ 777755\\ 777755\\ 777755\\ 777755\\ 777755\\ 77775\\ 778826\\ 77775\\ 77957\\ 77957\\ 79575\\ 79575\\ 79575\\ 79575\\ 79575\\ 79575\\ 79575\\ 79575\\ 79575\\ 79575\\ 79575\\ 79557\\ 795575\\ 795575\\ 795575\\ 795575\\ 795575\\ 795557\\ 795557\\ 7955575\\ 7955557\\ 79555557\\ 7955557\\ 79555557\\ 7955555\\ 795555555555$	$\begin{array}{c} 71163\\ 4643\\ 71201\\ 7227\\ 7227\\ 73334\\ 74201\\ 7457\\ 73334\\ 7457\\ 7457\\ 75570\\ 7757\\ 75570\\ 7757\\ 75570\\ 7757\\ 75570\\ 7757\\ 75570\\ 7757$ 7757 77550\\ 7757 77550 77550	$\begin{array}{c} 7174\\ 712229\\ 72247\\ 72229\\ 73357\\ 73357\\ 73357\\ 74302\\ 74302\\ 743357\\ 74302\\ 743357\\ 74464\\ 75219\\ 7757612\\ 7757612\\ 7777953\\ 76654\\ 7777953\\ 78866\\ 80059\\ 779912\\ 79978\\ 800594\\ 279576\\ 7795757\\ 78850\\ 800594\\ 79978\\ 800597\\ 79978\\ 80059\\ 800597\\ 79978\\ 80059\\ 80$	$\begin{array}{c} 72236\\ 7223564\\ 73324642\\ 773324642\\ 777777777777777777777777777777777777$	$\begin{array}{c} 72249\\ 72263\\ 733186\\ 4442\\ 7488\\ 773377\\ 74442\\ 74898\\ 67551\\ 775667\\ 775667\\ 775667\\ 7777\\ 775667\\ 7777\\ 7777\\ 778\\ 8386\\ 8386\\ 8009\\ 8143\\ 8176\\ 8114\\ 8116\\ 8124$ 8124\\ 8124 8124\\ 8124 8124\\ 8124 8124\\ 8124 8124\\ 8124 8124\\ 8124 8124\\ 8124 8124\\ 8124 8124\\ 8124 8124 8124 8124\\ 8124 8124 8124 8124 8124\\ 8124 8124 8124 8124 8124 8124 8124 8124 8124 8124 8124 8	72772997777777777777777777777777777777	$\begin{array}{c} 773375\\ 773353\\ 774458\\ 775464\\ 7752664\\ 7755464\\ 7755464\\ 7755464\\ 7755464\\ 7755464\\ 7755464\\ 777777792\\ 77575663\\ 77777792\\ 78288\\ 891531\\ 88030\\ 88030\\ 88124\\ 425\\ 880356\\ 881223\\ 880356\\ 881277\\ 77777\\ 7800\\ 880356\\ 880356\\ 88127\\ 77777\\ 7800\\ 880356\\ 880356\\ 88127\\ 7800\\ 880356\\ 88127\\ 7777\\ 7777\\ 7800\\ 880356\\ 880356\\ 88127\\ 77777\\ 77777\\ 77777\\ 77777\\ 77777\\ 77777$ 77777	$\begin{array}{c} 733461\\ 733963\\ 733461\\ 73777\\ 744348\\ 6330\\ 75513530\\ 777558052\\ 77777814\\ 775513530\\ 7777777777777814\\ 77777814\\ 800241\\ 8005752\\ 800241\\ 8005752\\ 900241\\ 8005752\\ 800241\\ 8005752\\ 8002553\\ 8005752\\ 8002553\\ 8005752\\ 8002553\\ 8005752\\ 80$	$\begin{array}{c} 73559\\ 7773667\\ 744218\\ 777777777555459\\ 7766286680\\ 777777777555459\\ 7766286680\\ 777777777777777777777777777777777777$	$\begin{array}{c} 7361\\ 7378\\ 7429\\ 7446\\ 7491\\ 7491\\ 7491\\ 7532\\ 7583\\ 7583\\ 7583\\ 7618\\ 76583\\ 76583\\ 76583\\ 76583\\ 76583\\ 76583\\ 76583\\ 76583\\ 76583\\ 77754\\ 77754\\ 77754\\ 77754\\ 77754\\ 77890\\ 77974\\ 7857\\ 7892\\ 8028\\ 8080\\ 81131\\ 81682\\ 8080\\ 81131\\ 81682\\ 8080\\ 81131\\ 81682\\ 8080\\ 81131\\ 81682\\ 8080\\ 81131\\ 81682\\ 81216\\ 8$	$\begin{array}{c} 7367\\ 7421\\ 744355\\ 755229\\ 77555229\\ 77555229\\ 777555229\\ 7777555229\\ 77777777777777777777777777777777777$	$\begin{array}{c} 7413\\ 7426\\ 74463\\ 774546\\ 775541\\ 807\\ 775581\\ 80135\\ 775581\\ 80135\\ 775581\\ 80135\\ 8015\\ 8015\\ 8015\\ 8015\\ 8015\\ 8015\\ 8015\\ 8015\\ 8015\\ 801$	77477777777777777777777777777777777777	7465 7465 7481 7498 7511 7537 7537 7547 7580 7597 7613 7680 7680 77613 7680 7680 77630 7680 77630 7680 77630 7680 77630 77746 77752 77828 77872 77828 77872 77828 77872 77828 77872 77828 77873 77952 77828 77873 77952 77828 77952 77828 77952 77952 77952 77828 80026 80059 80059 80126 80129 80120 80129 80120 80100 80120 8000 800

						TE	MPERA	TURE	IN DEG	REES	FAHRE	NHEIT					
	40.0	41.0	42.0	43.0	44.0	45.0	46.0	47.0	48.0	49.0	50.0	51.0	52.0	53.0	54.0	55.0	56.0
$\begin{array}{c} 31.00\\ 30.95\\ 30.05\\ 30.85\\ 30.60\\ 30.55\\ 30.65\\ 30.65\\ 30.65\\ 30.20\\ 30.25\\ 30.20\\ 30.25\\ 30.25\\ 30.25\\ 30.25\\ 30.25\\ 29.90\\ 29.95\\ 29.29\\ 29.65\\ 29.29\\ 29.29\\ 29.29\\ 29.29\\ 29.25\\ 29.29\\ 29.25\\ 29.29\\ 29.25\\ 29.29\\ 29.25\\ 29.25\\ 29.29\\ 29.25\\ 22.29\\ 22.29\\ 22.29\\ 22.29\\ 22.25\\ 22.29\\ 22.25\\ 22.29\\ 22.25\\ 22$	$\begin{array}{c} 883382772777777777777777777777777777777$	$\begin{array}{c} 770394\\ 770583\\ 7707777777777777777777777777777777777$	$\begin{array}{c} 0.4550\\$	$\begin{array}{c} 6616\\ 770560\\ 770777777777777777777777777777777777$	$\begin{array}{c} 2257\\ 770616\\ 6116\\ 7099594\\ 994094\\ 83827\\ 7111228\\ 8507\\ 71777\\ 711228\\ 850594\\ 99499\\ 911122\\ 850594\\ 911222\\ 850594\\ 912222\\ 850594\\ 912222\\ 850594\\ 912222\\ 850594\\ 912222\\ 850594\\ 912222\\ 85059594\\ 912222\\ 85059594\\ 912222\\ 85059594\\ 9122222\\ 85059594\\ 9122222\\ 85059594\\ 9122222222\\ 85059594\\ 912222222222\\ 85059594\\ 91222222222222222222222222222222222222$	$\begin{array}{c} 7706672\\ 77078661150494393852672616186195005049949388382727777777777777777777777777777777$	$\begin{array}{c} 706638827\\ 7707837\\ 7707837\\ 771122505949444494838266837727\\ 7211225059972661\\ 11121335949449483827\\ 7112250597266161502222333949483837\\ 72112233596161505050503333355672763335567277333868357277777777777777777777777777777777777$	$\begin{array}{c} 70749\\ 770794\\ 70883\\ 770794\\ 7112261\\ 16494\\ 7111261\\ 7111261\\ 7111261\\ 7111261\\ 71112261\\ 7111261\\ 71112222233244\\ 711222233244\\ 711222233244\\ 711222233244\\ 711222233244\\ 711222233244\\ 711222233244\\ 711222233244\\ 711222233244\\ 711222233244\\ 711222233244\\ 711222233244\\ 711222233244\\ 711222233244\\ 711222233244\\ 71222233244\\ 71222233244\\ 71222233244234\\ 712222233244234\\ 712222233244234\\ 712222233244234\\ 71222233244234\\ 71222233244234\\ 71222233244234\\ 71222233244234\\ 71222233244234\\ 71222223344234\\ 71222223344234\\ 71222223344234\\ 71222233244234\\ 71222223344234$ 71222223344234\\ 71222223344234 7122223344234 71222223344234 7122223344 7122223344 71222223344 71222223344 71222223344 71222223344 71222223344 71222223344 7122223344 71222223344 71222223344 71222223344 71222223344 71222223344 71222223344 71222223344 71222223344 71222223344 71222223344 71222223344 71222223344 712222233244 71222223324222223234 7122222232342222222222222222222222222222	770885094994837727777777777777777777777777777777777	77777777777777777777777777777777777777	770991607771122594937267261600504949383727777777777777777777777777777777777	$\begin{array}{c} 937277777777777777777777777777777777777$	77777777777777777777777777777777777777	$\begin{array}{c} 777777777777777777777777777777777777$	$\begin{array}{c} 0.59\\ 7.71122938377115516615029493837227161222233415059493827266160504948383827266166160233837277777777777777777777777777777777$	$\begin{array}{c} 605\\ 777777777777777777777777777777777777$	77777777777777777777777777777777777777

Table 44 English—Low Alt, Low Temp, Low Humidity (Temp = 40 to 56° F, Press = 27 to 31 inches, 20% Humidity)

	- <b>u</b>		TE	MPER/			BEEC	EVHD		•				·
57.0 58.	0 59.0	60.0 61.												
31.00 7127 713		7144 714			64.0 7166	65.0 7171	66.0 7177	67.0 7182	68.0 7188	69.0 7193			72.0	73.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 726\\ 771455716605504938372777722253150494883727777777777777777777777777777777777$	71444       7144         7148       7153         7153       7155         7153       7157         7153       7157         71562       7167         7157       7176         7185       7157         7176       7181         7190       7199         7204       7200         7213       7217         7223       72237         7236       7241         72207       72237         72236       72264         72264       72664         72263       72277         72273       72272         72290       7292         72201       7292         72202       7230         72273       72267         72287       72272         72290       7292         72300       7310         7310       7310         7310       7310         7310       7310         7310       7310         7310       7310         7310       7310         7310       7310         73247       7322      <	4         7159           7164         7169           7169         7169           7169         7169           7173         7173           7173         7187           7173         7187           7173         7187           7173         7196           7173         7196           7173         7196           7210         7210           7210         7210           7212         7210           7224         72243           72242         72247           72251         7265           72265         72709           72283         72297           7302         7311           7316         7329           7329         7331           7329         7329           7329         7329	7165 7170 7174	$\begin{array}{c} 71670507180493829722161\\ 71780493829722126176075077777777777777777777777777777777$	777777777777777777777777777777777777	$\begin{array}{c} 777777777777777777777777777777777777$	$\begin{array}{c} 777777777777777777777777777777777777$	777777777777777777777777777777777777	$\begin{array}{c} 7177777777777777777777777777777777777$	$\begin{array}{c} 777777777777777777777777777777777777$	$\begin{array}{c} 7220837226617288904993332260722332594483772777777777777777777777777777777777$	$\begin{array}{c} 72722361\\ 7222323331\\ 72333261\\ 7233261\\ 723261\\ 723261\\ 723261\\ 723261\\ 723261\\ 723261\\ 723261\\ 723261\\ 723$	$\begin{array}{l} 72194\\ 722337\\ 72237\\ 72246\\ 722337\\ 722550\\ 72264\\ 722550\\ 72264\\ 722550\\ 72264\\ 722550\\ 72264\\ 722550\\ 72264\\ 722550\\ 72264\\ 722550\\ 72264\\ 72264\\ 72265\\ 72264\\ 72266\\ 72272\\ 72266\\ 72266\\ 72272\\ 72267\\ $

Table 45 English—Low Alt, Low-Mid Temp, Low Humidity (Temp = 57 to 73° F, Press = 27 to 31 inches, 20% Humidity)

							TEN	IPERA	TURE I	N DEG	REESI	AHRE	NHEIT		3			
		74.0	75.0	76.0	77.0	78.0	79.0	80.0	81.0	82.0	83.0	84.0	85.0	86.0	87.0	88.0	89.0	90.0
BAROMETRIC PRESSURE IN INCHES OF MERCURY	05050505050505050505050505050505050505	$\begin{array}{c} 0.492338277160559482271160559482772223324277777777777777777$	$\begin{array}{c} 50049333338257166004933372461550449533334615504938277122344455660493827122334455516605333333333333333333$	$\begin{array}{c} 05594483772224483777777777777777777777777777$	$\begin{array}{c} 600\\ 77224558377160599488372256150749377777777777777777777777777777777777$	$\begin{array}{c} 1 \\ 7 \\ 7 \\ 2 \\ 2 \\ 2 \\ 5 \\ 5 \\ 9 \\ 3 \\ 8 \\ 0 \\ 1 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7 \\ 7$	$\begin{array}{c} 6&1&5\\ 7&7&7&7&7&7&7&7&7&7&7&7&7&7&7&7&7&7&7&$	, 160059482716005948271605948271605938271605938271605938271504938271504938271504938271555566715049382777777777777777777777777777777777777	$\begin{array}{c} 771660749388271150149382261150493377777777777777777777777777777777777$	$\begin{array}{c} 226115048837726005594827716059948377777777777777777777777777777777777$	777777777777777777777777777777777777	$\begin{array}{c} 27781504993726115948371600594827177777777777777777777777777777777777$	72289159483777777777777777777777777777777777777	$\begin{array}{c} 2777777777777777777777777777777777777$	$\begin{array}{c} 8226\\ 77777777777777777777777777777777777$	$\begin{array}{c} & 772777777777777777777777777777777777$	$\begin{array}{c} 82261504837160493827615948371604937261594882771552233827155048371605938226159483777777777777777777777777777777777777$	$\begin{array}{c} 7303\\ 7307\\ 7317\\ 7307\\ 7317\\ 7316\\ 7320\\ 7322$ 7322

Table 46 English—Low Alt, Mid Temp, Low Humidity (Temp = 74 to 90° F, Press = 27 to 31 inches, 20% Humidity)

30.95 7312 7317 7322 7327 7332 7337 7342 7347 7352 7357 7362 7367 7372 7377 7382 73 30.90 7317 7322 7327 7332 7337 7342 7347 7351 7356 7361 7366 7371 7376 7381 7386 73 30.85 7321 7326 7331 7336 7341 7346 7351 7356 7361 7366 7371 7375 7380 7385 7390 73 30.80 7325 7330 7335 7340 7345 7350 7355 7350 7365 7370 7375 7380 7385 7389 7394 73 30.75 7330 7335 7340 7345 7350 7355 7359 7364 7369 7374 7379 7384 7389 7394 7399 73 40.70 7334 7339 7344 7349 7354 7359 7364 7369 7374 7378 7388 7388 7393 7398 7402 740 30.65 7338 7343 7348 7353 7358 7363 7367 7372 7377 7382 7387 7392 7397 7402 7407 74 30.65 7343 7348 7353 7358 7363 7367 7372 7377 7382 7387 7392 7397 7402 7406 7411 741 30.65 7347 7352 7357 7362 7367 7372 7377 7382 7386 7391 7396 7401 7406 7411 741	106.0         107.0           7382         7387           7386         7391           391         7396           395         7400           7399         7404           403         7408           404         7417           412         7417
30.95 7312 7317 7322 7327 7332 7377 7342 7347 7352 7357 7362 7367 7372 7377 7382 73 30.90 7317 7322 7327 7332 7337 7342 7347 7351 7356 7361 7366 7371 7376 7381 7386 73 30.85 7321 7326 7331 736 7341 7346 7351 7356 7361 7366 7371 7375 7380 7385 7390 73 30.80 7325 7330 7335 7340 7345 7350 7355 7360 7365 7370 7375 7380 7385 7389 7394 73 30.75 7330 7335 7340 7345 7350 7355 7359 7364 7369 7374 7379 7384 7389 7394 7399 74 30.70 7334 7339 7344 7349 7354 7359 7364 7369 7374 7378 7388 7398 7398 7403 74 30.65 7338 7343 7348 7358 7368 7363 7368 7373 7378 7383 7388 7392 7397 7402 7407 74 30.65 7347 7352 7357 7358 7368 7363 7367 7372 7377 7382 7387 7392 7397 7402 7406 7411 7415 74 30.55 7347 7352 7357 7362 7367 7372 7377 7382 7386 7391 7392 7401 7406 7411 7415 74	7386 7391 7391 7396 7395 7400 7399 7404 7403 7408 7408 7412 7412 7417
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$

#### Table 47 English—Low Alt, High-Mid Temp, Low Humidity (Temp = 91 to 107° F, Press = 27 to 31 inches, 20% Humidity)

						ΤE	MPERA	TURE	IN DEG	REES	FAHR	ЕМНЕП	•				
	40.0	41.0	42.0	43.0	44.0	45.0	46.0	47.0	48.0	49.0	50.0	51.0	52.0	53.0	54.0	55.0	56.0
23.05	777777777777777777777777777777777777	$\begin{array}{c} 1227\\ 744334460560504779498383827227717555615561561567057777777777777777777$	77777777777777777777777777777777777777	7277777777777777777777777777777777777	$\begin{array}{c} 4 3 3 7 2 7 7 7 7 7 7 7 7$	77777777777777777777777777777777777777	7445726716717777777777777777777777777777777	77476777777777777777777777777777777777	77777777777777777777777777777777777777	77447772777777777777777777777777777777	$\begin{array}{c} 8682772271777777777777777777777777777777$	74777777777777777777777777777777777777	7744899716015025949338837277777777777777777777777777777777	77777777777777777777777777777777777777	77449926116153249777777777777777777777777777777777777	77777777777777777777777777777777777777	77777777777777777777777777777777777777

Table 48 English—High Alt, Low Temp, Low Humidity (Temp = 40 to 56° F, Press = 23 to 27 inches, 20% Humidity)

-

										· ·			·····	
57.0 5					ATURE	IN DE	GREES	S FAHR	RENHE	Т				
	3.0 59.0 303 7500		.0 62.						0 68.0	69.0	70.0	71.0	72.0	73.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	07277553350 01277553350 01277553350 012775555556 0127775555556 012777555556 0127777555556 0127777555556 012777777555556 012777777555556 012777777555556 012777777555556 012777777555556 012777777555556 012777777555556 012777777555556 012777777555556 012777777555556 012777777555556 012777777555556 012777777555556 012777777555556 012777777555556 012777777555556 012777777555556 012777777555556 0127777777555556 0127777777555556 0127777777555556 012777777775755556 012777777777777777777777777777777777777	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	45 755, 559 756, 559 756, 559 756, 568 757, 757, 758, 573 757, 777 758, 589 756, 599 756, 599 756, 500 760, 500 7770, 500 7770, 7770, 7780, 7780,	716 537 537 755 755 755 755 755 755	25 5346555948 5346616555948 53466193 775555948 7755778277559005049 7766193 7766297 77777777777777777777777777777777777	777777777777777777777777777777777777777	460500493827160100493837260494515004948372677777777777777777777777777777777777	5555667383726611493837246155049615 7755565778377777777777777777777777777777	15077755677837266192837726656649383726656649383726656649382777777777777777777777777777777777777	50 777555778837261500494837261500493827 7775755599005049483726615266666788272666667777777777777777777777	59445372616005948372616005948372666667777777777777777777777777777777	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	7858 7867 7867 7871 7876 7881 7885 7890 7894 7899 7903 7903 7908 7917 7921 7921	75793 7558827 77558927 77660159483372615 7776624833726615 7776624837 7776664515 7776664515 7776664515 77777777777777777777777777777777777

Table 49 English—High Alt, Low-Mid Temp, Low Humidity (Temp = 57 to 73° F, Press = 23 to 27 inches, 20% Humidity)

Table 50 English—High Alt, Mid Temp, Low Humidity (Temp = 74 to 90° F, Press = 23 to 27 inches, 20% Humidity)

**.** .

						ŤE	MPER/	TURE	IN DEC	REES	FAHRE	NHEIT		·			
	91.0	92.0	93.0	94.0	95.0	96.0	97.0	98.0	99.0	100.0	0 101.0	102.0	103.0	104.0	105.0	106.0	107.0
095005050505050505050505050505050505050	77777777777777777777777777777777777777	77777777777777777777777777777777777777	$\begin{array}{c} 777777777777777777777777777777777777$	$\begin{array}{c} 9382615594827712230482771550648377181604999372605938266155948827115048337160493982961599989990015997777777777777777777777777777777$	$\begin{array}{c} 7882615594827717777777777777777778800\\ 766886155977777777777777777777777777777777777$	77777777777777777777777777777777777777	266195948261259482715948271150482071150482837160491912726060449377777777777777999827260059382600593826	861599482612594827715964827715948827 7777777777777777777777777777777777	9159948261259482615594826159948261594882611594882661594882661594882615948826159488261594882615948826159488261594888888888888888888888888888888888888	76797777777777777777777777777777777777	777082 77772294 77772294 77772294 77777777777	482261259482612593826026015937266024493717777777777777777777777777777777777	826002316125938261155938260004937777777777777777777777777777777777	261259382602559377777777777777777777777777777777777	$\begin{array}{c} 777777777777777777777777777777777777$	$\begin{array}{c} 777777777777777777777777777777777777$	7725 7729 7734 7738 7742 7734 7738 7742 7745 7750 7755 7755 7755 7755 7755 7755

#### Table 51 English—High Alt, High-Mid Temp, Low Humidity (Temp = 91 to 107° F, Press = 23 to 27 inches, 20% Humidity)

31.02       7025       7025       7025       7005       7105       7105       7105						TE	MPERA	TURE	IN DEG	REES	FAHRE	NHEIT					
30.95 7034 7040 7046 7052 7058 7064 7070 7078 7087 7087 7087 7087 7087 7104 7110 7115 7121 7127 7130 7140 7140 7125 7130 7140 7140 7125 7130 7140 7140 7125 7130 7140 7140 7125 7130 7140 7140 7145 7140 7140 7145 7140 7140 7140 7140 7140 7140 7140 7140	40.	0 41.0	42.0	43.0	44.0	45.0	46.0	47.0	48.0	49.0	50.0	51.0	52.0	53.0	54.0	55.0	56.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 31.00 \\ 702 \\ 30.95 \\ 703 \\ 30.80 \\ 704 \\ 30.80 \\ 704 \\ 30.75 \\ 705 \\ 30.75 \\ 705 \\ 30.65 \\ 706 \\ 30.65 \\ 706 \\ 30.65 \\ 707 \\ 30.55 \\ 708 \\ 30.45 \\ 708 \\ 30.35 \\ 709 \\ 30.25 \\ 710 \\ 30.35 \\ 709 \\ 30.25 \\ 710 \\ 30.35 \\ 712 \\ 30.00 \\ 711 \\ 30.00 \\ 711 \\ 30.00 \\ 711 \\ 30.00 \\ 711 \\ 30.00 \\ 712 \\ 29.95 \\ 713 \\ 29.85 \\ 714 \\ 29.75 \\ 714 \\ 29.75 \\ 714 \\ 29.75 \\ 714 \\ 29.60 \\ 716 \\ 29.55 \\ 716 \\ 29.60 \\ 716 \\ 29.55 \\ 716 \\ 29.45 \\ 717 \\ 29.45 \\ 717 \\ 29.45 \\ 717 \\ 29.45 \\ 717 \\ 29.45 \\ 717 \\ 29.45 \\ 717 \\ 29.45 \\ 717 \\ 29.45 \\ 717 \\ 29.45 \\ 716 \\ 29.55 \\ 726 \\ 28.80 \\ 724 \\ 28.55 \\ 726 \\ 28.55 \\ 726 \\ 28.45 \\ 727 \\ 28.35 \\ 726 \\ 28.65 \\ 725 \\ 28.65 \\ 725 \\ 28.65 \\ 725 \\ 28.65 \\ 726 \\ 28.40 \\ 727 \\ 27.75 \\ 736 \\ 27.55 \\ 736 \\ 27.55 \\ 736 \\ 27.55 \\ 736 \\ 27.55 \\ 736 \\ 27.55 \\ 736 \\ 27.55 \\ 736 \\ 27.55 \\ 736 \\ 27.55 \\ 736 \\ 27.55 \\ 736 \\ 27.55 \\ 736 \\ 27.20 \\ 738 \\ 27.20 \\ 7$	9 7035 9 7045 9 7045 8 7064 8 7054 8 7059 8 7069 8 7069 8 7069 8 7069 8 7069 8 7069 8 7069 8 7069 8 7069 7 7083 7 7083 7 7083 7 7083 7 7093 6 7107 7 7083 7 7093 6 7107 7 7083 7 7093 6 7107 7 7083 7 7093 6 7107 7 7121 6 7121 1 7107 6 7122 1 7107 6 7122 1 7164 9 7174 9 7275 9 7289 9 7380 9 7380 9 7389 9 7399 9 7399 9 7399 9 738 9 7399 9 7399 9 738 9 7399 9 738 9 7399 9 739 9 730 9 730 9 739 9 730 9 730 9 739 9 739 9 730 9 730 9 739 9 739 9 739 9 730 9 739 9 739 9 730 9 730 9 739 9 739 9 730 9 730	$\begin{array}{c} 166160050594949383747271122272777777777777777777777777777$	$\begin{array}{c} 777777777777777777777777777777777777$	383727777777777777777777777777777777777	$\begin{array}{c} 9499.7\\ 7777777777777777777777777777777777$	$\begin{array}{c} 5005949948382277731611227134160594994883892022121261602559494838837277777777777777777777777777777777$	$\begin{array}{c} 7708059949948322777111551606050494932324115512222331441551222233241125122222332142152222223323222222222$	77268916005010594938382572716185050494838372777777777777777777777777777777777	$\begin{array}{c} 777777777777777777777777777777777777$	$\begin{array}{c} 9938377277777777777777777777777777777777$	$\begin{array}{c} 94949490108338377777777777777777777777777777777$	$\begin{array}{c} 050(49) 48388247256160050499383722716155949383272889272611605049483826726160594993837271112283445561605777777777777777777777777777777777$	$\begin{array}{c} 061150259493838627777777777777777777777777777777777$	$\begin{array}{c} 71122600501449486162772686160050149483382722616605084948388272616833844504415044249483882726667504499483827266675049483384455638494838445565166665666666666666666666666666666$	7727777777777777777777777777777777777	56.0 7123 7137 71426 7137 71426 7157 71560 71650 7174 71560 7174 71567 7272 7225 72207 7225 72237 72257 72577 72257 72357 72357 72357 72357 72467 7444 74558 74448 745587 74457 74457 74457

Table 52 English—Low Alt, Low Temp, Med Humidity (Temp = 40 to 56° F, Press = 27 to 31 inches, 50% Humidity)

		TEM				NUCT			
· · · · · · · · · · · · · · · · · · ·			PERATURE						
			53.0 64.0	65.0 66			69.0 70.0		72.0 73.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	145       7151       7         150       7155       7         154       7160       7         155       7164       7         163       7174       7         173       7173       7         173       7173       7         182       7187       7         186       7197       7         186       71201       7         200       7200       7201         210       7220       7222         7223       7224       7         223       7224       7         2242       7247       7         2251       7257       7         2260       7261       7         2260       7261       7         2260       7261       7         2260       7261       7         2260       7261       7         2260       7261       7         2274       7289       7         2283       7293       7         3200       7326       7         3300       7330       73         3310       7344       73 </th <th>156       7162       7         161       7166       7         165       7176       7         170       7185       7         170       7185       7         170       7185       7         171       7       7         170       7185       7         170       7189       7         188       7199       7         198       7203       7         111       7212       7         120       72212       7         121       72217       7         123       72235       7         7230       72235       7         7230       72237       7         7257       7267       7267         7267       7281       7         7380       7295       7         7300       7304       7         7313       7318       7         740       73237       7         7267       7364       7         7313       7318       7         7440       73559       7         727       7364       7</th> <th>1163         7168           7167         7173           1167         7173           1172         7173           1172         7173           1172         7173           1180         7191           1190         7190           1195         7200           209         7214           213         7219           2204         7210           2212         7228           2222         7228           2224         7244           2254         7264           2268         7274           2277         7282           2291         7296           2291         7296           2291         7296           2300         7310           3013         7330           3114         7319           322         7338           332         73310           3332         73310           3305         7310           3305         7310           3314         7319           3322         7338           3327         7420           330</th> <th>7174         71           7179         71           7179         71           7188         71           7192         71           7192         72           7201         72           7205         72           7205         72           7206         72           7207         72           7208         72           7233         72           7242         72           7256         72           7257         7242           7257         7242           7257         7242           7257         7242           727         7244           727         7247           7265         72           7270         72           7288         72           7300         733           7320         733           7320         733           7320         733           7320         733           7320         733           7320         733           7320         733           7320         733</th> <th><math display="block">\begin{array}{c} 844 \\ 7,1904 \\ 893 \\ 7,1999 \\ 893 \\ 7,2038 \\ 7,2038 \\ 7,2038 \\ 7,2038 \\ 7,2038 \\ 7,2235 \\ 7,2244 \\ 9,328 \\ 7,2258 \\ 7,229 \\ 7,2258 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,228 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,235 \\ 7,238 \\ 7,235 \\ 7,238 \\ 7,24 \\ 7,449 \\ 7,449 \\ 7,449 \\ 7,453 \\ 7,538</math></th> <th>719504 772049 772218 777777777777777777777777777777777777</th> <th><math display="block">\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr</math></th> <th><math display="block">\begin{array}{c} 22161\\ 7722250\\ 77722349\\ 8257\\ 77722250\\ 77722250\\ 77722250\\ 77722250\\ 77722257\\ 7777777777</math></th> <th>7212       7218         7217       7222         7222       7227         7226       7231         7235       7240         7240       7245         7235       7240         7240       7245         72247       7253         7253       7258         72526       7227         7271       7276         7280       7285         7280       7285         7280       7285         7280       7285         7280       7285         7280       7285         7280       7285         7280       7285         7280       7285         7280       7285         7280       7285         7280       7394         7312       7312         7321       7320         7333       7375         7331       7312         7321       7320         7333       7344         7343       7384         7357       7362         3300       7375         3311       7380         3329</th>	156       7162       7         161       7166       7         165       7176       7         170       7185       7         170       7185       7         170       7185       7         171       7       7         170       7185       7         170       7189       7         188       7199       7         198       7203       7         111       7212       7         120       72212       7         121       72217       7         123       72235       7         7230       72235       7         7230       72237       7         7257       7267       7267         7267       7281       7         7380       7295       7         7300       7304       7         7313       7318       7         740       73237       7         7267       7364       7         7313       7318       7         7440       73559       7         727       7364       7	1163         7168           7167         7173           1167         7173           1172         7173           1172         7173           1172         7173           1180         7191           1190         7190           1195         7200           209         7214           213         7219           2204         7210           2212         7228           2222         7228           2224         7244           2254         7264           2268         7274           2277         7282           2291         7296           2291         7296           2291         7296           2300         7310           3013         7330           3114         7319           322         7338           332         73310           3332         73310           3305         7310           3305         7310           3314         7319           3322         7338           3327         7420           330	7174         71           7179         71           7179         71           7188         71           7192         71           7192         72           7201         72           7205         72           7205         72           7206         72           7207         72           7208         72           7233         72           7242         72           7256         72           7257         7242           7257         7242           7257         7242           7257         7242           727         7244           727         7247           7265         72           7270         72           7288         72           7300         733           7320         733           7320         733           7320         733           7320         733           7320         733           7320         733           7320         733           7320         733	$\begin{array}{c} 844 \\ 7,1904 \\ 893 \\ 7,1999 \\ 893 \\ 7,2038 \\ 7,2038 \\ 7,2038 \\ 7,2038 \\ 7,2038 \\ 7,2235 \\ 7,2244 \\ 9,328 \\ 7,2258 \\ 7,229 \\ 7,2258 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,228 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,229 \\ 7,235 \\ 7,238 \\ 7,235 \\ 7,238 \\ 7,24 \\ 7,449 \\ 7,449 \\ 7,449 \\ 7,453 \\ 7,538$	719504 772049 772218 777777777777777777777777777777777777	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$\begin{array}{c} 22161\\ 7722250\\ 77722349\\ 8257\\ 77722250\\ 77722250\\ 77722250\\ 77722250\\ 77722257\\ 7777777777$	7212       7218         7217       7222         7222       7227         7226       7231         7235       7240         7240       7245         7235       7240         7240       7245         72247       7253         7253       7258         72526       7227         7271       7276         7280       7285         7280       7285         7280       7285         7280       7285         7280       7285         7280       7285         7280       7285         7280       7285         7280       7285         7280       7285         7280       7285         7280       7394         7312       7312         7321       7320         7333       7375         7331       7312         7321       7320         7333       7344         7343       7384         7357       7362         3300       7375         3311       7380         3329

#### Table 53 English—Low Alt, Low-Mid Temp, Med Humidity (Temp = 57 to 73° F, Press = 27 to 31 inches, 50% Humidity)

					TE	MPER/	TURE	IN DEG	REES	FAHRE	INHEIT	•				
74.0	75.0	76.0	77.0	78.0	79.0	80.0	81.0	82.0	83.0	84.0	85.0	86.0	87.0	88.0	89.0	90.0
$\begin{array}{c} 27.65 \\ 7524 \\ 27.60 \\ 7529 \\ 27.55 \\ 7533 \\ 27.55 \\ 7538 \\ 27.45 \\ 7542 \\ 27.40 \\ 7547 \\ 27.30 \\ 7551 \\ 27.30 \\ 7556 \\ 27.25 \\ 7560 \\ 27.20 \\ 7564 \\ 27.15 \\ 7563 \\ 27.10 \\ 7573 \\ 27.10 \\ 7578 \end{array}$	77777777777777777777777777777777777777	777777777777777777777777777777777777	$\begin{array}{c} 777226615726615722898277777777777777777777777777777777$	77777777777777777777777777777777777777	77777777777777777777777777777777777777	777777777777777777777777777777777777	$\begin{array}{c} 7727777777777777777777777777777777777$	777777777777777777777777777777777777	77261559488271160593824711605938247177777777777777777777777777777777777	771600593827150493777777777777777777777777777777777777	777777777777777777777777777777777777	$\begin{array}{c} 8296105044837160593826715084993772777777777777777777777777777777777$	$\begin{array}{c} 2777777777777777777777777777777777777$	777777777777777777777777777777777777	$\begin{array}{c} 30826\\ 3082\\ 777777777777777777777777777777777777$	77577777777777777777777777777777777777

Table 54 English—Low Alt, Mid Temp, Med Humidity (Temp = 74 to 90° F, Press = 27 to 31 inches, 50% Humidity)

		TEMPER	ATURE IN	DEGREES	FAHREN	HEIT					
91.0 92.0 93.0	94.0 95.0	96.0 97.0	98.0	99.0 100.	0 101.0	102.0 1	103.0	104.0	105.0	106.0	107.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	7654 7659 7658 7663 7663 7667 7667 7672 7671 7676	7340         7345           7344         7350           7353         7358           7357         7362           7367         7366           7370         7357           7370         7357           7370         7357           7370         7357           7371         7380           7379         7384           7383         7393           7392         7397           7360         7401           7400         7414           7413         7418           7422         7427           7435         7440           7433         7448           7443         7448           7443         7448           7456         7461           7456         7461           7457         7456           7458         7437           7459         7504           7504         7509           7521         7526           7522         7530           7533         7538           7543         7543           7543         7543           7544 <th>73553 77733682 777733893 77733893 77733893 777777777777777777777777777777777777</th> <th><math display="block">\begin{array}{rrrr} 7356 &amp; 7361 \\ 7364 &amp; 7376 \\ 7364 &amp; 7377 \\ 7364 &amp; 7378 \\ 7377 &amp; 7378 \\ 7377 &amp; 7386 \\ 7377 &amp; 7390 \\ 7390 &amp; 7408 \\ 7407 &amp; 7411 \\ 7416 &amp; 7425 \\ 7424 &amp; 7434 \\ 7425 &amp; 7434 \\ 7446 &amp; 7425 \\ 7446 &amp; 7445 \\ 7446 &amp; 7445 \\ 7446 &amp; 7455 \\ 7455 &amp; 7468 \\ 7455 &amp; 7455 \\ 7574 &amp; 7455 \\ 7556 &amp; 7555 \\ 75574 &amp; 75528 \\ 75574 &amp; 7558 \\ 75578 &amp; 7558 \\ 7578 &amp; 7579 \\ 3588 &amp; 7647 \\ 7626 \\ 7665 \\ 7667 &amp; 7655 \\ 7667 &amp; 7655 \\ 7667 &amp; 7655 \\ 7667 &amp; 7657 \\ 7578 &amp; 7578 \\ 7588 &amp; 7647 \\ 7656 \\ 7667 &amp; 7657 \\ 7688 \\ 7669 \\ 769 \\ 703 \\</math></th> <th>77777777777777777777777777777777777777</th> <th>737581 777777777777777777777777777777777777</th> <th>73859 77733982 777777777777777777777777777777777777</th> <th>747474747474747474747474747477777777777</th> <th>749015 777777777777777777777777777777777777</th> <th>7557 7567 7567 75655 75574 75578 75578 75578 7559 75599 75777 75599 75777 75777 75777 75777 75777 75777 75777 75777 75777 75777 77714 77724</th> <th>73971 7400 7414 7412 7412 74227 7435 74427 74435 74456 74452 74456 74452 74555 74552 74555</th>	73553 77733682 777733893 77733893 77733893 777777777777777777777777777777777777	$\begin{array}{rrrr} 7356 & 7361 \\ 7364 & 7376 \\ 7364 & 7377 \\ 7364 & 7378 \\ 7377 & 7378 \\ 7377 & 7386 \\ 7377 & 7390 \\ 7390 & 7408 \\ 7407 & 7411 \\ 7416 & 7425 \\ 7424 & 7434 \\ 7425 & 7434 \\ 7446 & 7425 \\ 7446 & 7445 \\ 7446 & 7445 \\ 7446 & 7455 \\ 7455 & 7468 \\ 7455 & 7468 \\ 7455 & 7468 \\ 7455 & 7468 \\ 7455 & 7468 \\ 7455 & 7468 \\ 7455 & 7468 \\ 7455 & 7468 \\ 7455 & 7455 \\ 7574 & 7455 \\ 7556 & 7555 \\ 75574 & 75528 \\ 75574 & 7558 \\ 75578 & 7558 \\ 7578 & 7558 \\ 7578 & 7558 \\ 7578 & 7558 \\ 7578 & 7558 \\ 7578 & 7558 \\ 7578 & 7558 \\ 7578 & 7558 \\ 7578 & 7558 \\ 7578 & 7558 \\ 7578 & 7558 \\ 7578 & 7558 \\ 7578 & 7558 \\ 7578 & 7579 \\ 3588 & 7647 \\ 7626 \\ 7665 \\ 7667 & 7655 \\ 7667 & 7655 \\ 7667 & 7655 \\ 7667 & 7657 \\ 7578 & 7578 \\ 7588 & 7647 \\ 7656 \\ 7667 & 7657 \\ 7688 \\ 7669 \\ 769 \\ 703 \\$	77777777777777777777777777777777777777	737581 777777777777777777777777777777777777	73859 77733982 777777777777777777777777777777777777	747474747474747474747474747477777777777	749015 777777777777777777777777777777777777	7557 7567 7567 75655 75574 75578 75578 75578 7559 75599 75777 75599 75777 75777 75777 75777 75777 75777 75777 75777 75777 75777 77714 77724	73971 7400 7414 7412 7412 74227 7435 74427 74435 74456 74452 74456 74452 74555 74552 74555

Table 55 English—Low Alt, High-Mid Temp, Med Humidity (Temp = 91 to 107° F, Press = 27 to 31 inches, 50% Humidity)

					TE	MPER/	TURE	IN DEG	REES	FAHRE	INHEIT					
40.0	41.0	42.0	43.0	44.0	45.0	46.0	47.0	48.0	49.0	50.0	51.0	52.0	53.0	54.0	55.0	56.0
$\begin{array}{c} 26.65 & 7446\\ 26.65 & 7451\\ 26.55 & 7456\\ 26.55 & 7456\\ 26.45 & 7466\\ 26.45 & 7466\\ 26.45 & 7485\\ 26.25 & 7485\\ 26.25 & 7485\\ 26.25 & 7485\\ 26.25 & 7494\\ 26.10 & 7499\\ 26.05 & 7504\\ 26.00 & 7509\\ 25.95 & 7514\\ 25.85 & 7523\\ 25.80 & 7528\\ 25.85 & 7523\\ 25.80 & 7528\\ 25.65 & 7542\\ 25.65 & 7542\\ 25.65 & 7542\\ 25.55 & 7557\\ 25.55 & 7557\\ 25.55 & 7557\\ 25.55 & 7557\\ 25.45 & 7562\\ 25.35 & 7576\\ 25.25 & 7581\\ 25.30 & 7576\\ 25.25 & 7581\\ 25.30 & 7576\\ 25.25 & 7581\\ 25.30 & 7576\\ 25.25 & 7581\\ 25.30 & 7576\\ 25.25 & 7581\\ 25.30 & 7576\\ 25.25 & 7581\\ 25.30 & 7576\\ 25.25 & 7581\\ 25.30 & 7576\\ 25.25 & 7581\\ 25.45 & 7662\\ 25.10 & 7595\\ 25.00 & 7600\\ 24.95 & 7610\\ 24.95 & 76610\\ 24.95 & 76638\\ 24.60 & 7643\\ 24.60 & 7643\\ 24.60 & 7643\\ 24.60 & 7643\\ 24.60 & 7663\\ 24.45 & 7667 & 7\\ 24.20 & 7686 & 7\\ 24.40 & 7676 & 7\\ 24.20 & 7686 & 7\\ 24.30 & 7677 & 7\\ 24.20 & 7686 & 7\\ 24.30 & 7677 & 7\\ 23.95 & 7715 & 7\\ 23.80 & 7720 & 7\\ 23.80 & 7720 & 7\\ 23.30 & 7768 & 7\\ 23.30 & 7768 & 7\\ 23.30 & 7768 & 7\\ 23.15 & 7787 & 7\\ 23.15 & 7787 & 7\\ 23.15 & 7787 & 7\\ 23.15 & 7787 & 7\\ 23.15 & 7787 & 7\\ 23.15 & 7787 & 7\\ 23.15 & 7787 & 7\\ 23.15 & 7787 & 7\\ 23.15 & 7787 & 7\\ 23.15 & 7787 & 7\\ 23.15 & 7787 & 7\\ 23.05 & 7792 & 7\\ 23.$	742433727777777777777777777777777777777	7634 7643 7643 76643 76572 76657 76657 76657 76657 76667 76686 76686 7700 7710 7710 7710 7724 7734 7733 7748 7758 7763 7763 7763 7763 7777 7786 7777 7786 7777 7781 7796	77777777777777777777777777777777777777	77777777777777777777777777777777777777	77777777777777777777777777777777777777	77777777777777777777777777777777777777	77777777777777777777777777777777777777	7446673882727777777777777777777777777777777	77777777777777777777777777777777777777	77777777777777777777777777777777777777	7447849383727777777777777777777777777777777777	77777777777777777777777777777777777777	77777777777777777777777777777777777777	77777777777777777777777777777777777777	$\begin{array}{c} 905994938272261460550494838272611605049388272777777777777777777777777777777777$	77777777777777777777777777777777777777

Table 56 English—High Alt, Low Temp, Med Humidity (Temp = 40 to 56° F, Press = 23 to 27 inches, 50% Humidity)

TEMPERATURE IN DEGREES FAHRENHEI	IT
57.0 58.0 59.0 60.0 61.0 62.0 63.0 64.0 65.0 66.0 67.0 68.	.0 69.0 70.0 71.0 72.0 73.0
27.00       7805       7514       7517       7525       7524       7534       7534       7544       7544       7547       7556       7556       7556       7556       7556       7557       7557       7556       7557       7556       7557       7557       7556       7557	A         7559         7563         7568         7573         7578           33         7568         7572         7577         7582         7587           33         7568         7572         7577         7582         7587           35         7568         7572         7577         7582         7587           37         7572         7577         7582         7586         7591           7581         7586         7591         7595         7600         7604           7604         7609         7613         7618         7622         7627         7632           3         7617         7622         7627         7631         7636         7640         7645           7622         7627         7631         7636         7663         7663         7668           7640         7645         7649         7654         7658         7663         7668         7672         7677           7663         7667         7672         7677         7681         7688         7663         7668         7672           7674         7664         7654         7657         76890         7699         704         70
23.10 7862 7866 7870 7874 7879 7883 7887 7891 7895 7900 7904 7908 23.05 7866 7870 7875 7879 7883 7887 7892 7896 7900 7904 7908 7912 23.00 7871 7875 7879 7884 7888 7892 7896 7900 7904 7909 7913 7917	7912 7916 7920 7924 7928 7916 7921 7925 7929 7933 7921 7925 7929 7933 7937

Table 57 English—High Alt, Low-Mid Temp, Med Humidity (Temp = 57 to 73° F, Press = 23 to 27 inches, 50% Humidity)

74.0         75.0         76.0 <th< th=""><th></th><th colspan="14">TEMPERATURE IN DEGREES FAHRENHEIT</th></th<>		TEMPERATURE IN DEGREES FAHRENHEIT													
26.85         7537         7628 <t< th=""><th colspan="14"></th></t<>															
23.05 7937 7941 7945 7949 7953 7957 7961 7965 7969 7973 7977 7981 7985 7989 7993 7997 8001	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	7597         7601           7601         7606           7601         7606           7610         7615           7610         7624           7623         7633           7637         7641           7659         7659           7655         7659           7664         7686           76637         7686           76637         7686           76638         7673           7659         76690           76959         7699           7668         7699           7699         7704           7708         7731           7717         7757           7730         7731           7731         7757           7750         7780           7744         7748           7755         7780           7780         7784           7784         7783           7780         7784           7780         7806           7811         7815           7820         7824           7820         7824           7821         7820           78	7606         7611         76           7610         7620         76           7610         7620         76           7619         7624         762           7628         7633         76           7637         7642         7646           7637         7642         76           7637         7642         76           7637         7642         76           7655         7660         76           7655         7660         76           7658         7667         76           7668         76         76           7669         77         76           7668         7699         77           7695         7669         77           7704         7708         77           7717         7722         772           7739         7744         77           7753         7762         77           7778         7778         77           7779         778         77           7779         778         77           7779         778         77           7777         7780	615         7620         7625           620         7625         7625           621         7633         7638           622         7633         7638           623         7638         7642           633         7638         7642           633         7638         7642           633         7638         7642           651         7655         7660           7655         7660         7673           7678         7678         7678           650         7673         7678           777         7622         7866           7695         7700         7704           7000         7704         7709           7001         7713         7712           7722         7726         7727           7613         7717         7722           7731         7733         7757           762         7766         7760           7753         7757         7762           7753         7757         7762           7757         7762         7777           7757         77762         77779	7629         7634           7638         7643           7638         7643           7647         7652           7651         7656           7665         7665           7665         7666           7667         7669           7667         7669           7667         7691           7687         7691           7695         7700           7700         7704           7703         7713           7713         7713           7713         7713           7713         7713           7731         7735           7766         7767           7766         7770           77735         7770           7775         7756           7775         7757           7757         7762           7775         7775           7775         7779           7779         7784           7788         7792           7792         7784           7786         7814           788         7922           7792         7784           788 <th>7639         7643         7648           7643         7648         7652           7657         7656         7661           7656         7665         7670           7665         7665         7670           7665         76670         7674           7668         7687         7692           7674         7678         7683           7687         7692         7666           7691         7692         7696           7692         7696         7700           7705         7709         7714           7705         7709         7714           7705         7709         7714           7718         7722         7727           7718         7722         7727           7731         7735         7757           7740         7744         7749           7744         7748         7752           7757         7762         7766           7770         7784         7784           7784         7782         7827           7797         7801         7805           7801         7805         7810</th> <th>7653         7657           7657         7662           7651         7666           7661         7666           7663         7674           7683         7683           7683         7688           7686         7696           7696         7709           7705         7709           7714         7718           7722         7727           7731         7736           7736         7744           7744         7749           7735         7757           7757         7757           7757         7757           7757         7757           7757         7757           7757         7757           7757         7757           7757         7757           7757         7757           7757         7757           7757         7757           7757         7757           7757         7757           7757         7757           7757         7757           7757         7757           7757         7757           7757</th>	7639         7643         7648           7643         7648         7652           7657         7656         7661           7656         7665         7670           7665         7665         7670           7665         76670         7674           7668         7687         7692           7674         7678         7683           7687         7692         7666           7691         7692         7696           7692         7696         7700           7705         7709         7714           7705         7709         7714           7705         7709         7714           7718         7722         7727           7718         7722         7727           7731         7735         7757           7740         7744         7749           7744         7748         7752           7757         7762         7766           7770         7784         7784           7784         7782         7827           7797         7801         7805           7801         7805         7810	7653         7657           7657         7662           7651         7666           7661         7666           7663         7674           7683         7683           7683         7688           7686         7696           7696         7709           7705         7709           7714         7718           7722         7727           7731         7736           7736         7744           7744         7749           7735         7757           7757         7757           7757         7757           7757         7757           7757         7757           7757         7757           7757         7757           7757         7757           7757         7757           7757         7757           7757         7757           7757         7757           7757         7757           7757         7757           7757         7757           7757         7757           7757         7757           7757								

Table 58 English—High Alt, Mid Temp, Med Humidity (Temp = 74 to 90° F, Press = 23 to 27 inches, 50% Humidity)

•

					TE	MPER	ATURE	IN DE	GREES	FAHRE	NHEIT					
91.0	92.0	93.0	94.0	95.0	96.0	97.0	98.0	99.0	100.	0 101.0	102.0	103.0	104.0	105.0	106.0	107.0
$\begin{array}{c} 27.00 & 7662\\ 26.90 & 7666\\ 26.90 & 7675\\ 26.80 & 7679\\ 26.75 & 7684\\ 26.65 & 7679\\ 26.55 & 77092\\ 26.55 & 77091\\ 26.55 & 77711\\ 26.40 & 77711\\ 26.30 & 77712\\ 26.35 & 77712\\ 26.35 & 77712\\ 26.35 & 77731\\ 26.20 & 77711\\ 26.35 & 77732\\ 25.80 & 77757\\ 25.80 & 77757\\ 25.80 & 77757\\ 25.80 & 77757\\ 25.80 & 77757\\ 25.80 & 77757\\ 25.80 & 77757\\ 25.80 & 77771\\ 25.80 & 77771\\ 25.80 & 77771\\ 25.80 & 77771\\ 25.80 & 77771\\ 25.80 & 77771\\ 25.80 & 77771\\ 25.80 & 77772\\ 25.80 & 77771\\ 25.80 & 77772\\ 25.80 & 77771\\ 25.80 & 77771\\ 25.80 & 77772\\ 25.80 & 77772\\ 25.80 & 77772\\ 25.80 & 77772\\ 25.80 & 77772\\ 25.80 & 77772\\ 25.80 & 77772\\ 25.80 & 77772\\ 25.80 & 77772\\ 25.80 & 77772\\ 25.80 & 77772\\ 25.80 & 77772\\ 25.80 & 77772\\ 25.80 & 77772\\ 25.80 & 77772\\ 25.80 & 77772\\ 25.80 & 77772\\ 25.80 & 7784\\ 25.15 & 77872\\ 25.80 & 7784\\ 25.15 & 77872\\ 25.80 & 7784\\ 25.15 & 77872\\ 25.80 & 7784\\ 25.10 & 7814\\ 25.15 & 77872\\ 25.80 & 7784\\ 25.10 & 7814\\ 24.85 & 78871\\ 24.50 & 78971\\ 24.20 & 79051\\ 24.10 & 7914\\ 24.00 & 7923\\ 23.95 & 79361\\ 23.55 & 79361\\ 23.55 & 79361\\ 23.50 & 79971\\ 23.30 & 7984\\ 23.20 & 79972\\ 23.10 & 8005\\ 23.00 & 8010\\ 23.00 &$	$\begin{array}{c} 777777777777777777777777777777777777$	$\begin{array}{c} 7776684893711600493722606159488271160000918882600593882261594882717777777777777777777777777777777777$	$\begin{array}{c} 76688937\\ 77777777777777777777777777777777777$	77777777777777777777777777777777777777	7669982 659382 677071519482 669982 77777777777777777777777777777777777	$\begin{array}{c} 7669027\\ 77777777777777777777777777777777777$	7698 7703	9837777116048377160049371608493777777777777777777777777777777777777	7703 7707 7712 7716	7771203 777777777777777777777777777777777777	22612259 7772229 77777388262600593726000 7772229 7777555988937260001593728884493717777777777777777777777777777777777	$\begin{array}{c} 777777777777777777777777777777777777$	77777777777777777777777777777777777777	77777777777777777777777777777777777777	77777777777777777777777777777777777777	77359 77744 777359 77744 77560 77765 77765 77765 77765 77765 77765 77765 77762 77790 77792 77823 77904 77904 77904 77823 77824 77824 77824 77824 77824 77824 77824 77825 77824 77825 77825 77825 77825 77825 77825 77825 77825 77825 77825 77825 77825 77825 77825 77825 77825 77825 77925 779213 779213 779213 77925 79934 79955 79967 77955 77955 77955 779553 77955 779553 779575 779553 779553 779553 779553 779553 779575 799575 799575 799575 799575 799575 799575 799575 799575 799575 7995775 799575

#### Table 59 English—High Alt, High-Mid Temp, Med Humidity (Temp = 91 to 107° F, Press = 23 to 27 inches, 50% Humidity)

	TEMPERATURE IN DEGREES FAHRENHEIT													
40.0 41.0	42.0 43.0	44.0 45.0												
40.0 41.0 31.00 7030 7036	42.0 43.0 7043 7049	7055 7061			49.0 50.0 7084 7090	51.0 52.0		55.0 56.0						
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	7043         7043           7043         7053           7047         7053           7052         7058           7057         7058           7057         7058           7057         7058           7071         7077           7076         7082           7081         7087           7076         7082           7081         7087           7090         7096           7095         7101           7100         7114           7120         7124           7123         7139           7124         7120           7127         7177           7167         7182           7186         7192           7186         7192           7186         7192           7186         7192           7191         7196           7200         7206           7224         7230           7252         7268           7267         7261           7229         7234           7239         7244           7240         7320           7325 <th>7055         7065           7059         7055           7064         7077           7069         7075           7074         7082           7078         7088           7088         7094           7088         7094           7088         7094           7088         7094           7088         7094           7093         7092           7097         7003           7102         7108           7112         7113           7112         7112           7111         7116           7112         7113           7113         7137           7150         7154           7150         7154           7169         7173           7178         7184           7183         7189           7193         7193           7193         7193           7193         7193           7193         7193           7193         7193           7193         7193           7193         7193           7193         7193           7193<th>7071 707 7076 708 7081 708 7085 709 7090 709 7095 710 7100 710 7104 711</th><th>7         7083         7           7         7088         7           7         7088         7           7         7098         7           7         7093         7           7         7093         7           7         7093         7           1         7097         7           1         7107         7           1         7107         7           1         7111         7           1         71126         7           1         71135         7           2         71144         7           3         71157         7           3         71157         7           3         71168         7           7         71187         7           7         71187         7           7         71187         7           7         71267         7217           7         7127         72257           7         72206         723           7         72253         72           7         72253         72           7         72267</th><th>114       7419         119       7424         123       7429         128       7433         133       7438         134       7443         142       7447         1447       7452         152       7467         156       7462</th><th>7096         7102           7101         7110           7100         7111           7110         7116           7120         7125           7124         7130           7125         7134           7143         7149           7148         7153           7157         7163           7157         7163           7157         7166           7157         7166           7195         7200           7195         7200           7218         7214           7195         7200           7195         7200           7218         7214           7218         7214           7219         7205           7200         7214           7218         7224           7223         7228           72210         7225           7256         7261           7200         7275           7274         7285           7303         7303           7317         7317           7317         7317           7317         7317           7326<!--</th--><th>7112 7118 7117 7123 7122 7128 7126 7132 7131 7137 7136 7142 7140 7146 7145 7151 7150 7156 7155 7160 7155 7166</th><th>7119       7125         7124       7130         7129       7134         7133       7139         7134       7148         7147       7153         7157       7162         7157       7162         7161       7167         7175       7180         7180       7194         7200       7195         7194       7200         7195       7180         7180       7186         7180       7209         7208       7213         7217       7266         7221       7227         7231       72237         7223       7237         7236       7241         7250       7260         7253       7297         7266       7274         7273       7297         7296       7300         7320       7320         7320       7320         7320       7320         7320       7320         7320       7320         7320       7320         7320       7320         7320</th></th></th>	7055         7065           7059         7055           7064         7077           7069         7075           7074         7082           7078         7088           7088         7094           7088         7094           7088         7094           7088         7094           7088         7094           7093         7092           7097         7003           7102         7108           7112         7113           7112         7112           7111         7116           7112         7113           7113         7137           7150         7154           7150         7154           7169         7173           7178         7184           7183         7189           7193         7193           7193         7193           7193         7193           7193         7193           7193         7193           7193         7193           7193         7193           7193         7193           7193 <th>7071 707 7076 708 7081 708 7085 709 7090 709 7095 710 7100 710 7104 711</th> <th>7         7083         7           7         7088         7           7         7088         7           7         7098         7           7         7093         7           7         7093         7           7         7093         7           1         7097         7           1         7107         7           1         7107         7           1         7111         7           1         71126         7           1         71135         7           2         71144         7           3         71157         7           3         71157         7           3         71168         7           7         71187         7           7         71187         7           7         71187         7           7         71267         7217           7         7127         72257           7         72206         723           7         72253         72           7         72253         72           7         72267</th> <th>114       7419         119       7424         123       7429         128       7433         133       7438         134       7443         142       7447         1447       7452         152       7467         156       7462</th> <th>7096         7102           7101         7110           7100         7111           7110         7116           7120         7125           7124         7130           7125         7134           7143         7149           7148         7153           7157         7163           7157         7163           7157         7166           7157         7166           7195         7200           7195         7200           7218         7214           7195         7200           7195         7200           7218         7214           7218         7214           7219         7205           7200         7214           7218         7224           7223         7228           72210         7225           7256         7261           7200         7275           7274         7285           7303         7303           7317         7317           7317         7317           7317         7317           7326<!--</th--><th>7112 7118 7117 7123 7122 7128 7126 7132 7131 7137 7136 7142 7140 7146 7145 7151 7150 7156 7155 7160 7155 7166</th><th>7119       7125         7124       7130         7129       7134         7133       7139         7134       7148         7147       7153         7157       7162         7157       7162         7161       7167         7175       7180         7180       7194         7200       7195         7194       7200         7195       7180         7180       7186         7180       7209         7208       7213         7217       7266         7221       7227         7231       72237         7223       7237         7236       7241         7250       7260         7253       7297         7266       7274         7273       7297         7296       7300         7320       7320         7320       7320         7320       7320         7320       7320         7320       7320         7320       7320         7320       7320         7320</th></th>	7071 707 7076 708 7081 708 7085 709 7090 709 7095 710 7100 710 7104 711	7         7083         7           7         7088         7           7         7088         7           7         7098         7           7         7093         7           7         7093         7           7         7093         7           1         7097         7           1         7107         7           1         7107         7           1         7111         7           1         71126         7           1         71135         7           2         71144         7           3         71157         7           3         71157         7           3         71168         7           7         71187         7           7         71187         7           7         71187         7           7         71267         7217           7         7127         72257           7         72206         723           7         72253         72           7         72253         72           7         72267	114       7419         119       7424         123       7429         128       7433         133       7438         134       7443         142       7447         1447       7452         152       7467         156       7462	7096         7102           7101         7110           7100         7111           7110         7116           7120         7125           7124         7130           7125         7134           7143         7149           7148         7153           7157         7163           7157         7163           7157         7166           7157         7166           7195         7200           7195         7200           7218         7214           7195         7200           7195         7200           7218         7214           7218         7214           7219         7205           7200         7214           7218         7224           7223         7228           72210         7225           7256         7261           7200         7275           7274         7285           7303         7303           7317         7317           7317         7317           7317         7317           7326 </th <th>7112 7118 7117 7123 7122 7128 7126 7132 7131 7137 7136 7142 7140 7146 7145 7151 7150 7156 7155 7160 7155 7166</th> <th>7119       7125         7124       7130         7129       7134         7133       7139         7134       7148         7147       7153         7157       7162         7157       7162         7161       7167         7175       7180         7180       7194         7200       7195         7194       7200         7195       7180         7180       7186         7180       7209         7208       7213         7217       7266         7221       7227         7231       72237         7223       7237         7236       7241         7250       7260         7253       7297         7266       7274         7273       7297         7296       7300         7320       7320         7320       7320         7320       7320         7320       7320         7320       7320         7320       7320         7320       7320         7320</th>	7112 7118 7117 7123 7122 7128 7126 7132 7131 7137 7136 7142 7140 7146 7145 7151 7150 7156 7155 7160 7155 7166	7119       7125         7124       7130         7129       7134         7133       7139         7134       7148         7147       7153         7157       7162         7157       7162         7161       7167         7175       7180         7180       7194         7200       7195         7194       7200         7195       7180         7180       7186         7180       7209         7208       7213         7217       7266         7221       7227         7231       72237         7223       7237         7236       7241         7250       7260         7253       7297         7266       7274         7273       7297         7296       7300         7320       7320         7320       7320         7320       7320         7320       7320         7320       7320         7320       7320         7320       7320         7320						

Table 60 English—Low Alt, Low Temp, High Humidity (Temp = 40 to 56° F, Press = 27 to 31 inches, 80% Humidity)

-

	_													······		
					TE	MPER	ATURE	IN DEC	REES	FAHRI	ENHEIT	•				
57.0	58.0	59.0	60.0	61.0	62.0	63.0	64.0	65.0	66.0	67.0	68.0	69.0	70.0	71.0	72.0	73.0
$\begin{array}{c} 29.45 \\ 7275 \\ 29.40 \\ 7279 \\ 29.35 \\ 7284 \\ 29.30 \\ 7289 \\ 29.25 \\ 7293 \\ 29.20 \\ 7298 \\ 29.15 \\ 7303 \\ 29.10 \\ 7307 \\ 29.05 \\ 7312 \\ 29.00 \\ 7316 \\ 28.95 \\ 7321 \\ 28.95 \\ 7321 \\ 28.80 \\ 7335 \\ 28.85 \\ 7330 \\ 28.85 \\ 7330 \\ 28.80 \\ 7335 \\ 28.75 \\ 7340 \\ 28.65 \\ 7344 \\ 28.65 \\ 7344 \\ 28.65 \\ 7344 \\ 28.65 \\ 7354 \\ 28.55 \\ 7358 \\ 28.55 \\ 7358 \\ 28.55 \\ 7367 \\ 28.40 \\ 7372 \\ 28.35 \\ 7367 \\ 28.45 \\ 7367 \\ 28.40 \\ 7372 \\ 28.35 \\ 7377 \\ 28.30 \\ 7381 \\ 28.25 \\ 7386 \\ 28.00 \\ 7409 \\ 27.95 \\ 7414 \\ 27.95 \\ 7442 \\ 27.85 \\ 7423 \\ 27.85 \\ 7423 \\ 27.75 \\ 7423 \\ 27.65 \\ 7442 \\ 27.65 \\ 7442 \\ 27.65 \\ 7442 \\ 27.55 \\ 745 \\ 27.35 \\ 7460 \\ 27.45 \\ 7460 \\ 27.35 \\ 7460 \\ 27.45 \\ 7460 \\ 27.35 \\ 7461 \\ 27.55 \\ 7451 \\ 27.55 \\ 7451 \\ 27.55 \\ 7451 \\ 27.55 \\ 7451 \\ 27.55 \\ 7451 \\ 27.55 \\ 7451 \\ 27.55 \\ 7451 \\ 27.55 \\ 7451 \\ 27.55 \\ 7451 \\ 27.55 \\ 7451 \\ 27.55 \\ 7451 \\ 27.55 \\ 7451 \\ 27.55 \\ 7451 \\ 27.55 \\ 7451 \\ 27.55 \\ 7451 \\ 27.55 \\ 7451 \\ 27.55 \\ 7451 \\ 27.30 \\ 7474 \\ 27.25 \\ 7479 \\ 27.20 \\ 7483 \\ 72.15 \\ 7488 \\ 27.10 \\ 7493 \\ 27.10 \\ 7493 \\ 27.10 \\ 7493 \\ 27.10 \\ 7493 \\ 27.10 \\ 7493 \\ 27.10 \\ 7493 \\ 27.10 \\ 7493 \\ 27.10 \\ 7493 \\ 27.10 \\ 7493 \\ 27.10 \\ 7493 \\ 27.10 \\ 7493 \\ 27.10 \\ 7493 \\ 27.10 \\ 7493 \\ 27.10 \\ 7493 \\ 27.10 \\ 7493 \\ 27.10 \\ 7493 \\ 27.10 \\ 7493 \\ 27.10 \\ 7493 \\ 27.10 \\ 7493 \\ 27.10 \\ 749 \\ 74.5 \\ 740$	$\begin{array}{c} 77441\\ 77146\\ 7155\\ 7155\\ 7155\\ 7164\\ 97174\\ 7167\\ 7174\\ 7178\\ 7188\\ 7192\\ 7211\\ 72202\\ 772202$	7252538377777777777777777777777777777777	7452 7457 7466 7471 7466 7471 7480 7485 7489 7489 7489 7489 7499 7499 7499 7499	$\begin{array}{c} 548382771691500494838227162155049483827160015049338377277777777777777777777777777777777$	$\begin{array}{c} 7116649\\ 771778872221948837222194883727777777777777777777777777777777777$	$\begin{array}{c} 777777777777777777777777777777777777$	$\begin{array}{c} 71750\\ 7178859\\ 7198859\\ 712230827\\ 722242558290\\ 722222222\\ 72224453829\\ 7222355044\\ 722230504\\ 7222728\\ 7222728\\ 7222728\\ 722777\\ 7222909\\ 722777777\\ 7222909\\ 722777777777\\ 722909\\ 7227777777777777777777777777777777777$	$\begin{array}{c} 7716895994992138227772255649382772222266115777777777777777777777777777$	$\begin{array}{c} 7189\\ 719005049382716649382777777777777777777777777777777777777$	$\begin{array}{c} 711901611502493382472266150497223182277777777777777777777777777777777$	$\begin{array}{c} 938372261525049938227\\ 777222233493822722288938227\\ 7222222245572626775049938227\\ 7222222224557262777777777777777777777777$	$\begin{array}{c} 9948 \\ 9948 \\ 77220137 \\ 72223500 \\ 722233500 \\ 4993 \\ 820137 \\ 72223350 \\ 7223330 \\ 7223330 \\ 7233330 \\ 7233330 \\ 7233330 \\ 7233330 \\ 7233330 \\ 7233330 \\ 72330 \\ 723330 \\ 723330 \\ 723330 \\ 723330 \\ 72330 \\ 72330 \\ 723330 \\ 723330 \\ 7230$	$\begin{array}{c} 777777777777777777777777777777777777$	$\begin{array}{c} 722124\\ 7222337\\ 72224461550\\ 7222837\\ 72224461550\\ 7222837\\ 72224461550\\ 7222837\\ 7222837\\ 7222837\\ 7222837\\ 7222837\\ 7222837\\ 7222837\\ 7222837\\ 7222837\\ 7222837\\ 7232827\\ 7333861\\ 73338861\\ 7333891500\\ 440593\\ 7444583\\ 744583\\ 7449583\\ 745835\\ 745553350\\ 74555582\\ 755555\\ 755555\\ 755555\\ 755555\\ 755555\\ 755555\\ 755555\\ 755555\\ 755555\\ 755555\\ 755555\\ 755555\\ 755555\\ 755555\\ 755555\\ 755555\\ 75555\\ 755555\\ 755555\\ 755555\\ 755555\\ 7$	$\begin{array}{c} 77722229488377266152948827777777777777777777777777777777777$	$\begin{array}{c} 72220\\ 722305\\ 72232344\\ 722537722232344\\ 72253772225372266\\ 722899382777228992\\ 7228992277228992\\ 72300116\\ 733229927733229\\ 733229927733229\\ 733229927733229\\ 7332299277332259\\ 7332299277332259\\ 7332299277332259\\ 7332299277733882277336\\ 7332259777338822777338822773366\\ 7377338827773388227773388227737338822725526\\ 737733882277777374461550493827775522326\\ 744960059448377255249\\ 7450059448377255249\\ 755549538277555493827755549\\ 7555381555771755549\\ 7555381557777777777777777777777777777777$

Table 61 English—Low Alt, Low-Mid Temp, High Humidity (Temp = 57 to 73° F, Press = 27 to 31 inches, 80% Humidity)

	TEMPERATURE IN DEGREES FAHRENHEIT																
	74.0	75.0	76.0	77.0	78.0	79.0	80.0	81.0	82.0	83.0	84.0	85.0	86.0	87.0	88.0	89.0	90.0
BAROMETRIC PRESSURE IN INCHES OF MERCURY	$\begin{array}{c} 31.00 & 7227\\ 30.95 & 7231\\ 30.90 & 7236\\ 30.85 & 7240\\ 30.85 & 7240\\ 30.65 & 7254\\ 30.65 & 7257\\ 30.55 & 7267\\ 30.55 & 7267\\ 30.55 & 7267\\ 30.45 & 7285\\ 30.35 & 7290\\ 30.25 & 7290\\ 30.25 & 7290\\ 30.25 & 7290\\ 30.25 & 7302\\ 29.85 & 7330\\ 29.95 & 7321\\ 29.95 & 73312\\ 29.95 & 73312\\ 29.95 & 73312\\ 29.95 & 73312\\ 29.95 & 73321\\ 29.95 & 73321\\ 29.95 & 73321\\ 29.95 & 73321\\ 29.95 & 73322\\ 29.85 & 73352\\ 29.55 & 7336\\ 29.55 & 73375\\ 29.55 & 73375\\ 29.55 & 73375\\ 29.30 & 73776\\ 29.35 & 73776\\ 29.35 & 73776\\ 29.35 & 73776\\ 29.35 & 73776\\ 29.35 & 73776\\ 29.35 & 73776\\ 29.35 & 73776\\ 29.35 & 73776\\ 29.35 & 73776\\ 29.35 & 73776\\ 29.35 & 7424\\ 28.85 & 7420\\ 28.90 & 7411\\ 28.85 & 7424\\ 28.55 & 7424\\ 28.55 & 7424\\ 28.55 & 7426\\ 28.35 & 7465\\ 28.35 & 7465\\ 28.35 & 7465\\ 28.35 & 7465\\ 28.35 & 7465\\ 28.35 & 7465\\ 28.35 & 7465\\ 28.35 & 7465\\ 28.35 & 7465\\ 28.35 & 7465\\ 28.35 & 7465\\ 27.95 & 75511\\ 27.85 & 75514\\ 27.75 & 75537\\ 27.35 & 75555\\ 27.305 & 75563\\ 27.35 & 75563\\ 27.305 & 75563\\ 27.305 & 75563\\ 27.35 & 75572\\ 27.35 & 75575\\ 27.35 & 75572\\ 27.35 & 75575\\ 27.$	7237 7241 7246 7250	$\begin{array}{c} 3427\\ 7722556059483722015948372601594837277777777777777777777777777777777777$	7248 7252 7257 7261 7266 7270 7270	7253 7258 7262 7267 7271 7271 7276	$\begin{array}{c} 7726994993827716607493838277177777777777777777777777777777777$	772269004938271500493826150777777777777777777777777777777777777	$\begin{array}{c} 5504\\ 72277882260150\\ 733132272882260150\\ 73333334450488377777777777777777777777777777777777$	7275 7280	7281	$\begin{array}{c} 826152299908371160059333442777777777777777777777777777777777$	7292 7296 7300 7305 7309 7314 7318 7322 7327	93716059382715504937260594827177777777777777777777777777777777777	7303 7307 7311 7316 7320 7324 7329	$\begin{array}{c} 777777777777777777777777777777777777$	$\begin{array}{c} 777777777777777777777777777777777777$	$\begin{array}{c} 7314\\ 7323\\ 73323\\ 73345\\ 73345\\ 73345\\ 733562\\ 73345\\ 733562\\ 737584\\ 93899\\ 735667\\ 7375884\\ 9397\\ 744193\\ 8997\\ 744193\\ 8997\\ 744228\\ 8937\\ 744450\\ 44232\\ 611593\\ 8893\\ 744193\\ 8997\\ 744450\\ 744450\\ 744450\\ 744893\\ 7755115\\ 93555\\ 8938\\ 755563\\ 7755563\\ 755563\\ 755563\\ 755563\\ 755982\\ 266337\\ 16628\\ 37755598\\ 266337\\ 16628\\ 37755563\\ 755563\\ 755563\\ 755982\\ 266337\\ 16628\\ 37755563\\ 755563\\ 755982\\ 266337\\ 16626\\ 76659\\ 376659\\ 76659$

Table 62	English—Low Alt, Mid Temp, High Humidity
(Temp	= 74 to 90° F, Press = 27 to 31 inches, 80% Humidity)

272

		TE	EMPER/	ATURE	IN DEG	REES	FAHRE	NHEIT					
91.0 92.0 93.	0 94.0 9	5.0 96.0	97.0	98.0	99.0	100.0	101.0	102.0	103.0	104.0	105.0	106.0	107.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	5         7341         7           9         7345         7           9         7345         7           8         7354         7           8         7354         7           8         7354         7           8         7354         7           8         7354         7           7         7362         7           7         7362         7           7         7366         7           7         7375         7           7         7388         7           7         7397         7           7         7397         7           7         7401         7           7         7414         7           7         7423         7           7         7423         7           7         7423         7           7         7423         7           7         7423         7           7         7423         7           7         7423         7           7         7423         7           7         7424         7	09 7614 14 7619 18 7623 22 7627 27 7631 1 7636 35 7640 40 7644 44 7649 48 7653 52 7657 7662 57 7662 561 7666 57 7665 7670 7675 74 7679 768 7688	7357 7361 7365 7370 7374 7378 7383 7387 7391 7391 7396 7400 7404 7408 7413 7413	77777777777777777777777777777777777777	$\begin{array}{c} 73367261\\ 733889382611593826615593826615593826155938266156666666666666666666666666666666666$	$\begin{array}{c} 93772860059937260493777777777777777777777777777777777777$	$\begin{array}{c} 75671\\ 75779\\ 75779\\ 7588\\ 7592\\ 7588\\ 7592\\ 76005\\ 76009\\ 7613\\ 82613\\ 76622\\ 63593\\ 76655\\ 6665\\ 7776682\\ 6699\\ 7695\\ 7770\\ 7682\\ 6699\\ 7770\\ 7770\\ 7777$	7584937775977777777777777777777777777777777	76061 7777628 7777777777777777777777777777777	7675 7680 7684 7692 7697 7705 7705 7709 7713 7713 7712 7726	75837 75591 75595 76004 76617 76629 76629 766559 766889 777010 77716 77777 77777 77777777777777	7584 7592 777596 77605 77605 77662 776630 776630 776630 776630 776630 776630 776651 6660 776694 776694 77705 77766894 77705 77715 77715 77715 77728 77728 77728 77736	74011 74120 74248 74237 74248227 744582666 7777777777777777777777777777777777

#### Table 63 English—Low Alt, High-Mid Temp, High Humidity (Temp = 91 to 107° F, Press = 27 to 31 inches, 80% Humidity)

Table 64 English—High Alt, Low Temp, High Humidity (Temp = 40 to 56° F, Press = 23 to 27 inches, 80% Humidity)

Table 65 English—High Alt, Low-Mid Temp, High Humidity (Temp = 57 to 73° F, Press = 23 to 27 inches, 80% Humidity)

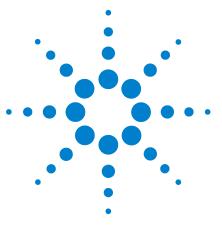
						TE	MPER	ATURE	IN DEC	GREES	FAHRI	ENHEIT	-				
	74.0	75.0	76.0	77.0	78.0	79.0	80.0	81.0	82.0	83.0	84.0	85.0	86.0	87.0	88.0	89.0	90.0
BAROMETRIC PRESSURE IN INCHES OF MERCURY	$\begin{array}{c} 27.00 & 7586\\ 26.95 & 7590\\ 26.95 & 7590\\ 26.85 & 7690\\ 26.75 & 7604\\ 26.75 & 7664\\ 26.75 & 7662\\ 26.55 & 7622\\ 26.55 & 7622\\ 26.55 & 7622\\ 26.55 & 76631\\ 26.45 & 7635\\ 26.35 & 7644\\ 26.35 & 7664\\ 26.35 & 7664\\ 26.35 & 7667\\ 26.05 & 7667\\ 26.00 & 7676\\ 25.95 & 76680\\ 25.85 & 76694\\ 25.85 & 76694\\ 25.85 & 76694\\ 25.85 & 76694\\ 25.85 & 77703\\ 25.65 & 77712\\ 25.55 & 77712\\ 25.55 & 77724\\ 25.55 & 77734\\ 25.35 & 77734\\ 25.35 & 77748\\ 25.35 & 77748\\ 25.35 & 77748\\ 25.35 & 77748\\ 25.35 & 77748\\ 25.35 & 77774\\ 24.85 & 7780\\ 24.95 & 7784\\ 24.95 & 77801\\ 24.455 & 7806\\ 24.455 & 7806\\ 24.455 & 7806\\ 24.455 & 7806\\ 24.455 & 7806\\ 24.455 & 7806\\ 24.455 & 7806\\ 24.455 & 7806\\ 24.455 & 7806\\ 24.455 & 7806\\ 24.455 & 78819\\ 24.305 & 7828\\ 24.20 & 7837\\ 24.15 & 7828\\ 24.20 & 7837\\ 24.15 & 78783\\ 23.95 & 78649\\ 23.95 & 78738\\ 23.75 & 7878\\ 23.75 & 7878\\ 23.65 & 78738\\ 23.75 & 7878\\ 23.75 & 7878\\ 23.75 & 7878\\ 23.75 & 7878\\ 23.55 & 78966\\ 23.35 & 78966\\ 23.45 & 7918\\ 23.55 & 78966\\ 23.45 & 7918\\ 23.55 & 7896\\ 23.305 & 7924\\ 23.55 & 7994\\ 23.55 & 7994\\ 23.55 & 7940\\ 23.05 & 7940\\ 23.00 & 7945\\ 23.00 & 7945\\ 23.00 & 7945\\ 23.00 & 7946\\ 23.00 & 7946\\ 23.00 & 7945\\ 23.00 & 7940\\ 23.00 & 7945\\ 23.00 & 7946\\ 23.00 & 7945\\ 23.00 & 7946\\ 23.00 & 7945\\ 23.00 & 7946\\ 23.00 & 7945\\ 23.00 & 7946\\ 23.00 & 7945\\ 23.00 & 7946\\ 23.00 & 7945\\ 23.00 & 7946\\ 23.00 & 7945\\ 23.00 & 7946\\ 23.00 & 7945\\ 23.00 & 7946\\ 23.00 & 7945\\ 23.00 & 7946\\ 23.00 & 7945\\ 23.00 & 7946\\ 23.00 & 7945\\ 23.00 & 7946\\ 23.00 & 7945\\ 23.00 & 7946\\ 23.00 & 7945\\ 23.00 & 7945\\ 23.00 & 7946\\ 23.00 & 7945\\ 23.00 & 7946\\ 23.00 & 7945\\ 23.00 & 7946\\ 23.00 & 7945\\ 23.00 & 7946\\ 23.00 & 7945\\ 23.00 & 7946\\ 23.00 & 7945\\ 23.00 & 7946\\ 23.00 & 7946\\ 23.00 & 7946\\ 23.00 & 7946\\ 23.00 & 7945\\ 23.00 & 7946\\ 23.00 & 7946\\ 23.00 & 7945\\ 23.00 & 7946\\ 23.00 & 7945\\ 23.00 & 7946\\ 23.00 & 7945\\ 23.00 & 7946\\ 23.00 & 7945\\ 23.00 & 7946\\ 23.00 & 7945\\ 23.00 & 7945\\ 23.00 & 7945\\ 23.00 & 7946\\ 23.00 & 7945\\ 23.00 & 7946\\ 23.00 & 7945\\ 23.00 & 7946\\ 23.00 & 7946\\ 23.00 & 7945\\ 23.00 & 794$	7595	77777777777777777777777777777777777777			$\begin{array}{c} 76619\\ 777777777777777777777777777777777777$	777777777777777777777777777777777777	777777777777777777777777777777777777	$\begin{array}{c} 259382277777777777777777777777777777777777$	$\begin{array}{c} 766384456666948271\\ 77766666948291600938226150493777777777777777777777777777777777777$	$\begin{array}{c} 7766645561559488397777777777777777777777777777777777$	$\begin{array}{c} 7766480555665077887266901594837717777777777777777777777777777777777$	7664556671503882601501488372260259386271504493727777777777777777777777777777777777	$\begin{array}{c} 7766556661594882716004937727777777777777777777777777777777777$	$\begin{array}{c} 766566715704889377777777777777777777777777777777777$	777777777777777777777777777777777777	76672 776780 776780 77680 7777777777777777777

Table 66 English—High Alt, Mid Temp, High Humidity (Temp = 74 to 90° F, Press = 23 to 27 inches, 80% Humidity)

					TEI	MPERA	TURE	IN DEG	REES	FAHRE	NHEIT					
91.0	92.0	93.0	94.0	95.0	96.0	97.0	98.0	99.0	100.0	101.0	102.0	103.0	104.0	105.0	106.0	107.0
$\begin{array}{c} 27.00 & 7668\\ 26.90 & 7672\\ 26.85 & 7681\\ 26.80 & 7681\\ 26.80 & 7680\\ 26.70 & 7694\\ 26.60 & 77707\\ 26.50 & 77707\\ 26.50 & 77711\\ 26.45 & 77716\\ 26.45 & 77729\\ 26.20 & 77729\\ 26.20 & 77729\\ 26.20 & 77729\\ 26.20 & 77737\\ 26.10 & 77426\\ 26.30 & 77729\\ 26.20 & 77750\\ 26.30 & 77750\\ 26.30 & 77750\\ 26.30 & 77750\\ 25.90 & 77750\\ 25.90 & 77763\\ 25.90 & 77763\\ 25.90 & 77763\\ 25.90 & 77763\\ 25.90 & 77777\\ 25.65 & 77794\\ 25.50 & 77794\\ 25.50 & 77850\\ 25.55 & 778850\\ 25.55 & 778850\\ 25.50 & 778850\\ 25.25 & 78229\\ 25.10 & 78857\\ 25.10 & 78857\\ 25.10 & 78857\\ 24.50 & 78857\\ 24.50 & 78855\\ 24.70 & 78855\\ 24.70 & 78855\\ 24.70 & 78855\\ 24.70 & 78855\\ 24.70 & 78855\\ 24.70 & 78855\\ 24.70 & 78855\\ 24.70 & 78855\\ 24.70 & 78855\\ 24.70 & 78855\\ 24.70 & 78994\\ 24.30 & 79903\\ 24.20 & 79911\\ 24.10 & 79224\\ 23.85 & 79954\\ 23.85 & 79954\\ 23.85 & 79954\\ 23.85 & 79954\\ 23.85 & 79954\\ 23.55 & 79977\\ 23.45 & 79948\\ 23.55 & 79977\\ 23.45 & 79948\\ 23.55 & 79977\\ 23.45 & 79948\\ 23.55 & 79977\\ 23.45 & 79948\\ 23.55 & 79977\\ 23.45 & 79948\\ 23.50 & 79948\\ 23.50 & 79948\\ 23.50 & 79948\\ 23.50 & 79948\\ 23.50 & 79948\\ 23.50 & 79948\\ 23.50 & 79948\\ 23.50 & 79948\\ 23.50 & 79948\\ 23.25 & 79948\\ 23.50 & 79948\\ 23.50 & 79948\\ 23.50 & 79948\\ 23.00 & 8016\\ 2$	$\begin{array}{c} 777777777777777777777777777777777777$	777689059938261259482711550468377166683771680949937260259382261559482777777777777777777777777777777777777	77699504827172150482777777777777777777777777777777777777	776916 69916 69916 777777777777777777777	77777777777777777777777777777777777777	777014 777077777777777777777777777777777	77060 77714 777227 777340 777728 7777449 777777777777777777777777777777	06115 7771533415 777777777777777777777777777777777777	$\begin{array}{c} 1150\\ 7777224\\ 82827\\ 777777777777558\\ 8297150\\ 48827150\\ 8482271359\\ 482271559\\ 482271559\\ 482271559\\ 482271559\\ 482271559\\ 482271559\\ 482271559\\ 482271559\\ 482271559\\ 482271559\\ 482271559\\ 482271559\\ 482271559\\ 48227159\\ 48222262\\ 48227159\\ 48227159\\ 48222262\\ 48227159\\ 4827159$	160 77724 77777777777777777777777777777777	77725 777734 777755 77775 77775 77775 77775 77777777	77734 777777777777777777777777777777777	77777777777777777777777777777777777777	$\begin{array}{c} 777404\\ 77757\\ 77748\\ 77757\\ 777615\\ 9937\\ 77826\\ 9037\\ 778822\\ 8007\\ 778822\\ 8007\\ 778822\\ 8007\\ 778822\\ 8007\\ 788224\\ 9037\\ 788224\\ 8007\\ 788224\\ 8007\\ 788224\\ 800222\\ 8007\\ 77825\\ 7882416\\ 8007\\ 77825\\ 7882416\\ 8007\\ 77825\\$	8058 8062 8066 8070 8075	77459 777582 77777777777777777777777777777777

#### Table 67 English—High Alt, High-Mid Temp, High Humidity (Temp = 91 to 107° F, Press = 23 to 27 inches, 80% Humidity)

### 13 Wavelength-of-Light Compensation



Agilent Laser and Optics User's Manual Volume I

# 14 Material Expansion Coefficients

Linear Thermal Expansion Coefficients of Metals and Alloys, 280



## **Linear Thermal Expansion Coefficients of Metals and Alloys**

Table 68 provides the linear thermal expansion coefficients of the most frequently used metals and allows.

	Coefficient of	Coefficient of Expansion	
Alloys	ppm/°C	ppm/°F	
ALUMINUM AND ALUMINUM ALLOYS			
Aluminum (99.996%)	23.6	13.1	
Wrought Alloys			
EC 1060 and 1100	23.6	13.1	
2011 and 2014	23.0	12.8	
2024	22.8	12.7	
2218	22.3	12.4	
3003	23.2	12.9	
4032	19.4	10.8	
5005, 5050, and 5052	23.8	13.3	
5056	24.1	13.4	
5083	23.4	13.0	
5086	23.9	13.3	
5154	23.9	13.3	
5357	23.7	13.2	
5456	23.9	13.3	
6061 and 6063	23.4	13.0	
6101 and 6151	23.0	12.8	
7075	23.2	12.9	
7090 and 7178	23.4	13.0	

Table 68 Linear thermal expansion coefficients of metals and alloys

	Coefficient of Expansion	
Alloys	ppm/°C	ppm/°F
ALUMINUM AND ALUMINUM ALLOYS (Continued)		
Casting Alloys		
A13	20.4	11.4
43 and 108	22.0	12.3
A108	21.5	12.0
A132	19.0	10.6
D132	20.5	11.4
F132	20.7	11.5
138	21.4	11.9
142	22.5	12.5
195	23.0	12.8
B195	22.0	12.3
214	24.0	13.4
220	25.0	13.9
319	21.5	12.0
355	22.0	12.3
356	21.5	12.0
360	21.0	11.7
750	23.1	12.9
40E	24.7	13.8
COPPER AND COPPER ALLOYS		
Wrought Coppers		
Pure Copper	16.5	9.2
Electrolytic Tough Pitch Copper (ETP)	16.8	9.4
Deoxidized Copper, High Residual Phosphorous (DHP)	17.7	9.9
Oxygen-Free Copper	17.7	9.9
Free-Machining Copper 0.5% Te or 1% Pb	17.7	9.9

Table 68 Linear thermal expansion coefficients of metals and alloys (continued)

#### 14 Material Expansion Coefficients

	Coefficient of Ex	Coefficient of Expansion	
Alloys	ppm/°C	ppm/°F	
COPPER AND COPPER ALLOYS (Continued)			
Wrought Alloys (Continued)			
Gilding, 95%	18.1	10.1	
Commercial Bronze, 90%	18.4	10.3	
Jewelry Bronze, 87.5%	18.6	10.4	
Red Brass, 85%	18.7	10.4	
Low Brass, 80%	19.1	10.6	
Cartridge Brass, 70%	19.9	11.1	
Yellow Brass	20.3	11.2	
Muntz Metal	20.8	11.5	
Leaded Commercial Bronze	18.4	10.2	
Low-Leaded Brass	20.2	11.3	
Medium-Leaded Brass	20.3	11.3	
High-Leaded Brass	20.3	11.3	
Extra-High-Leaded Brass	20.5	11.4	
Free-Cutting Brass	20.5	11.4	
Leaded Muntz Metal	20.8	11.6	
Forging Brass	20.7	11.5	
Architectural Bronze	20.9	11.6	
Inhibited Admiralty	20.2	11.3	
Naval Brass	21.2	11.8	
Leaded Naval Brass	21.2	11.8	
Manganese Bronze (A)	21.2	11.8	
Phosphorous Bronze, 5% (A)	17.8	9.9	
Phosphorous Bronze, 8% (C)	18.2	10.1	
Phosphorous Bronze, 10%(D)	18.4	10.3	
Phosphorous Bronze, 1.25%	17.8	9.9	

Table 68	Linear thermal	expansion	coefficients	of metals	and alloys	(continued)	)
		capanoion	Cocincicito	or metals	ana anoys	(continucu)	1 -

	Coefficient of Expansion	
Alloys	ppm/°C	ppm/°F
COPPER AND COPPER ALLOYS (Continued)		
Wrought Alloys (Continued)		
Free-Cutting Phosphorous Bronze	17.3	9.6
Cupro-Nickel, 30%	16.2	9.0
Cupro-Nickel, 10%	17.1	9.5
Nickel Silver, 65-18	16.2	90
Nickel Silver, 55-18	16.7	9.3
Nickel Silver, 65.12	16.2	9.0
High-Silicon Bronze (A)	18.0	10.0
Low-Silicon Bronze (B)	179	10.0
Aluminum Bronze (3)	16.4	9.2
Aluminum-Silicon Bronze	18.0	10.0
Aluminum Bronze	16.8	9.4
Beryllium Copper	17.8	9.9
Casting Alloys		
88 Cu-8 SN-4 Zn	18.0	10.0
88 Cu-11 Sn	18.4	10.3
88 Cu-6 Sn-1.5 Pb-4.5 Zn	18.5	10.3
87 Cu-8 Sn-1 Pb-4 Zn	18.0	10.0
87 Cu-10 Sn-1 Pb-2 Zn	18.0	10.0
80 Cu-10 Sn-10 Pb	18.5	10.3
78 Cu-7 Sn-15 Pb	18.5	10.3
85 Cu-5 Sn-5 Pb-5 Zn	18.1	10.0
72 Cu-1 Sn-3 Pb-24 Zn	20.7	11.5
67 Cu-1 Sn-3 Pb-29 Zn	20.2	11.3
61 Cu-1 Sn-1 Pb-37 Zn	21.6	12.0
Manganese Bronze (60,000 psi)	20.5	11.4

Table 68 Linear thermal expansion coefficients of metals and alloys (continued)

	Coefficient of Expansion	
Alloys	ppm/°C	ppm/°F
COPPER AND COPPER ALLOYS (Continued)		
Casting Alloys (Continued)		
Manganese Bronze (65,000 psi)	21.6	12.0
Manganeze Bronze (110,000 psi)	19.8	11.0
Aluminum Bronze (Alloy 9A)	17.0	9.5
Aluminum Bronze (Alloy 9B)	17.0	9.5
Aluminum Bronze (Alloys 9C & 9D)	16.2	9.0
IRON AND IRON ALLOYS		
Pure Iron	11.7	6.5
Fe-C Alloys		
0.06% C	11.7	6.5
0.22% C	11.7	6.5
0.40% C	11.3	6.3
0.56% C	11.0	6.1
1.08% C	10.8	6.0
1.45% C	10.1	5.6
Invar (36 Ni)	0 to 2	to 1.1
13 Mn-1.2 C	18.0	10.0
13 Cr-0.35 C	10.0	5.6
12.0 Cr-0.4 Ni-0.09 C	9.8	5.5
17.7 Cr-9.6 Ni-0.06 C	16.5	9.2
18. W-4 Cr-1 V	11.2	6.2
Gray Cast Iron	10.5	5.7
Malleable Iron (Pearlitic)	12.0	6.7
LEAD AND LEAD ALLOYS		
Corroding Lead (99.73+% Pb)	29.3	16.3
5-95 Solder	28.7	16.0
20-80 Solder	26.5	14.8
50-50 Solder	23.4	13.0

Table 68	Linear thermal	expansion	coefficients	of metals	and alloys	(continued)

	Coefficient of Expansion	
Alloys	ppm/°C	ppm/°F
LEAD AND LEAD ALLOYS (Continued)		
1% Antimonial Lead	28.8	16.1
Hard Lead (96 Pb, 4 Sb)	27.8	15.5
Hard Lead (94Pb, 6 Sb)	27.2	15.2
8% Antimonial Lead	26.7	14.9
9% Antimonial Lead	26.4	14.7
Lead-Base Babbitt:		
SAE 14	19.6	10.9
Alloy 8	24.0	13.4
MAGNESIUM AND MAGNESIUM ALLOYS		
Magnesium (99.8%)	25.2	14.1
Casting Alloys		
AM100A	25.2	14.1
AZ63A	26.1	14.6
AZ91A, B, C	26.0	14.5
AZ92A	25.2	14.1
HZ32A	26.7	14.9
ZH42	27.0	15.1
ZH62A	27.1	15.1
AK51A	26.1	14.6
EZ33A	26.1	14.6
EK30A and EK41A	26.1	14.6
Wrought Alloys		
M1A and A3A	26.0	14.5
AZ31B and PE	26.0	14.5
AZ61A and AZ80A	26.0	14.5
ZK60A, B	26.0	14.5
HM31A	26.1	14.6

Table 68 Linear thermal expansion coefficients of metals and alloys (continued)

### 14 Material Expansion Coefficients

	Coefficient of E	Coefficient of Expansion	
Alloys	ppm/°C	ppm/°F	
NICKEL AND NICKEL ALLOYS			
Nickel (99.95% Ni-+Co)	13.3	7.4	
Duranickel	13.0	7.2	
Monel	14.0	7.8	
Monel (cast)	12.9	7.2	
Inconel	11.5	6.4	
Ni-o-nel	12.9	7.2	
Hastelloy B	10.0	5.6	
Hastelloy C	11.3	6.3	
Hastelloy D	11.0	6.1	
Hastelloy F	14.2	7.9	
Hastelloy N	10.4	5.8	
Hastelloy W	11.3	6.3	
Hastelloy X	13.8	7.7	
Illium G	12.19	6.8	
Illium R	12.0	26.7	
80 Ni-20 Cr	17.3	9.6	
60 Ni-24 Fe-16Cr	17.0	9.5	
35 Ni-45 Fe-20 Cr	15.8	8.8	
Constantan	18.8	10.5	
STAINLESS STEELS			
301	16.9	9.4	
302	17.3	9.6	
302B	16.2	9.0	
303	17.3	9.6	
304	17.3	9.6	
305	17.3	9.6	
308	17.3	9.6	

Table 68 Linear thermal expansion coefficients of metals and alloys (continued)

	Coefficient of Expansion	
Alloys	ppm/°C	ppm/°F
STAINLESS STEELS (Continued)		
309	14.9	8.3
310	14.4	8.0
314	15.1	8.4
316	16.0	8.9
317	16.0	8.9
321	16.7	9.3
347	16.7	9.3
501	11.15	6.2
502	11.15	6.2
403	9.9	5.5
405	10.8	6.0
410	11.0	6.1
416	9.9	5.5
420	10.25	5.7
430	10.45	5.8
430F	10.45	5.8
431	11.7	6.5
440A	10.1	5.6
440B	10.1	5.6
440C	10.1	5.6
446	10.6	5.9
TITANIUM AND TITANIUM ALLOYS		
99.9% Ti	8.41	4.7
99.0% Ti	8.55	4.76
Ti-5 A1-2.5 Sn	9.36	5.2
Ti-8 Mn	8.64	4.8

Table 68 Linear thermal expansion coefficients of metals and alloys (continued)

	Coefficient of Ex	Coefficient of Expansion	
Alloys	ppm/°C	ppm/°F	
ZINC AND ZINC ALLOYS			
Pure Zinc	39.7	22.1	
AG40A Alloy	27.4	15.3	
AC41A Alloy	27.4	15.3	
Commercial Rolled Zinc:			
0.08 Pb	32.5	18.1	
03 Pb, 0.3 Cd	33.9*	18.9	
Rolled Zinc Allow (1Cu, 0.010 Mg)	34.8**	19.4	
An-Cu-Ti Alloy (0.8 Cu, 0.15 Ti)	24.9***	13.9	
** With the gra	rain; 23.4 across the grain ain; 21.1 across the grain ain; 19.4 across the grain		
PURE METALS			
Beryllium	11.6	6.5	
Cadmium	29.8	16.6	
Calcium	22.3	12.4	
Chromium	6.2	3.5	
Cobalt	13.8	7.7	
Gold	14.2	7.9	
Iridium	6.8	3.8	
Lithium	56.0	31.0	
Manganese	22.0	12.3	
Palladium	11.76	6.6	
Platinum	8.9	5.0	
Rhenium	6.7	3.7	
Rhodium	8.3	4.6	
Ruthenium	9.1	5.1	
Silicon	5.0	2.8	

Table 68 Linear thermal expansion coefficients of metals and alloys (continued)

	Coefficient of Expansion	
Alloys	ppm/°C ppm/°F	
PURE METALS (Continued)		
Silver	19.68	11.0
Tungsten	4.6	2.7
Vanadium	8.3	4.6
Zirconium	5.85	3.3

Table 68 Linear thermal expansion coefficients of metals and alloys (continued)

### 14 Material Expansion Coefficients





**Abbé error** – Abbé error occurs when the measuring point of interest is displaced from the actual measuring scale location and unwanted angular motion occurs in the positioning system.

Abbé error makes the indicated position either shorter or longer than the actual position, depending on the angular offset.

AC interferometer – A two-frequency interferometer.

**Accuracy** – The maximum deviation of a measurement from a known standard or true value.

**Air deadpath** – The most frequently encountered form of interferometer deadpath is the difference in air path lengths between the reference and measurement arms when the stage is at its zero or home position.

**Axis electronics** – The modular electronics needed to run one axis of measurement.

**Beam splitter** – A device to separate and direct light beams, sending the beams straight through, reflecting them at a right angle, or both.

**CMM** – A precision coordinate measuring machine.

**Compensation, Wavelength-of-Light** – Correction for the small changes in the wavelength of light due to changes in the refractive index of air.

**Cosine error** – An error between the measured distance and the actual distance traveled. The error results from misalignment of the measurement axis (the laser beam) to the mechanical axis of motion. This error is called cosine error because its magnitude is proportional to the cosine of the angle of misalignment.

**Cube corner** – Also called a retroreflector. A mirror assembly that always reflects the light beam parallel to the incoming beam.

**DC interferometer** – A single-frequency interferometer.

**Deadpath** – The difference in OPL (optical path length) between the reference and measurement arms of an interferometer when the stage is at its zero or home position.

**Deadpath error**— If interferometer deadpath exists and is not compensated, the measurement stage zero point or home position will appear to move around with changes in air temperature, pressure, humidity and/or with changes in temperature of glass components and the metrology frame.

**Differential interferometer** – An interferometer assembly in which the fixed reference mirror can be remotely mounted, allowing a differential measurement.

**Differential measurement** – A measurement in which both the reference beam and the measurement beam travel to external mirrors outside the interferometer housing.

# THE SIX DEGREES OF FREEDOM

Figure 71 Degrees of freedom (for X-Axis)

**Degrees of freedom** – Possible motions.

Generally, there are six degrees of freedom for each axis as shown in Figure 71. Three of the degrees of freedom are translational. Three of the degrees of freedom are rotational.

**ESD** – Electrostatic Discharge. A natural phenomenon which, while possibly insignificant on a human scale, can ruin a static-sensitive electronic component. For ESD-avoidance steps, see the Chapter 8, "Troubleshooting," in this manual.

**Etalon** – An etalon is an optical reference cavity. When used in the wavelength tracker, the etalon provides a fixed physical distance reference to the differential interferometer. Any length change measured in the etalon is presumed to be due to a change in the optical path length through the air in the cavity, rather than a change in the cavity size

 $\mathbf{f_l}$  – The lower one of the two frequencies in the laser beam.

 $\mathbf{f}_2$  – The higher one of the two frequencies in the laser beam.

 $\mathbf{f}_{\mathbf{A}}, \mathbf{f}_{\mathbf{B}}$  – Frequency paths in an interferometer.

**Half-wave plate** — An optical element which introduces a relative phase shift of 180 degrees between the orthogonal components of a wave. This changes the handedness of elliptical and circular light, changing right to left and vice-versa.

HEX – Short for Hexadecimal. See Number systems.

**Interferometer** — The term interferometer may be applied to any optical arrangement where a beam of light from a light source is separated into two or more paths by a beam splitter and the parts are subsequently recombined after traversing different optical paths. The two components then produce interference.

**Kinematic mounting** – Kinematic means that all six degrees of freedom (3 translational, 3 rotational) are uniquely and unambiguously restricted.

For kinematic mounting uses a locating plane, a locating line, and a locating point.

The locating plane will be the surface to which the top or the bottom of the interferometer is bolted.

The locating line should be a 2-point contact (or rail) which aligns the front face of the interferometer.

The locating point should be a 1-point contact (or pad) which constrains side-to-side translations of the interferometer.

When installing the interferometer, press it firmly against its locating plane, line, and point while torquing down the mounting screws. If the platform is made with reasonable accuracy, this mounting method can completely eliminate the need to adjust or align a referenced interferometer during installation. Then only the laser beam itself will need to be aligned to its proper position.

**Laser** – An acronym for "Light Amplification by Stimulated Emission of Radiation." A laser is a device that uses the natural oscillations of atoms or molecules between energy levels for generating coherent light.

**Laser Head** – The laser source with its focusing and polarization components.

**Laser Interferometry** – A technique for measuring distance using the wavelength of laser light by observing and counting optical interference patterns. It can also refer to devices using interferometric techniques to measure surface flatness.

**Linear interferometer** – An interferometer designed to use cube corners (retroreflectors) as opposed to plane mirrors.

**Measurement frequency** – The frequency of interference wavefronts detected by the receiver.

MTC – Material Temperature Compensation term.

**Number systems** – Number systems used in dealing with the computer are typically one (or more) of the following: binary, octal, decimal, or hexadecimal (hex). To help you understand the relationship of these number systems, refer to Table 69. Calculators and computer programs that can convert from one of these number systems to another are available from Agilent Technologies and other sources.

Throughout this manual, numbers may be represented in binary (base 2), octal (base 8), decimal (base 10), or hexadecimal (base 16) number systems. Where it is necessary to specify the number system used in order to reduce the possibility of confusion, a base number will be indicated as a subscript or in brackets ("[]") at the end of the number.

For example, 100[16] = 256[10] = 400[8] = 10000000[2].

Base	Binary 2	Octal 8	Hexa- decimal 16	Decimal 10
	0 000	0 0	0	0
	0 001	01	1	1
	0 010	02	2	2
	0 011	03	3	3
	0 100	04	4	4
	0 001	05	5	5
	0 110	06	6	6
	0 111	07	7	7
	1 000	10	8	8
	1 001	11	9	9
	1 010	12	А	10
	1 011	13	В	11
	1 100	14	С	12
	1 001	15	D	13
	1 110	16	E	14
	1 111	17	F	15
Note that any one or more of the hexadecimal values shown here as "A" through "F" may				
be represented in lower case ("a", "b", etc).				

Table 69Number systems

**Parallelism measurement** – A parallelism measurement consists of two straightness measurements made along the same axis from the same straightness reflector.

Parallelism is calculated by comparing the slopes of the two straightness measurements.

**Plane mirror interferometer** – An interferometer designed to use plane (flat) mirrors to measure motion.

**Proportional error** – A laser wavelength error that is a function of the distance measured.

**Quarter-wave plate** – An optical element which introduces a relative phase shift of 90 degrees between the orthogonal components of a wave. This converts linear polarized light to elliptical light and vice versa.

**Receiver** – The detector, mixer, and electronics to convert the optical signal to an electrical signal.

**Reference frequency** – The laser Reference Frequency is the difference in frequency between the two orthogonally polarized frequency components of the laser beam. The higher the reference frequency, the greater the measurement velocity or slew rate allowed during a measurement (except as limited by system electronics).

The Reference Frequency may also be referred to as the split frequency.

**Referenced interferometer** – An interferometer having internal optical components and laser beam paths whose positions are related to reference surfaces on its housing in specified ways.

**Repeatability** – The maximum deviation between measurements under the same conditions and with the same measuring instrument. This also refers to how stable the measurement will be over time.

**Retroreflector** – Also called a cube corner. A mirror assembly that always reflects light back parallel to the incoming beam.

**Split frequency** – Another name for the Reference Frequency.

The difference between the two frequencies in a two-frequency laser system.

**Straightness** – Straightness is a measurement of displacement perpendicular to the axis of intended motion of the optics.

TCN – Total Compensation Number.

This is a combined compensation term that contains a Wavelength-of-Light compensation term (WCN) and a Material Temperature compensation term (MTC).

**Wavelength tracker** – A device with an interferometer and a fixed measurement path that is immune to ambient temperature and pressure changes. By monitoring the apparent changes in this fixed pathlength, wavelength changes can be very accurately detected (and corrected).

# Index

### Numerics

10717A Wavelenght Tracker troubleshooting, 148 10751C/D Air Sensor, 212 10751C/D Air sensor, 47 10757D/E/F Material Temperature Sensor, 47, 212 10790A/B/C Receiver Cable. 83 10791A/B/C Laser Head Cable, 81 10880A/B/C Receiver Cable, 83 10881A/B/C Laser Head Cable, 81 10881D/E/F Laser Head Cable, 82 10885A PC Axis Board, 46 10886A PC Compensation board, 47 10887B PC Calibrator Board, 47 10888A Remote Control unit, 47 10895A VMEbus Laser Axis Board, 46 10897B High Resolution VMEbus Laser Axis Board, 46 10898A High Resolution VMEbus Dual Laser Axis Board, 46 5517C-009, 75 5517C-009 9-mm Laser Head, 53 5519A/B Laser Head, 47 55292A USB Expansion Module, 47 5529A/55292A system, 47 9-mm beam 5517C-009, 75

# Α

Abbé error definition, 186 minimizing, 220 absolute pressure, 224 ac interferometer, 292 accuracy, 292 definition, 168 accuracy considerations, 40 adjustable mounts, 56, 84 mounts adjustable, 48

adjustment considerations, 48 adjustments, positioning, 56 aids, alignment, 97 air deadpath, 292 air sensor 10751C/D, 47, 212 air turbulence, 214 air turbulence, reducing, 215 aligning and mounting next generation, 123 aligning optic, 88 aligning optics, 32,88 alignment aids, 97 alignment method autoreflection, 92 overlapping dots, 94 alignment principles, 90 alignment techniques autoreflection and overlapping dots, 92 ambient pressure, 224 angular motion, 39 pitch or yaw, 39 API library installation, 29 applications vacuum. 56 atmospheric compensation error, 173 automatic compensation, 210 automatic compensation for the wavelength of light, 160 autoreflection alignment method, 98 autoreflection method alignment procedure, 92 autoreflection method of alignmen, 92 axis electronics. 292 axis, measurement, 106

# В

barometric pressure, 224
basic Agilent Laser Measurement System components, 164
beam benders, 40
beam legs, 91
beam path loss, power budget, 59
beam power loss, optical power loss, 59
beam splitter, 292
beam splitters, 40
beam through window, 114

# С

cable 10881D/E/F Laser Head, 82 N1250A/B High Performance Receiver Cable, 83 N1251A/B High Performance Laser Head Cable, 82 cable, list, 44, 45 cables 10790A/B/C Receiver Cable, 83 10791A/B/C Laser Head Cable, 81 10880A/B/C Receiver Cable, 83

10881A/B/C Laser Head Cable, 81 10881D/E/F Laser Head Cable, 82 laser head, 81 cabling external, 81 calculation of exact Wavelength-of-Light (WOL) compensation factor, 225 calculation of signal loss, 61 calibration board 10887B PC, 47 calibration system electronics, 47 characteristics, required, window, 57 checklist, pre-installation, 80 cleaning fiber-optic cable, 133 cleaning optics, 132 clearance laser heads, 52 CMM. 292 color-coded labels, 81 compensation automatic, 210 manual, 210 compensation board 10886A PC. 47 compensation, Wavelength-of-Light, 292 components basic laser measurement system, 164 computing the optical power loss, 59 configuration effects, 55 configuration example four-axis measurement configuration, 68 multiaxis system for a precision X-Y stage. 67 multiaxis systems using Agilent 10719A and Agilent 10721A, 75 single-axis to control servo-track writing, 65 three-axis measurement system using discrete plane mirror interferometers, 71 two-axis measurement system using two Agilent 10715A differential interferometers, 71 two-axis plane mirror, 69 two-axis plane mirror in a vacuum, 69 configurations multiaxis, 66 controller, 28, 36 coordinate measuring machine, 292 coordinate measuring machines, 215 cosine error, 292 definition, 188

cover, protective, telescoping, 49 cube corner, 292

### D

dc interferometer, 292 deadpath, 292 deadpath counts, 218 deadpath error, 292 definition, 180 deadpath errors compensation for, 217 minimizing, 216 degrees of freedom, 293 determining, 64 determining the overall laser system measurement accuracy, 213 differential configurations customized. 57 differential interferometer, 292 differential measurement, 293 differential measurement in a lithography application, 114 differential measurements with interferometers, 57 differential measurements, with interferometers, 114 direction sense. 110 displacement, how it is measured, 161 doppler frequency shifting, 162 dynamic calibrator 5529A, 47 USB Expansion Module, 47

# E

E1826E/F/G Single-Axis Plane Mirror Interferometer, 218 E1827A Two-Axis Interferometer. 218 E1837A Three-Axis Interferometer, 218 effect on measurement direction sense, 54 effects of configuration, 55 effects of temperature changes, 160 efficiency values. 61 electronic resolution, 170 electronics 10885A PC Axis Board, 46 10897B. 46 5529A/55292A calibration system, 47 N1231A PCI Three-Axis Board, 46 electronics cables connecting, 31 electronics error, 170 electrostatic discharge (ESD), 29 electrostatic discharge, ESD, 293 environment temperature-controlled, 214 environment sensors, 166 environmental conditions, 166 environmental effects, 214

environments vacuum, 56 environments, non-uniform, 214 equipment required, 140 error abbé, 186 atmospheric compensation, 173 cosine, 188, 292 deadpath, definition, 180 proportional, 295 error, deadpath, 292 error, electronics, 170 ESD, 29 ESD, Electrostatic Discharge, 293 etalon, 293 example, determining accuracy and repeatability IC Wafer Stepper, 199 Precision Coordinate Measuring Machine (CMM) example, 191 examples calculation of measurement accuracy and repeatability of Agilent laser systems, 190 expansion coeffients, 280 expansion module USB, 55292A, 47

### F

f2, 293 fA. 293 fasteners, 113 fasteners for optics, 56 fB, 293 fiber-optic cable cleaning, 133 five-axis interferometer Z4421B, 218 five-axis interferometers Z4420B, 218 fl, 293 four-axis measurement configuration example configurations, 68 frequency measurement, 294 fundamental optical resolution, 110

# G

gauge block, 93 grounding laser head, 51 PC electronics, 51 PCI electronics, 51 receiver, 51 system, 81 VME electronics, 51 grounding, system 10895A, 51 10897B, 51 10898A Dual Laser Axis, 51

### Н

half-wave plate, 294 HEX, 294 Hexadecimal, 294

# 

IC Wafer Stepper example, 199 installing laser electronics in PC, 29 inteferometry, Laser, 294 interferometer, 294 ac, 292 dc, 292 differential, 292 E1826E/F/G, 218 E1827A Two-Axis, 218 E1837A Three-Axis, 218 linear. 294 plane mirror, 295 Z4399A Three-Axis, 218 Z4420B Five-Axis (NGI), 218 Z4421B Five-Axis, 218 7.4422B Three-Axis, 218 interferometer (reference) site preparation, 78 interferometer resolutions, 110 interferometers, 160 referenced, a list, 78 interferometers, differential measurements, 114 isolation thermal, 53 vibration, 53

# Κ

kinematic mounting, 294

# L

labels, color-coded, 81 Laser 294 laser beam introducing offset, 58 laser beam protection, 48 laser beam through window, 114 Laser Head, 294 laser head. 164 5517C-009 9-mm, 53 5519A/B, 47 orientation, 52 site preparation, 76 laser head cables, 81 laser head powerup, 31 laser head, mounting feet, 52 Laser Interferometry, 294 laser measurement systems basic parts, 38 laser positioning system one-axis example, 26

laser tube assembly, packing for storage or shipment, 156
laser wavelength, 169
linear interferometer, 294
linear thermalexpansion coefficients of metals and alloys, 280
list of cables, 44, 45
lithography equipment, 215
lithography, differential measurement, 114

### Μ

magnetic shielding, 53 making a measurement, 33 manual compensation, 210 manual organization, 20 manuals available, 23 manuals, how to order. 24 material temperature sensor 10757D/E/F, 47, 212 measurement differential. 293 differential with interferometers, 57 making, 33 parallelism, 295 measurement axis, 106 measurement direction sense, 110 optics affect, 54 measurement frequency, 294 measurement optics summary, table, 107 measurement point tolerance next generation interferometers, 129 metals and alloys linear thermal expansion coeffients, 280 monitor application installation from CD, 29 motion, angluar, 39 motions, possible component, 39 mounting and aligning next generation interferometers, 123 mounting feet on the laser head, 52 mounting plane tolerance, 52 mounting screws for optics, 56 mounting, fasteners, 113 mounting, kinematic, 294 MTC, 294 multiaxis configurations, 66 multiaxis measuring system considerations when designing, 59 multiaxis system for a precision X-Y stage example configuration, 67 multiaxis systems using Agilent 10719A and Agilent 10721A example configuraton, 75 multiaxis systems using Agilent 10735A and Agilent 10736A example configuration, 75

### Ν

N1231A PCI Three-Axis Board, 46 Agilent N1231A. 46 N1250A/B High Performance Receiver Cable, 83 N1251A/B High Performance Laser Head Cable, 82 next generation iInterferometer, 118 next generation interferometer measurement point tolerance, 129 next generation interferometers fiber optic interface specifications, 130 NGI introduction, 118 nominal optical measurement range, 110 Nonlinearity 10706B, 200 10716A, 192 Nonlinearity, 10716A, 192 nonlinearity, optics definition, 172 number systems, 295 base 10, 295 base 16, 295 base 2, 295 base 8, 295

### 0

offset into the laser beam introducing, 58 optic aligning, 88 optical device troubleshooting, 75, 148 optical devices site preparation, 76 optical efficiency, 59, 61 optical power loss computing, 59 optics, 54 aligning, 88 cleaning, 132 system, 164 optics alignment, 32 optics nonlinearity definition, 172 optics protection, 48 optics thermal drift definition, 176 option 5517C-009, 75 overlapping dot alignment procedure alignment method, 102 overlapping dots alignment procedure, 92 overlapping dots alignment method, 94

### Ρ

packaging, original materials, 156 parallelism measurement, 295 pentaprism, 91 pitch, 39 plane and direction, 91 plane mirror interferometer, 295 E1826E/F/G, 218 pointing stability, 53 possible component motions, 39 power safety factor, 62 powering up system, 31 powering up the laser head, 31 Precision Coordinate Measuring Machine (CMM) example, 191 pressure absolute, 224 barometric, 224 problems, solving, 36 proportional error, 295 protecting laser beam, 48 protecting optics, 48

# R

range, nominal optical measurement, 110 receiver, 165 only restriction, 39 receiver cables, 82 receiver mounting locations and positions, 64 receiver troubleshooting, 144 referenced interferometers a list. 78 referenced mirrors (true squares), 98 remote control units 10888A, 47 repeatability definition, 168 resolution system for interferometers, 171 resolution, electronics, 170 resolution, fundamental optical, 110 resolution, interferometers, 110 retroreflectors, 160 returning product to Agilent Technologies, 156 roll, 39

# S

safety checks, 135, 151 sense, measurement direction, 110 sensor placement, 211 sensors, environment, 166 shielding, magnetic, 53 shipment laser tube assembly, 156 single-axis plane mirror interferometer E1826E/F/G, 218 single-axis system to control servo-track writing example configuration, 65 site preparation for laser head, 76

### Index

site preparation for optical devices, 76 site preparation for referenced interferometers, 78 six degrees of freedom, 293 stability, pointing, 53 starting system, 31 storage laser tube assembly, 156 summary of measurement optics, table, 107 system grounding, 51, 81 10895A, 51 10898A, 51 laser head, 51 PC electronics, 51 PCI electronics, 51 receiver, 51 VME electronics, 51 system measurement resolution for each interferometer, 171 system optics, 164 system power-up, 31

### Т

tagging returned products, 156 temperature changes, effects, 160 temperature-controlled environment, 214 test equipment required, 140 thermal drift, optics definition, 176 thermal expansion coeffients, 280 thermal gradients, avoiding, 215 thermal isolation, 53 three-axis interferometer E1837A, 218 Z4399A, 218 Z4422B, 218 three-axis measurement system using discrete plane mirror interferometers example configuration, 71 tolerance, mounting plane, 52 troubleshooting 10717A Wavelength Tracker, 148 10780C/F Receiver, 144 5519A/B Laser Head. 144 laser head, 141 optical device, 75, 148 test equipment required, 140 troubleshooting, receiver, 144 true square, 91, 93 true squares (referenced mirrors), 98 two-axis interferometer E1827A, 218 two-axis measurement system using two Agilent 10715A interferometers example configuration, 71 two-axis plane mirror example configuration, 69 two-axis plane mirror in a vacuum example configuration, 69

two-frequency laser beam, how created, 161

### U

USB Expansion Module, 47

### V

vacuum applications, 56, 114 vacuum chamber, 57 vacuum environments, 56 values efficiency, 61 vibration isolation, 53, 113 VME electronics 10897B High Resolution VMEbus Laser Axis Board, 46 10898A Dual Laser Axis Board, 46

### W

wavelength conversion factor, 219
wavelength of laser light, 160
wavelength, laser, 169
Wavelength-of-Light (WOL), 224
wavelength-of-light value, 160
window, laser beam going through, 114
WOL compensation factor, calculation, 225
WOL compensation method comparison, 213

# Y

yaw, <mark>39</mark>

### Ζ

Z4399A Three-Axis Interferometer, 218 Z4420B Five-Axis Interferometer, 218 Z4421B Five-Axis Interferometer, 218 Z4422B Three-Axis Interferometer, 218



# Service and Support

### **Contacting Agilent Technologies:**

For more information about Agilent test and measurement products, applications, and services, visit our web site at http://www.agilent.com/services/English/index.html.

### Agilent's Test Measurement Fax Service for United States and Canada:

Technical information for test and measurement products and services is available 24 hours a day, 7 days a week, by calling 1-800-829-4444.

### **Technical Support:**

If you need technical assistance with an Agilent test and measurement product or application, you can find a list of local service representatives on the web site listed above. If you do not have access to the Internet, one of the following centers can direct you to your nearest representative:

### **Asia Pacific:**

Hong Kong SAR

Tel: (852) 2599-7777 Fax: (852) 2506-9284

### Australia/New Zealand:

Blackburn, Victoria, Australia

Tel: 61 3 9210 5555

### Canada:

Mississauga, ON, Canada

Tel: 877-894-4414 Fax: (905) 206-4700

### **Europe:**

European Marketing Organization The Netherlands

Tel: +31 20 547 2000 Fax: +31 20 547 7799 Japan:

Measurement Assistance Center Tokyo, Japan

Tel: 81-426-56-7832 Fax: 81-426-60-8747

United States: Test & Measurement Call Center Englewood, CO, U.S.A.

Tel: (800) 829-4444 (Toll free in US)

Printed in U.S.A Data subject to change Rev 12/06

### Continued from front matter. . .

### Warranty (contd)

Agilent does not warrant that the operation of Agilent products will be uninterrupted or error free. If Agilent is unable, within a reasonable time, to repair or replace any product to a condition as warranted, customer will be entitled to a refund of the purchase price upon prompt return of the product.

Agilent products may contain remanufactured parts equivalent to new in performance or may have been subjected to incidental use.

The warranty period begins on the date of delivery or on the date of installation if installed by Agilent. If customer schedules or delays Agilent installation more than 30 days after delivery, warranty begins on the 31st day from delivery.

Warranty does not apply to defects resulting from (a) improper or inadequate maintenance or calibration, (b) software, interfacing, parts or supplies not supplied by Agilent, (c) unauthorized modification or misuse, (d) operation outside of the published environmental specifications for the product, or (e) improper site preparation or maintenance.

TO THE EXTENT ALLOWED BY LOCAL LAW, THE ABOVE WARRANTIES ARE EXCLUSIVE AND NO OTHER WARRANTY OR CONDITION, WHETHER WRITTEN OR ORAL, IS EXPRESSED OR IMPLIED AND AGILENT SPECIFICALLY DISCLAIMS ANY IMPLIED WARRANTIES OR CONDITIONS OF MERCHANTABILITY, SATISFACTORY QUALITY, AND FITNESS FOR A PARTICULAR PURPOSE.

Agilent will be liable for damage to tangible property per incident up to the greater of \$300,000 or the actual amount paid for the product that is the subject of the claim, and for damages for bodily injury or death, to the extent that all such damages are determined by a court of competent jurisdiction to have been directly caused by a defective Agilent product.

TO THE EXTENT ALLOWED BY LOCAL LAW, THE REMEDIES IN

THIS WARRANTY STATEMENT ARE CUSTOMER'S SOLE AND EXCLUSIVE REMEDIES. EXCEPT AS INDICATED ABOVE, IN NO EVENT WILL AGILENT OR ITS SUPPLIERS BE LIABLE FOR LOSS OF DATA OR FOR DIRECT, SPECIAL, INCIDENTAL, CONSEQUENTIAL (INCLUDING LOST PROFIT OR DATA), OR OTHER DAMAGE, WHETHER BASED IN CONTRACT, TORT, OR OTHERWISE.

For consumer transactions in Australia and New Zealand: the warranty terms contained in this statement, except to the extent lawfully permitted, do not exclude, restrict or modify and are in addition to the mandatory statutory rights applicable to the sale of this product to you.

### Assistance

Product maintenance agreements and other customer assistance agreements are available for Agilent products.

For any assistance, contact your nearest Agilent Sales and Service Office.





Manual Part Number 05517-90086, Volume I